

# Southern Ocean Time Series (SOTS) Quality Assessment and Control Report PAR Instruments

Version 2.0 - December 2020

Photosynthetically Available Radiation Records 2009-2019

Peter Jansen, Thomas W. Trull, Christina Schallenberg, James Harley



## Citation

Jansen P, Trull TW, Schallenberg C, and Harley, J (2020). Southern Ocean Time Series (SOTS) Quality Assessment and Control Report PAR Instruments, CSIRO, Australia. DOI: 10.26198/5ce4a647af256 (<http://dx.doi.org/10.26198/5ce4a647af256>)

## Copyright

© Commonwealth Scientific and Industrial Research Organisation 20XX. To the extent permitted by law, all rights are reserved and no part of this publication covered by copyright may be reproduced or copied in any form or by any means except with the written permission of CSIRO.

## Important disclaimer

CSIRO advises that the information contained in this publication comprises general statements based on scientific research. The reader is advised and needs to be aware that such information may be incomplete or unable to be used in any specific situation. No reliance or actions must therefore be made on that information without seeking prior expert professional, scientific and technical advice. To the extent permitted by law, CSIRO (including its employees and consultants) excludes all liability to any person for any consequences, including but not limited to all losses, damages, costs, expenses and any other compensation, arising directly or indirectly from using this publication (in part or in whole) and any information or material contained in it.

CSIRO is committed to providing web accessible content wherever possible. If you are having difficulties with accessing this document please contact [csiroenquiries@csiro.au](mailto:csiroenquiries@csiro.au).

# Contents

Acknowledgments.....	4
Executive summary .....	5
1 Introduction .....	6
2 Moorings Description.....	8
3 Summary of Instruments .....	9
4 Summary of Instrument Handling and Data Processing .....	11
5 QC Specifics.....	12
5.1 QC tests and flags .....	12
5.2 Applied tests .....	13
5.3 Flag statistics.....	20
6 Discussion and recommendations .....	25
6.1 QARTOD tests that were not performed: .....	25
6.2 Main causes for data flagging and associated uncertainties .....	25
6.3 Did the QC tests work and how good are the data?.....	25
6.4 Could the QC tests be improved? What are the implications for QA? .....	28
6.5 Which data should you use?.....	29
7 Plots of PAR vs. Shortwave comparisons .....	30
8 QC flag plots.....	31
9 Accessing the Data .....	32
10 References .....	35
Appendix A Python code used for processing.....	36
Appendix B Sensor Calibration Sheets .....	37

# Acknowledgments

SOTS is supported by the NCRIS IMOS program, CSIRO Oceans and Atmosphere, Bureau of Meteorology, Antarctic Climate and Ecosystems CRC, Australian Antarctic Program Partnership, University of Tasmania, Australian Marine National Facility, and Australian Antarctic Division.

## Executive summary

The Southern Ocean Time Series (SOTS) Observatory located near 141°E and 47°S provides high temporal resolution observations in Subantarctic waters. It is focused on the Subantarctic Zone because waters formed at the surface in this region by deep wintertime convection slide under warmer subtropical and tropical waters, carrying CO<sub>2</sub> and heat into the deep ocean, where it is out of contact with the atmosphere. This process also supplies oxygen for deep ocean ecosystems, and exports nutrients that fuel ~70% of global ocean primary production. Local biological production also impacts carbon cycling and the SOTS moorings measure several variables important to these processes, including photosynthetically available radiation (PAR).

This report describes the quality control procedures applied to PAR data collected from the SOTS moorings between 2009 and 2019. The quality-controlled datasets are publicly available via the IMOS Data Portal. This report should be consulted when using the data.

# 1 Introduction

The Southern Ocean Time Series (SOTS) Observatory provides high temporal resolution observations in Subantarctic waters. Observations are broad and include measurements of physical, chemical and biogeochemical parameters from multiple deep-water moorings in the Subantarctic Zone southwest of Tasmania (Figure 1). The emphasis is on seasonal and inter-annual variations of lower atmosphere and upper ocean properties and their influence on exchange with the deep ocean. The continuous time-series information allows the study of ocean physics and chemistry, climate change, carbon cycling and biogeochemical controls on marine productivity. These moorings provide cost-effective observations and overcome the infrequent availability of ships in the region. The Southern Ocean Time Series is an Australian contribution to the international OceanSITES global network of time series observatories ([www.OceanSITES.org](http://www.OceanSITES.org)) and is one of the few comprehensive Southern Ocean sites globally. More information on the SOTS Sub-Facility is available on-line at <http://www.imos.org.au/>.

The Southern Ocean (south of 30°S) is responsible for ~40% of the total global ocean uptake of human-induced CO<sub>2</sub> emissions, and 75% of the additional heat that these emissions have trapped on Earth. The Southern Ocean Time Series site is focused on the Subantarctic Zone because waters formed at the surface in this region, the Subantarctic mode and Antarctic Intermediate waters, slide under warmer subtropical and tropical waters and carry this CO<sub>2</sub> and heat into the deep ocean, out of contact with the atmosphere. This process also supplies oxygen for deep ocean ecosystems, and exports nutrients that fuel ~70% of global ocean primary production. The Subantarctic Zone and these processes are expected to change with global warming but the potential impacts of these changes are not yet known.

The Southern Ocean Time Series site southwest of Tasmania is comprised of a number of elements including a deep ocean sediment trap mooring (SAZ), a surface biogeochemistry mooring (Pulse) and an air-sea flux mooring (SOFS). Located in the sub-Antarctic Zone near 141°E, 47°S, the site is particularly vulnerable to the extreme weather events that typify the area including very large waves, strong currents and severe storms, presenting significant technical and engineering challenges.

SOTS (red star in Figure 1) is located in a low current region, north of the Subantarctic Front (SAF) that marks the northern edge of the Antarctic Circumpolar Current. SOTS is located in deep waters (>4500 m) west of the Tasman Rise (the shallow region south of Tasmania; with waters less than 2000m deep, shown in blue). The SOTS site exhibits oceanographic properties representative of the Australian sector of the sub-Antarctic Zone (from ~90 to 145 °E; Trull et al., 2001). Waters flowing southward in the East Australian Current reach this region by transiting through channels in the Tasman Rise (Herraiz-Borreguero et al., 2011).

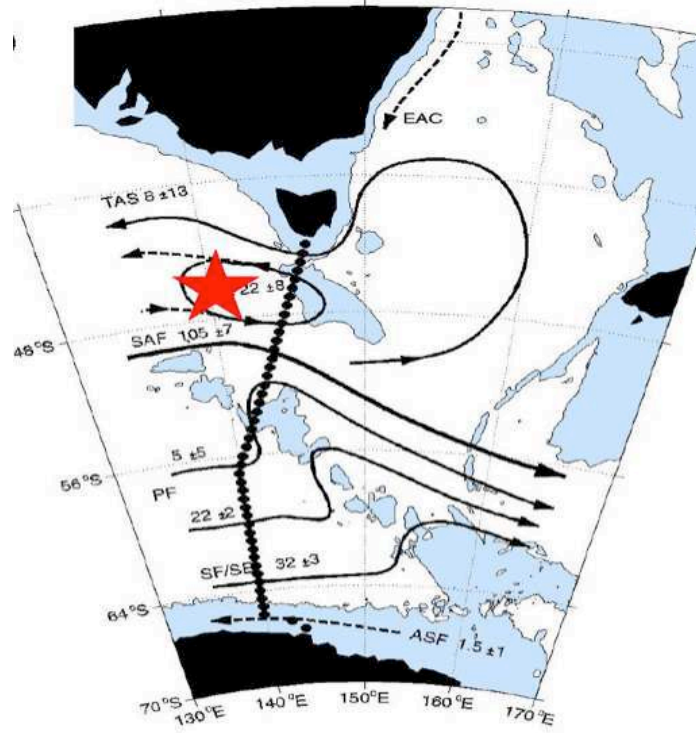


Figure 1 Location of the SOTS observatory; Figure adapted from Herraiz-Borreguero et al., 2011

## 2 Moorings Description

The Southern Ocean Time Series moorings are the Pulse biogeochemistry mooring, the Sub-Antarctic Zone (SAZ) sediment trap mooring, and the Southern Ocean Flux Station (SOFS).

The Pulse biogeochemistry mooring is used to measure upper ocean carbon cycle and phytoplankton productivity processes. Measured parameters include temperature, salinity, dissolved oxygen, total dissolved gases, nitrate, chlorophyll fluorescence and optical particulate backscatter. This mooring also collects water samples for measurements of dissolved carbon and nutrients, and phytoplankton microscopic identification.

The SAZ sediment trap mooring collects sinking particles to quantify carbon fluxes, and provides current meter measurements and a deep ocean CTD to measure heat contents below the depth of Argo profiling float measurements.

The SOFS meteorological tower mooring has dual sets of incoming solar radiometers, temperature and humidity sensors, precipitation gauges and sonic anemometers, and a pCO<sub>2</sub> sensor provided by NOAA. Surface photosynthetically active radiation (PAR) is also measured to help assess light available for phytoplankton production.

All three moorings are anchored to the ocean floor ~4.5 kilometres below the surface. The SOFS and Pulse moorings are s-tether designs that are longer than this, and correspondingly their surface floats move in large 'watch circles'. In contrast, the SAZ mooring is a stiff subsurface mooring with all components more than 700m below the surface. The moorings record hourly sensor observations until they are swapped with a duplicate mooring the following year. In the 2016-17 year, the SOFS and Pulse capabilities were combined into a single prototype mooring known as FluxPulse-1.

Surface data collected from Pulse and SOFS are relayed back by satellite. The sub-surface data are stored and downloaded when the moorings are retrieved (approximately a year later). All data are available via the Australian Ocean Data Network (AODN) Portal.



### 3 Summary of Instruments

A total of 11 different instruments for measuring PAR were deployed at SOTS between 2009 and 2019. These instruments were deployed on two different mooring designs, at varying depths ranging from the surface to a depth of 50m (Refer to table 1 for the deployment depth of each sensor). All instruments were mounted facing upwards.

The PAR sensors deployed at SOTS can be divided into two main functional categories: cosine and spherical. Cosine sensors measure PAR as a downwelling vector quantity, whereas spherical sensors measure PAR as a scalar quantity.

Cosine sensors receive downwelling light through a flat surface and thus underestimate PAR as experienced by phytoplankton, as they are incapable of receiving upwelling light. However, they work well for estimating the downward attenuation of PAR. These sensors use a material that minimizes reflective losses and diffuses light to provide an approximately cosine response to incident angle, as required to estimate the downwelling component of the radiation. As these sensors receive light through a flat surface, they can be wiped to prevent biofouling. Of the cosine sensors deployed at SOTS, only the WET Labs cosine sensors had a wiper attached.

Spherical sensors use a spherical surface to diffuse incoming light before it reaches the sensor. This is intended to provide a more accurate representation of the way in which a cell in the water would receive light. This structure means that sensors mounted at or above the surface may receive light reflecting from the ocean surface. Additionally, spherical sensors are more susceptible to biofouling as the spherical surface cannot be wiped while the sensor is deployed (Kirk 1994).

**Table 1. Instrument deployment details for cosine sensors**

PRODUCER	MODEL	SERIAL NO.	DEPLOYMENTS AND DEPTH
<b>Alec Electronics</b>	DEFI-L	082V023	Pulse-10-2013 (50m) Pulse-11-2015 (50m)
<b>WET Labs</b>	ECO-PAR	134	Pulse-8-2011 (31.1m) Pulse-10-2013 (28m) Pulse-11-2015 (28m)
<b>WET Labs</b>	ECO-PAR	135	Pulse-6-2009 (37.5m) Pulse-7-2010 (31.1m) Pulse-9-2013 (38.5m)
<b>Wet Labs</b>	ECO_PARS	419	SOFS-7-2018 (30m) SOFS-7.5-2018 (30m)
<b>LiCor</b>	LI-190	Q47470	SOFS-4-2013 (Surface - in air) SOFS-5-2015 (Surface - in air) SPFS-6-2017 (Surface - in air) SOFS-7-2018 (Surface - in air) SOFS-7.5-2018 (Surface - in air)
<b>LiCor</b>	LI-190SA	Q40966	SOFS-1-2010 (Surface - in air) SOFS-2-2011 (Surface - in air) SOFS-3-2012 (Surface - in air) FluxPulse-1-2016 (Surface - in air)

**Table 2. Instrument deployment details for spherical sensors**

PRODUCER	MODEL	SERIAL NO.	DEPLOYMENTS AND DEPTH
<b>Alec Electronics</b>	MDS-MKV/L	201318	SOFS-1-2010 (40m) SOFS-2-2011 (40m) SOFS-4-2013 (20m) SOFS-5-2015 (20m)
<b>Alec Electronics</b>	MDS-MKV/L	201319	SOFS-2-2011 (10m) SOFS-4-2013 (40m) SOFS-5-2015 (40m)
<b>Alec Electronics</b>	MDS-MKV/L	200341	Pulse-6-2009 (Surface*) Pulse-7-2010 (Surface) Pulse-8-2011 (50m) Pulse-10-2013 (Surface)
<b>Alec Electronics</b>	MDS-MKV/L	200664	Pulse-6-2009 (27m) Pulse-7-2010 (50m) Pulse-8-2011 (27m)
<b>Alec Electronics</b>	MDS-MKV/L	200665	Pulse-6-2009 (50m) Pulse-7-2010 (27m) Pulse-8-2011 (Surface) Pulse-10-2013 (50m) Pulse-11-2015 (20m)

\*surface instruments were in air

## 4 Summary of Instrument Handling and Data Processing

All Alec Electronics sensors logged to their internal memories. LiCor sensors were logged by a CR1000 data logger. The WETLabs sensors were logged both internally and by an SBE16plusV2. Data obtained from periods when the instruments were out of the water were given a flag value of 6 before initiation of the QC tests applied here, with these flags carried through to the final data products. See Table 4 for flag assignments.

Sensor calibrations are based on different relationships between logged counts and PAR for each sensor type. All PAR data are reported as photon fluxes in units of  $\mu\text{mol m}^{-2}\text{s}^{-1}$ .

The Wet Labs sensors are logarithmic sensors, with counts converted to PAR using the following formula:

$$PAR = Im \times 10^{\frac{counts - a0}{a1}}$$

(Eqn 1.)

*Im* is a water immersion correction (=1 when deployed in air), *a0* corrects any offset from the reference count value for PAR =1, and *a1* represents the sensor's sensitivity.

The LiCor and Alec Electronics sensors are proportional sensors, with counts converted to PAR using the following formula:

$$PAR = A + B \times counts$$

(Eqn 2.)

Where *A* is an offset correction and *B* describes the sensor's sensitivity.

More detail on the specifics of these calibrations can be found in Appendix B.

## 5 QC Specifics

The hierarchy of tests recommended by Integrated Ocean Observing System (IOOS) for Quality Assurance of Real-Time Oceanographic Data (QARTOD; <https://ioos.noaa.gov/project/QARTOD>) was adapted for PAR data quality control. Some of the tests were not applicable to the PAR data and were not conducted, as described in section 5.4 and shown in Table 3. Each test was applied to all data points, including those that had been flagged as fail (flag=4) or suspect (flag=3) in previous tests (see Table 4 for flag nomenclature), and the highest flag from all tests is retained as the overall flag.

### 5.1 QC tests and flags

**Table 3. QC tests recommended by QARTOD for real-time quality assurance for coastal and oceanic ocean optics observations.**

TEST GROUP	TEST NO.	TEST NAME	CONDUCTED
<b>Group 1</b> <i>Required</i>	Test 1	Timing/Gap Test	Yes
	Test 2	Syntax Test	Yes
	Test 3	Location Test	Yes
	Test 4	Gross Range Test	Yes
	Test 5	Decreasing Radiance, Irradiance, and PAR Test	N/A
<b>Group 2</b> <i>Strongly Recommended</i>	Test 6	Photic Zone Limit for Radiance, Irradiance, and PAR Test	N/A
	Test 7	Climatology Test	Yes
	Test 8	Spike Test	No
	Test 9	Rate of Change Test	No
	Test 10	Flat Line Test	Yes
<b>Group 3</b> <i>Suggested</i>	Test 11	Multivariate Test	No
	Test 12	Attenuated Signal Test	No
	Test 13	Neighbour Test	Yes

**Table 4. Flags used in PAR quality control**

The QC flags are provided in the on-line netcdf files and follow the Argo Table 2A Flag convention (equivalent to IMOS Standard Flag, OCEANSITES, and IODE flag conventions) and are as follows:

N	MEANING
0	no QC was performed
1	good data
2	probably good
3	bad data that are potentially correctable
4	bad data
5	value changed
6	not deployed
7	not used
8	interpolated value
9	missing value

## 5.2 Applied tests

### Test 1. Timing/Gap Test:

The timing/gap test checks that all measurements were made at the correct time intervals. The only problem found was that for the in-air sensors on SOFS-1, 2, 3, 4, and 5, on some days only 23 hourly values were recorded (instead of the expected 24). This was considered unlikely to affect data quality and no flags were applied (see Discussion section for note on calculation of daily (24 hour) averages from these data). No other problems were found and therefore no flags were applied. Note that daily means calculated for days with only 23 hourly observations should be based on averaging the PAR observations by the recorded length (23) and not assume 24 hours.

### Test 2. Syntax Test:

The syntax test ensures that all measurements were made in the correct data format. No problems were found and therefore no flags were applied.

### Test 3. Location Test:

The location test is used to check that all measurements were taken at the correct location and at the correct depth. No problems were found and therefore no flags were applied.

### Test 4. Gross Range Test:

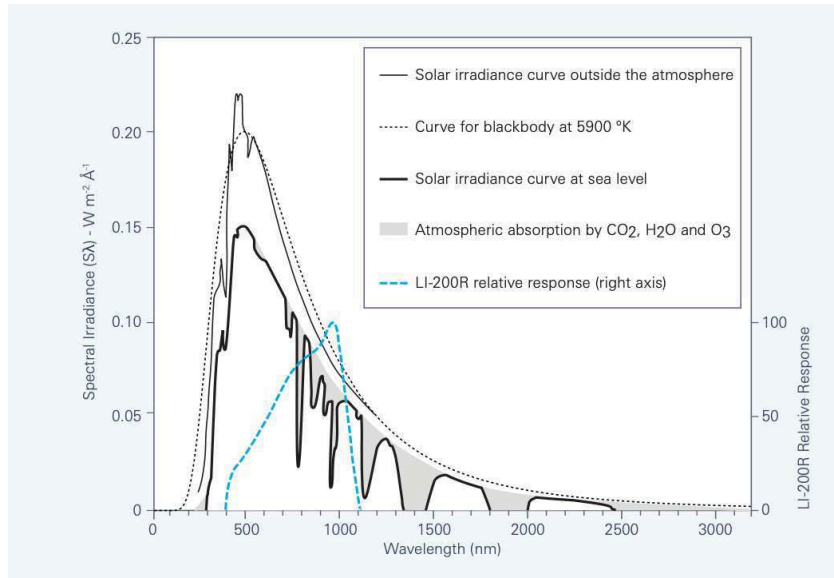
The gross range test checks whether the data are within a reasonable range of values. All data with a value less than -1.7 or higher than 10,000  $\mu\text{mol m}^{-2} \text{s}^{-1}$  were flagged as a fail (flag = 4), and values above 4500  $\mu\text{mol m}^{-2} \text{s}^{-1}$  were flagged as suspect (flag = 3). A lower bound of -1.7 was chosen because the lowest intercept (A) value for the proportional sensor is approximately -1.68. In principle the logarithmic sensors can never produce values less than 0. Therefore, this A value is the lowest possible value a sensor in this sensor set could return when 0 counts are obtained. **As the lower bound for this test is specific for this sensor set, future users of this quality control process will need to set their own lower bound.**

### Test 7. Climatology Test:

The climatology test functions similarly to the gross range test, but threshold values change seasonally. To create bounds for this test, estimates of maximum expected PAR at each depth were created from modelled incident solar irradiance at the top of the atmosphere, propagated to the ocean surface assuming no losses and propagated onward to ocean depth using the clear water value of the diffuse attenuation coefficient ( $K_d = 0.04$ ). This is a conservative  $K_d$  value as seasonal variation is expected. Summer  $K_d$  values reaching 0.1 have been measured at the SOTS

site from CTD casts, and in winter light hits the water at a lower incident angle, decreasing light below the surface due to reflection at the surface.

The solar irradiance model uses the solar constant value of  $1,361 \text{ W m}^{-2}$  and then creates a seasonal cycle based on the Earth's orbit and the solar altitude at different times of year. Top of atmosphere incoming solar radiation values (Figure 2) corresponding to each PAR measurement were calculated using the *suncycle.m* Matlab function (see Appendix A). This function calculates the expected clear-sky solar radiation based on latitude, longitude and date.



**Figure 2 distribution of solar energy**

All calculated solar radiation values from *suncycle.m* were converted from short wave (SW) radiation (300-2000 nm) in units of  $\text{W m}^{-2}$  to PAR (400-700 nm) in units of  $\mu\text{mol m}^{-2} \text{ s}^{-1}$  using a conversion coefficient of  $\text{PAR} = 2.114 \times \text{SW}$ . This conversion is approximate, because it depends on the spectral qualities of the radiation after passing through the atmosphere. The conversion combines two steps: i. estimating the fraction of SW represented by PAR and ii. converting PAR units from energy ( $\text{W m}^{-2}$ ) to photon flux ( $\mu\text{mol m}^{-2} \text{ s}^{-1}$ ). For step i., the fraction of SW represented by PAR averages 0.46 with a seasonal range of  $\sim 4\%$  as estimated by comparing SW and PAR sensors under varying sky conditions in Texas, USA (Britten and Dodd, 1976). For step ii.,  $\text{PAR (in } \mu\text{mol m}^{-2} \text{ s}^{-1}) = \sim 4.57 \times \text{PAR (in } \text{W m}^{-2})$  for combined sun and sky irradiance, with variation of  $\sim 9\%$  in this conversion factor across different sky conditions based on measurements in New Zealand (McCree, 1972; his Table II). Together these lead to the conversion factor of 2.114 ( $4.57 \times 0.46$ ) with precision of  $\sim 10\%$ .

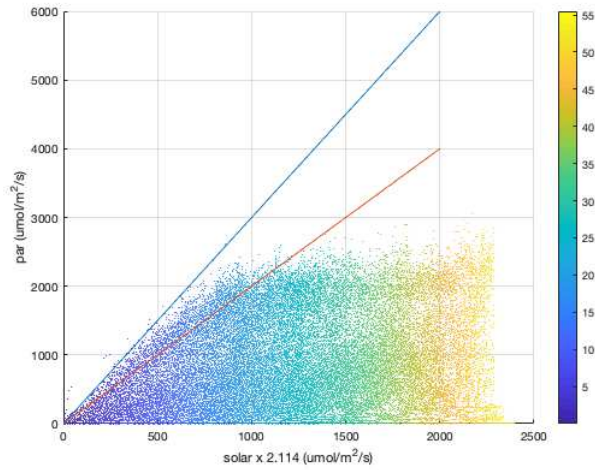
The downwelling climatological PAR estimated was calculated according to the following formula:

$$\text{PAR (sensor depth } z) = \text{PAR (at ocean surface)} \times e^{-K_d \times \text{depth } z \text{ of sensor}} \quad (\text{Eqn 3.})$$

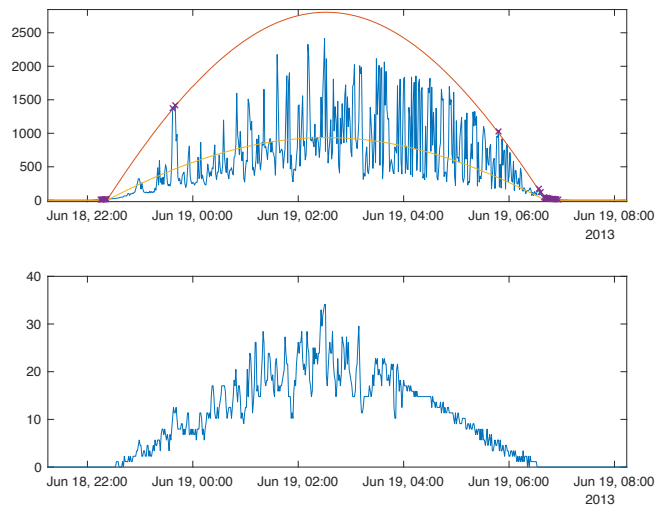
These PAR values represent the amount of down-welling radiation that would theoretically reach the sensors on a sunny, clear-sky day with completely clear water (for  $K_d = 0.04$ ), and no modulation by the air-sea interface (losses at the interface are typically 2-20% increasing with the angle from the vertical; thus assuming no loss leads to a conservative upper estimate of expected PAR). Spherical geometry sensor values can exceed these values by a factor of 2. Reflections from

the sea-surface can further increase radiation for in-air sensors, and focusing of light by waves can affect in-water sensors. To allow for these factors, we set the PAR threshold for this test as 3 times the climatological value, and any sensor values higher than this were assigned a flag value of 3.

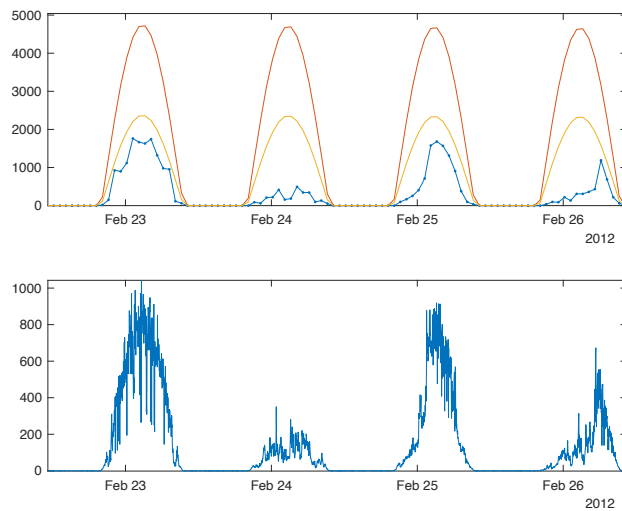
This test is less useful during dawn, dusk, and night as light conditions are not well represented by the solar radiation model (e.g. as a result of moonlight, low angle reflections from clouds, or refraction in the atmosphere) and the test begins to flag a large number of values that may be of good quality (an example is shown in Figure 3). Therefore, all data points when the sun altitude was below 10 degrees were deemed unable to be evaluated by the test and were assigned a flag value of 2, and when the sun was 15 degrees below the horizon, radiation values above  $15 \text{ } \mu\text{mol m}^{-2} \text{ s}^{-1}$  were flagged 4. Figures 4 and 5 show examples of the daily light cycle at the ocean surface (which has similar shape to that of the incoming insolation at the top of the atmosphere) and below the surface (where the daily cycle has a more triangle shape as a result of the surface reflection dependence on the insolation angle). These daily cycles are also strongly modulated by variations in cloudiness.



**Figure 3** surface spherical sensor example distribution, lines for 2x and 3x incoming radiation, coloured by sun altitude



**Figure 4** TOP: example surface spherical PAR sensor, lines for solar and 3x solar, BOTTOM: 50m spherical sensor



**Figure 5** TOP: example surface cosine sensor with solar and 2xsolar, BOTTOM: 10m spherical sensor



### Test 10. Flat Line Test:

The flat line test is intended to catch decreasing sensor sensitivity or failure. The flat line test was applied across all sensors. This test was only run on daytime data as all sensors would be expected to flat line somewhat during the night.

The flat line test was implemented using a rolling window of 5 data points. The following formula was applied to each set of data points:

$$|\mathit{maximum\ value} - \mathit{minimum\ value}| = 0 \quad (\text{Eqn 4.})$$

The final data point in any set of 5 points that returned TRUE for equation 5 was assigned a flag of 4. Any points that were unable to be evaluated due to not having enough subsequent points to create a window of 5 points were assigned a flag value of 2.

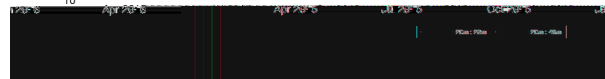
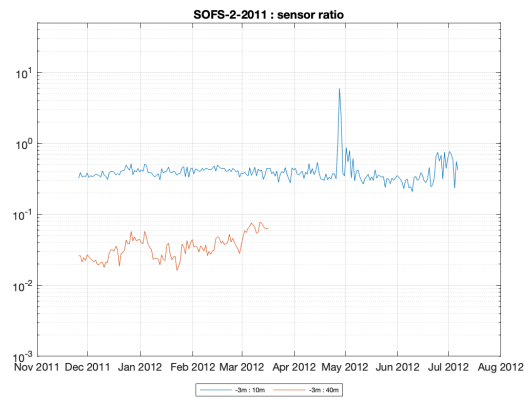
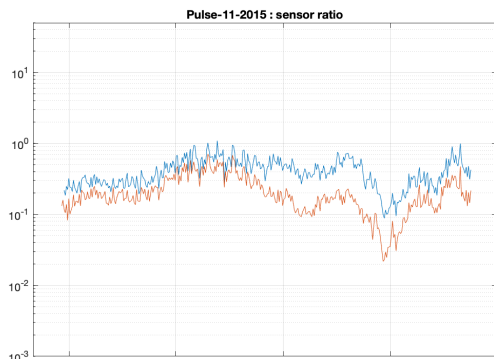
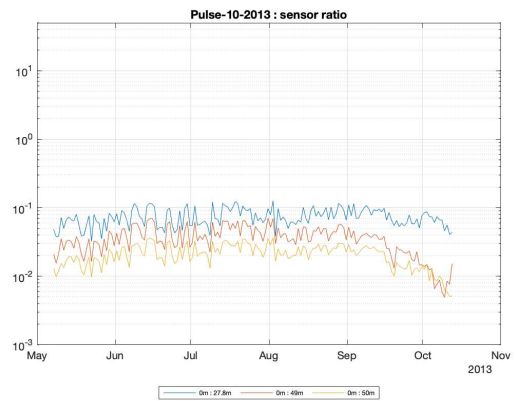
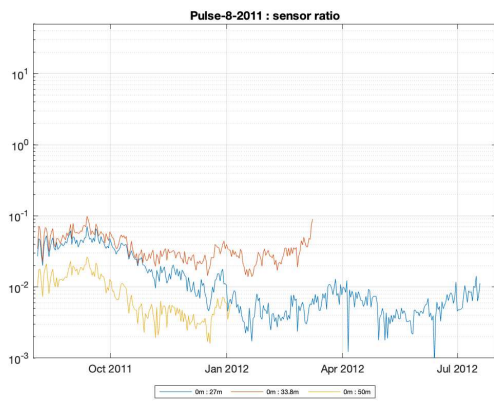
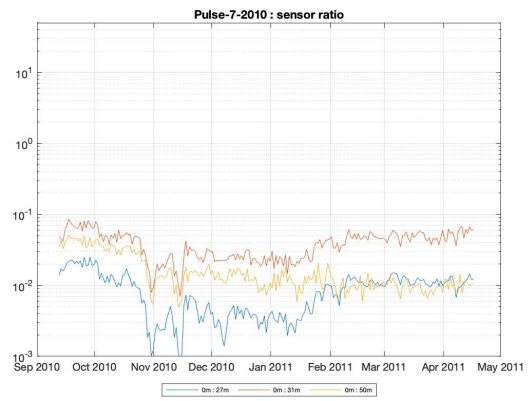
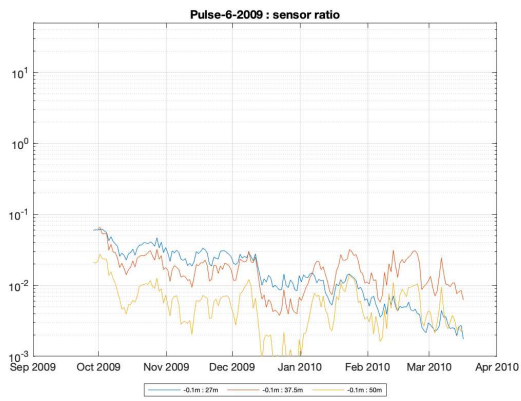
### Test 13. Neighbour Test:

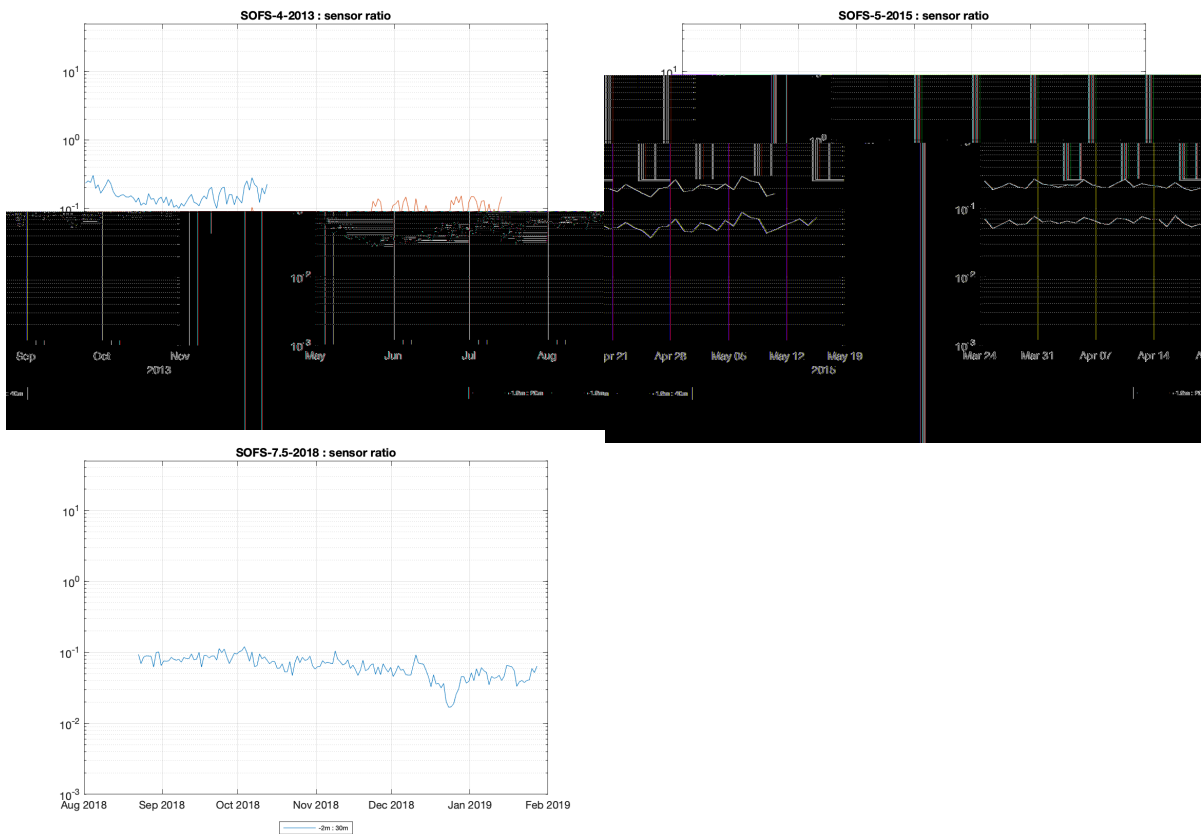
The neighbour test used all PAR sensors deployed on the same mooring and compared their records. The theory is that all sensors should show similar trends with time, with the sensors at greater depths giving a more attenuated signal. The test thus consisted of comparing each sensor to those mounted below and above them on the mooring. Daily means were used so that offsets between sensor clocks would not lead to flagging of data on days with fast passing clouds.

In Version 1.0 of this report, these comparisons were automated, but as noted there this meant that when only two sensors disagreed, e.g. with the shallower sensor having lower PAR than the deeper sensor, it was not possible to know which sensor was in error and thus both were flagged as suspect.

In this Version 2.0 of this report, we have instead implemented a visual check of the sensor ratios among the pairs of sensors to allow not only their relative values but also comparison of these across multiple pairs to be examined. These visualisations and the manual QC decisions based on them are detailed in section 5.2.1.

## 5.2.1 Plots of sensor ratios





**Manual QC decisions based on the Neighbour Test plots and inter-annual comparisons.**

The following sensors were marked 3 (probably bad) after inspection of the nearest Neighbour plots, as well as from inter-annual variations as discussed below in Section 6.

**Pulse-6**

SN 200341 after 2009-09-22: sensor scaling incorrect, saturates

SN 200664 after 2010-01-02: bio-fouled, drops below deeper sensor

**Pulse-7-2010**

SN 200665 after 2011-02-01: bio-fouled, drops below deeper sensor

**Pulse-8-2011**

SN 200664 after 2011-10-01: bio-fouled, drops below deeper sensor

**Pulse-11-2015**

SN 082V023 after 2013-09-15: bio-fouled, drops below deeper sensor

**SOFS-1-2010**

SN Q40966 after 2010-03-05: sensor scaling issue

## 5.3 Flag statistics

### Flags

- PAR\_quality\_control : overall flag
- PAR\_quality\_control\_cl : climatology flag
- PAR\_quality\_control\_gr : global range flag
- PAR\_quality\_control\_io : in/out of water flag
- PAR\_quality\_control\_man : manual flagging

**Table 5. Flag counts from each deployment for each test**

deployment	instrument	Serial number	depth	flag	unknown	Good data	Probably good data	Probably bad data	Bad data	Not deployed	interpolated	Missing value	
Pulse-6-2009	MDS-MKVL	200341	-0.1	Final	0	0	0	0	246304	15141	0	0	
			-0.1	Cl	0	187534	58504	267	0	0	0	0	
			-0.1	Gr	0	246305	0	0	0	0	0	0	0
			-0.1	Io	246304	0	0	0	0	0	15141	0	0
	-0.1	Man	0	0	0	0	0	246305	0	0	0		
	MDS-MKVL	200664	27	Final	0	104754	33485	108125	0	15114	0	0	
			27	Cl	0	187861	58504	0	0	0	0	0	
			27	Gr	0	246365	0	0	0	0	0	0	0
			27	Io	246364	0	0	0	0	0	15114	0	0
	27	Man	138240	0	0	108125	0	0	0	0	0		
	ECO-PAR	PARS-134	37.5	Final	0	3102	957	0	0	0	0	0	
			37.5	Cl	0	3102	957	0	0	0	0	0	
			37.5	Gr	0	4059	0	0	0	0	0	0	0
			37.5	Io	4059	0	0	0	0	0	0	0	0
	MDS-MKVL	200665	50	Final	0	187860	58504	0	0	0	15738	0	0
			50	Cl	0	187861	58504	0	0	0	0	0	0
50			Gr	0	246365	0	0	0	0	0	0	0	
50			Io	246364	0	0	0	0	0	15738	0	0	
SOF5-1-2010	LI-190SA	Q40966	-2.72	Final	0	0	0	0	7501	539	0	0	
			-2.72	Cl	0	5578	1727	196	0	0	0	0	
			-2.72	Gr	0	7501	0	0	0	0	0	0	0
			-2.72	Io	7501	0	0	0	0	0	539	0	0
	-2.72	Man	0	0	0	0	0	7501	0	0	0		
	MDS-MKVL	201318	40	Final	0	161082	48167	0	0	0	1801	0	0
			40	Cl	0	161083	48167	0	0	0	0	0	0
			40	Gr	0	209250	0	0	0	0	0	0	0
40			Io	209249	0	0	0	0	0	1801	0	0	
Pulse-7-2010	MDS-MKVL	200341	0	Final	0	240242	73437	0	0	23360	0	0	
			0	Cl	0	240243	73437	0	0	0	0	0	

deployment	instrument	Serial number	depth	flag	unknown	Good data	Probably good data	Probably bad data	Bad data	Not deployed	interpolated	Missing value
			0	Gr	0	313680	0	0	0	0	0	0
			0	lo	313679	0	0	0	0	23360	0	0
	MDS-MKVL	200664	27	Final	0	240242	73437	0	0	23396	0	0
			27	Cl	0	240243	73437	0	0	0	0	0
			27	Gr	0	313680	0	0	0	0	0	0
			27	lo	313679	0	0	0	0	23396	0	0
	ECO-PARS	PARS-135	31	Final	0	4022	1206	0	0	444	0	0
			31	Cl	0	4022	1206	0	0	0	0	0
			31	Gr	0	5228	0	0	0	0	0	0
			31	lo	5228	0	0	0	0	444	0	0
	MDS-MKVL	200665	50	Final	0	154369	50110	109200	0	122990	0	0
			50	Cl	0	240243	73437	0	0	0	0	0
			50	Gr	0	313680	0	0	0	0	0	0
			50	lo	313679	0	0	0	0	122990	0	0
			50	Man	204480	0	0	109200	0	0	0	0
Pulse-8-2011	MDS-MKVL	200665	0	Final	0	387857	117388	0	0	6755	0	0
			0	Cl	0	387858	117388	0	0	0	0	0
			0	Gr	0	505246	0	0	0	0	0	0
			0	lo	505245	0	0	0	0	6755	0	0
	MDS-MKVL	200664	27	Final	0	65866	17593	421786	0	6755	0	0
			27	Cl	0	387858	117388	0	0	0	0	0
			27	Gr	0	505246	0	0	0	0	0	0
			27	lo	505245	0	0	0	0	6755	0	0
			27	Man	83460	0	0	421786	0	0	0	0
	ECO-PARS	PARS-134	33.8	Final	0	20201	6254	0	0	1364	0	0
			33.8	Cl	0	20201	6254	0	0	0	0	0
			33.8	Gr	0	26455	0	0	0	0	0	0
			33.8	lo	26455	0	0	0	0	1364	0	0
	MDS-MKVL	200341	50	Final	0	169764	51870	0	0	3541	0	0
			50	Cl	0	169765	51870	0	0	0	0	0
			50	Gr	0	221635	0	0	0	0	0	0
			50	lo	221634	0	0	0	0	3541	0	0
SOFS-2-2011	LI-190SA	Q40966	-3	Final	0	3794	1284	336	0	385	0	0
			-3	Cl	0	3794	1284	336	0	0	0	0
			-3	Gr	0	5414	0	0	0	0	0	0
			-3	lo	5414	0	0	0	0	385	0	0
	MDS-MKVL	201319	10	Final	0	132334	41155	0	0	14492	0	0
			10	Cl	0	132335	41155	0	0	0	0	0

deployment	instrument	Serial number	depth	flag	unknown	Good data	Probably good data	Probably bad data	Bad data	Not deployed	interpolated	Missing value
			10	Gr	0	173490	0	0	0	0	0	0
			10	lo	173489	0	0	0	0	14492	0	0
	MDS-MKVL	201318	40	Final	0	61717	20221	0	0	3601	0	0
			40	Cl	0	61718	20221	0	0	0	0	0
			40	Gr	0	81939	0	0	0	0	0	0
			40	lo	81938	0	0	0	0	3601	0	0
<b>SOFS-3-2012</b>	LI-190SA	Q40966	-2.8	Final	0	3155	942	0	1	672	0	0
			-2.8	Cl	0	3156	942	0	0	0	0	0
			-2.8	Gr	0	4097	0	0	1	0	0	0
			-2.8	lo	4098	0	0	0	0	672	0	0
<b>Pulse-9-2012</b>	ECO-PARS	PARS-135	38	Final	0	15956	4727	0	0	4479	0	0
			38	Cl	0	15956	4727	0	0	0	0	0
			38	Gr	0	20683	0	0	0	0	0	0
			38	lo	20683	0	0	0	0	4479	0	0
<b>SOFS-4-2013</b>	LI-190SA	Q47470	-1.8	Final	0	1395	905	1691	0	1278	0	0
			-1.8	Cl	0	1395	905	1691	0	0	0	0
			-1.8	Gr	0	3991	0	0	0	0	0	0
			-1.8	lo	3991	0	0	0	0	1278	0	0
	MDS-MKVL	201318	20	Final	0	81219	25471	0	0	4861	0	0
			20	Cl	0	81220	25471	0	0	0	0	0
			20	Gr	0	106691	0	0	0	0	0	0
			20	lo	106690	0	0	0	0	4861	0	0
	MDS-MKVL	201319	40	Final	0	185634	54060	0	0	16809	0	0
			40	Cl	0	185635	54060	0	0	0	0	0
			40	Gr	0	239695	0	0	0	0	0	0
			40	lo	239694	0	0	0	0	16809	0	0
<b>Pulse-10-2013</b>	MDS-MKVL	200341	0	Final	0	177561	52082	3	0	26805	0	0
			0	Cl	0	177561	52082	3	0	0	0	0
			0	Gr	0	229646	0	0	0	0	0	0
			0	lo	229646	0	0	0	0	26805	0	0
	ECO-PARS	PARS-134	27.8	Final	0	14772	4368	0	0	156	0	0
			27.8	Cl	0	14772	4368	0	0	0	0	0
			27.8	Gr	0	19140	0	0	0	0	0	0
			27.8	lo	19140	0	0	0	0	156	0	0
	DEFI-L	082V023	49	Final	0	177564	52082	0	0	26933	0	0
			49	Cl	0	177564	52082	0	0	0	0	0

deployment	instrument	Serial number	depth	flag	unknown	Good data	Probably good data	Probably bad data	Bad data	Not deployed	interpolated	Missing value
			49	Gr	0	229646	0	0	0	0	0	0
			49	lo	229646	0	0	0	0	26933	0	0
	MDS-MKVL	200665	50	Final	0	177564	52082	0	0	26735	0	0
			50	Cl	0	177564	52082	0	0	0	0	0
			50	Gr	0	229646	0	0	0	0	0	0
			50	lo	229646	0	0	0	0	26735	0	0
<b>SOFS-5-2015</b>	LI-190SA	Q47470	-1.8	Final	0	6706	2073	322	6	583	0	0
			-1.8	Cl	0	6711	2074	322	0	0	0	0
			-1.8	Gr	0	9101	0	0	6	0	0	0
			-1.8	lo	9107	0	0	0	0	583	0	0
	MDS-MKVL	201318	20	Final	0	55916	15070	0	0	3035	0	0
			20	Cl	0	55916	15070	0	0	0	0	0
			20	Gr	0	70986	0	0	0	0	0	0
			20	lo	70986	0	0	0	0	3035	0	0
	MDS-MKVL	201319	40	Final	0	61322	16543	0	0	3035	0	0
			40	Cl	0	61322	16543	0	0	0	0	0
			40	Gr	0	77865	0	0	0	0	0	0
			40	lo	77865	0	0	0	0	3035	0	0
<b>Pulse-11-2015</b>	MDS-MKVL	200665	20	Final	0	389500	118320	0	0	4980	0	0
			20	Cl	0	389500	118320	0	0	0	0	0
			20	Gr	0	507820	0	0	0	0	0	0
			20	lo	507820	0	0	0	0	4980	0	0
	ECO-PAR	PARS-134	28	Final	0	6623	1991	0	0	242	0	0
			28	Cl	0	6623	1991	0	0	0	0	0
			28	Gr	0	8614	0	0	0	0	0	0
			28	lo	8614	0	0	0	0	242	0	0
	DEFI-L	082V022	49	Final	0	398182	120822	0	0	20946	0	0
			49	Cl	0	398182	120822	0	0	0	0	0
			49	Gr	0	519004	0	0	0	0	0	0
			49	lo	519004	0	0	0	0	20946	0	0
<b>FluxPulse-1-2016</b>	LI-190SA	Q40966	-1.8	Final	0	1831	525	0	1	977	0	0
			-1.8	Cl	0	1832	525	0	0	0	0	0
			-1.8	Gr	0	2356	0	0	1	0	0	0
			-1.8	lo	2357	0	0	0	0	977	0	0
<b>SOFS-6-2017</b>	LI-190SA	Q47470	-1.8	Final	0	2837	1070	1083	455	1199	0	0
			-1.8	Cl	0	3169	1193	1083	0	0	0	0

deployment	instrument	Serial number	depth	flag	unknown	Good data	Probably good data	Probably bad data	Bad data	Not deployed	interpolated	Missing value
			-1.8	Gr	0	4990	0	0	455	0	0	0
			-1.8	lo	5445	0	0	0	0	1199	0	0
<b>SOFS-7-2018</b>	LI-190SA	Q47470	-1.8	Final	0	184	61	0	0	560	0	0
			-1.8	Cl	0	184	61	0	0	0	0	0
			-1.8	Gr	0	245	0	0	0	0	0	0
			-1.8	lo	245	0	0	0	0	560	0	0
<b>SOFS-7.5-2018</b>	LI-190SA	Q47470	-2	Final	0	2815	905	33	0	1292	0	0
			-2	Cl	0	2815	905	33	0	0	0	0
			-2	Gr	0	3753	0	0	0	0	0	0
			-2	lo	3753	0	0	0	0	1292	0	0
	ECO-PARS	PARSB-419	30	Final	0	19460	6015	0	0	795	0	0
			30	Cl	0	19460	6015	0	0	0	0	0
			30	Gr	0	25475	0	0	0	0	0	0
			30	lo	25475	0	0	0	0	795	0	0



# 6 Discussion and recommendations

## 6.1 QARTOD tests that were not performed:

Some of the recommended QARTOD tests were deemed not applicable to the PAR data. As all the sensors are mounted at discrete depths on the mooring, tests related to depth profiles (Test 5 and Test 6 in Table 3) were not conducted.

Given that PAR values can change rapidly within a short period of time, a spike test was also not deemed useful. It would be difficult to differentiate a spike due to a problem with a sensor from natural changes in PAR, e.g. due to clouds covering or uncovering the sun, or wave focusing.

Similarly, the attenuated signal test cannot readily be adapted to the PAR data as it would be difficult to distinguish attenuation of the signal due to biofouling from attenuation due to periods of predominantly overcast conditions, as frequently observed in the Southern Ocean.

## 6.2 Main causes for data flagging and associated uncertainties

The most common reasons for data concern (flag 3) were showing too high

values in the Climatology test or values which did not display oceanographic consistency in the manual Neighbour test, i.e. the values were either higher than those from shallower sensors or lower than those from deeper sensors. The Neighbour Test was also the most common reason for data rejection (flag 4) which occurred when 1 sensor failed against multiple other sensors. The flagging of data by these tests is shown for all sensors in the plots in Section 8.

## 6.3 Did the QC tests work and how good are the data?

Evaluating the success of the tests requires determining whether they correctly identified and flagged only and all *truly* bad data (flag 4) and possibly bad data (flag 3) and retained only and all *truly* good (flag 1) data. This requires some independent understanding of which data is good. We examined this in several ways, as described in sections 6.3.1, 6.3.2, and 6.3.3.

### 6.3.1 Comparison to in-air shortwave sensors on the SOFS moorings

First the PAR fraction was estimated from the shortwave sensors, using the same expressions as for conversion of the modelled top of atmosphere insolation in the climatology test. Then plots of the ratio of the in-air PAR sensors to these shortwave-based PAR estimates were examined (plots are shown in Section 7). For the in-air sensors a ratio of 1 is expected, and often occurred. But some sensors were offset by 30-50%. This gives an indication of the relative accuracy of the sensors and interannual variations constructed from them. In general, these plots reveal very good agreement between the LiCor planar PAR sensors and the shortwave planar sensors, and also show that the spherical Alec sensors have higher values by  $\sim 2x$  as expected from geometrical considerations (with deviations that are highest in winter when the incident angle is low and reflections are more problematic).

### 6.3.2 Comparison to expected PAR values at depth

This is based on estimates for the PAR attenuation coefficient for reasonable values of biomass loading. In Version 1.0 of this report, this was done as an extension of the climatology test (which set upper bounds on PAR at depth using the blue water attenuation coefficient value of  $K_d = 0.04$ ), and consisted of calculating two other  $K_d$  estimates of 0.12 and 0.15 for chlorophyll levels of 0.5 and  $1.0 \mu\text{g L}^{-1}$ , respectively, using the equations of Morel et al., (2007):

**Table 6 typical  $K_d$  values for chlorophyll  $a$  concentration**

<i>chl (<math>\mu\text{g L}^{-1}</math>)</i>	<i>kd (490)</i>	<i>kd (PAR)</i>
0.03	0.02	0.05
0.5	0.07	0.12
1	0.09	0.15
5.6	0.26	0.30

$$K_d(\text{PAR})_2 = 0.0665 + 0.874 K_d(490) - 0.00121[K_d(490)]^{-1}$$

$$K_d(490) = 0.0166 + 0.0773[\text{Chl}]^{0.6715}$$

These choices of Chl values were based on sparse in-situ HPLC pigment analyses at the SOTS site and satellite remote sensing estimates which suggest that maximum chlorophyll  $a$  concentrations are typically  $\sim 0.6 \mu\text{g L}^{-1}$  (Eriksen et al., 2018). These  $K_d$  values were then used to calculate expected PAR values at depth to which the data were compared to assess whether the observed PAR values were reasonable (and in general they were – see the Version 1.0 report).

In this Version 2.0 report, we have modified the approach to compare observed and expected  $K_d$  values (rather than PAR values) and have used Chl estimates based on in-situ fluorescence measurements from the SOTS moorings to calculate expected  $K_d$  values. The observed  $K_d$  values were calculated from sensor ratios relative to the surface short wave radiation sensor (after conversion to  $\mu\text{mol m}^{-2} \text{s}^{-1}$  of PAR). The expected  $K_d$  values were calculated using the equations of Morel et al., (2007) from the chlorophyll measured at night by the FLNTUS sensor, after multiplying the sensor output by a scale factor of 0.32 as estimated from comparison to HPLC pigment analyses, as detailed in Schallenberg et al. (2019).

These observed and expected  $K_d$  values are shown in Figure 6. In general, they suggest that the low PAR values at depth can be understood as the result of attenuation by overlying biomass (rather than bio-fouling). Specifically, the  $K_d$  values based on the sensor pairs ranged from 0.04 (the blue water value) to 0.25, and the  $K_d$  values based on the FLNTUS chlorophyll estimates ranged from 0.04 to 0.21. The highest  $K_d$  values from the PAR sensor pairs do correspond with times of suspected bio-fouling based on the Neighbour test (see section 5). The plots also show that the observed lower seasonal amplitude of PAR variations at depth compared to at the surface is expected based on the seasonal cycle of chlorophyll. Interestingly, the FLNTUS based  $K_d$  estimates shown larger seasonality than the PAR based  $K_d$  estimates, which could arise from community or physiological variations (Schallenberg et al., 2019).

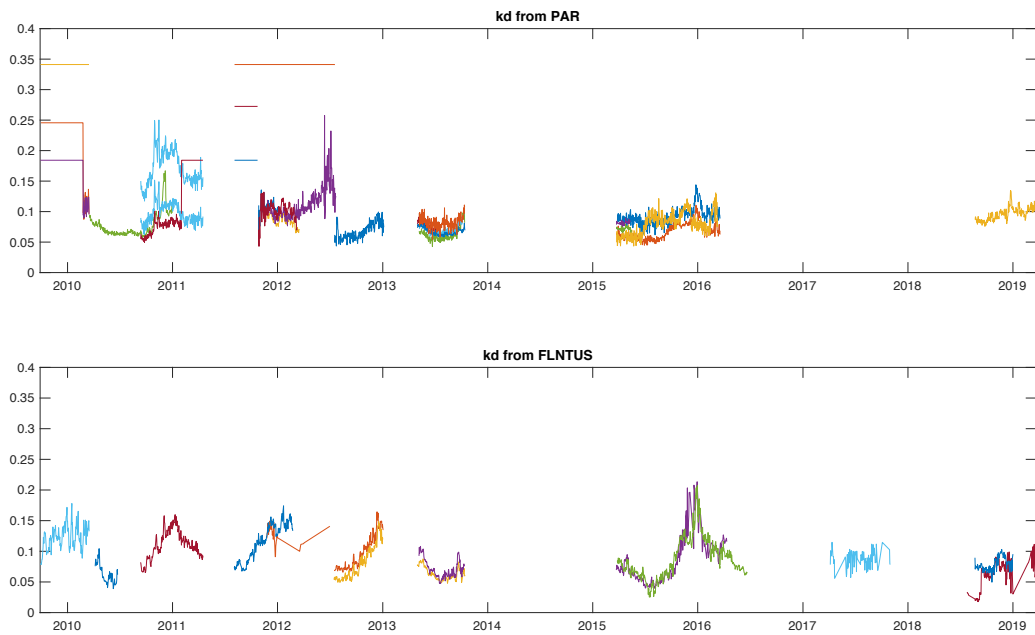
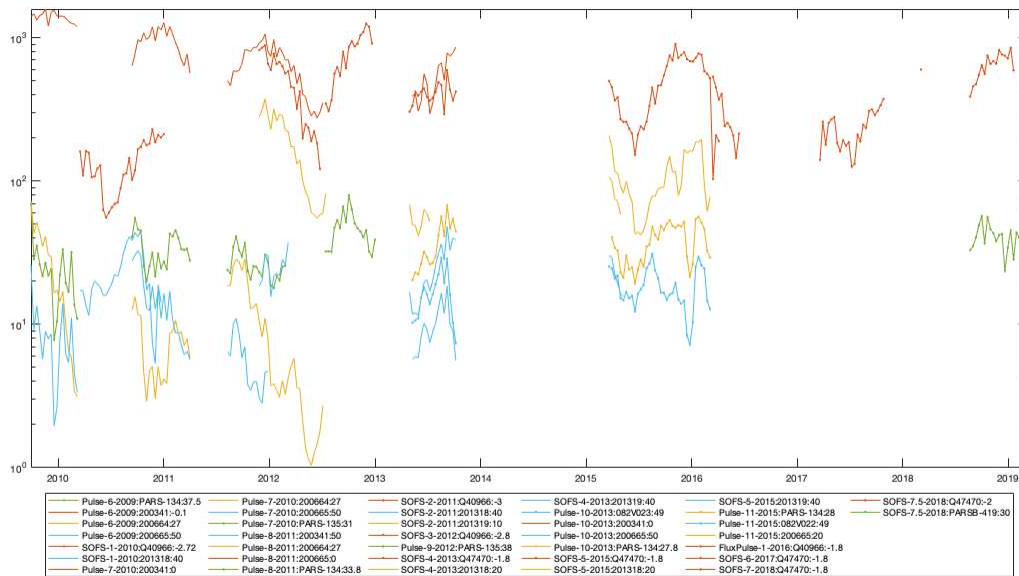


Figure 6 Top Panel, K<sub>d</sub> from PAR/SWR : Bottom Panel K<sub>d</sub> from FLNTUS data. The high K<sub>d</sub> values in 2011 (upper light blue) is the Pulse-7 sensor at 27m, which based on this comparison reads low (higher K<sub>d</sub>) as evident in the plots in section 5.2.1

### 6.3.3 Examination of multi-year records for consistency

The plots of the in-air PAR sensors across all years (Figure 7) suggested that the SOFS-1 data were unusually low and the Pulse-6 data were unusually high, and caused us to review these results. It was found that installation of the SOFS-1 sensor had not included a required resistor and that there was no way to assuredly re-scale for this error. Accordingly, all the SOFS-1 in-air PAR data was manually flagged 4. Comparison to the shortwave sensor on this mooring (see plots in Section 8) suggests it had a constant offset that could be corrected, but this was not pursued since it is more direct to simply use shortwave sensor data if a PAR estimate is required for SOFS-1. Review of the Pulse 6 in-air sensor calibration showed that its calibration values as provided by the manufacturer were unusual, and accordingly all its data were manually flagged 3 (as corrected data could be estimated in principle using a later sensor calibration).



**Figure 7. Daily daylight mean PAR values from surface sensors deployed at different times; note logarithmic scale on the y-axis. The mean PAR in summer for the SOFS 1 surface sensor was significantly lower than the records from other sensors placed at the same position in different years. Also note that the spherical sensor on Pulse 6 produces consistently higher summer values than the cosine sensors on the SOFS moorings. Based on these differences, review or those sensor results led to their flagging as suspect (flag 3). See Section 6 for Discussion.**

## 6.4 Could the QC tests be improved? What are the implications for QA?

A challenging obstacle to more thorough quality control of this dataset is the difficulty of distinguishing sensor issues from the impact of cloudy days on the PAR observations (and the full shortwave radiation observations). The QC effort could be improved if reliable cloudiness estimates become available to be used in tests or at least in evaluations.

Similarly, it is difficult to evaluate whether low PAR values at depth derive from biomass loading in the water column or from biofouling on the sensors. This problem favours the choice of wiped sensors, but with recognition that even they are not always immune from fouling.

There were many points that were flagged as suspect in the Neighbour test due to a sensor at a shallower depth producing lower PAR values. It is difficult for this pairwise test to show which of these sensors is at fault. In some cases, plots of the data help to discern the sensor most likely to be at fault, based on deviations from seasonal expectations (see plots in Section 7).

The multi-year consistency evaluations discussed in section 6.3.3 were important in recognizing several problems missed by the implemented QARTOD. In future years, it may be possible for an improved PAR climatology based in part on the SOTS observations to improve the bounds set on the Gross Range and Climatology test. Nonetheless, many aspects of this first evaluation of the PAR data emphasize that delayed mode QC requires dedicated visualization beyond what can be achieved with QARTOD type tests.

A few overall recommendations for Quality Assurance have emerged from the QC:

1. Check all sensor calibrations against the growing record of calibrations to verify that none are unusual and thus potentially suspect.
2. Favour wiped sensors over unwiped sensors.
3. Pair sensors whenever possible, and favour deploying pairs of sensors at a few depths over single sensors at more depths.
4. Compare all sensors against the shortwave sensors before and after deployment.

## 6.5 Which data should you use?

We recommend that you use all PAR data with flag values of 2 or less. This is because none of this data has failed a QC test (the only reason that a flag value of 2 has been assigned is that one or more of the tests could not be performed). For in-air PAR estimates, we recommend that the shortwave sensor measurements are likely to provide the highest quality estimates, after scaling to units of PAR as in the Climatology test. For in-water PAR estimates, it is important to recognize that the flat (cosine-response) sensors and the spherical sensors measure different quantities, and thus these should not be directly compared or combined (e.g. to estimate attenuation).

## 7 Plots of PAR vs. Shortwave comparisons

This section shows sets of 3 plots for all sensors deployed in each year, in chronological order.

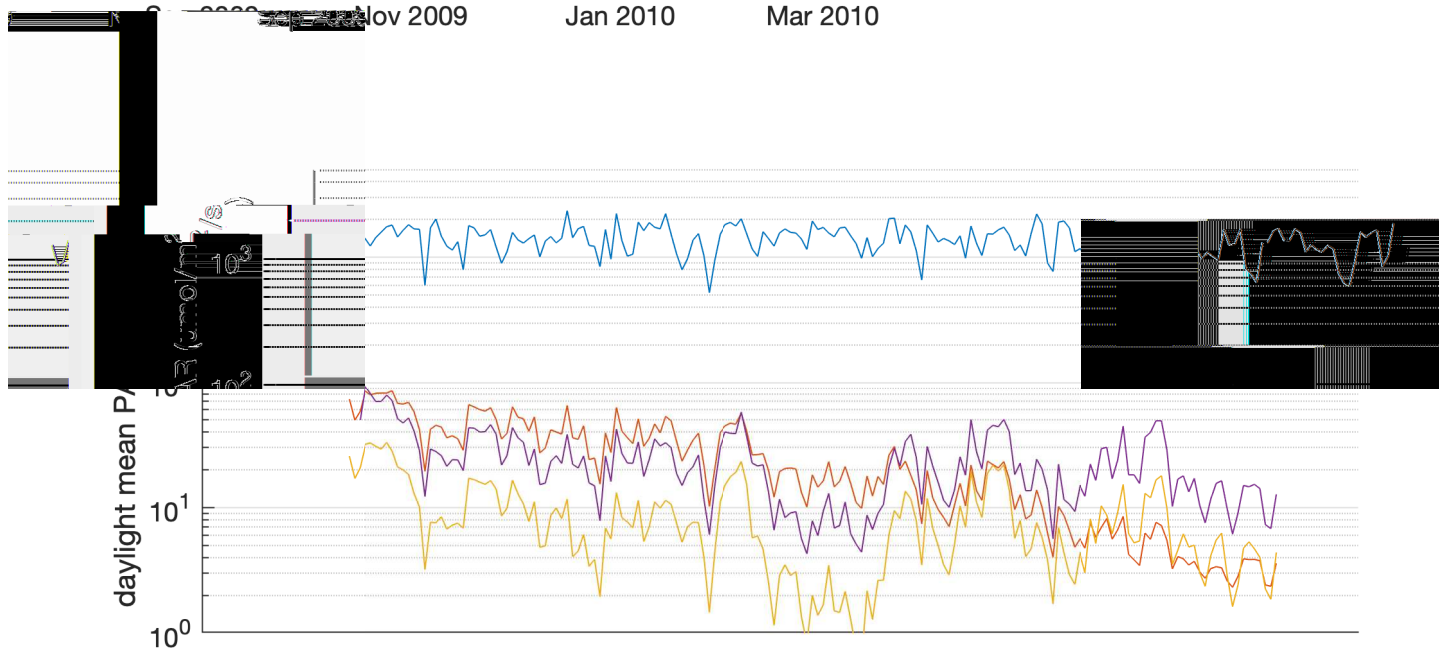
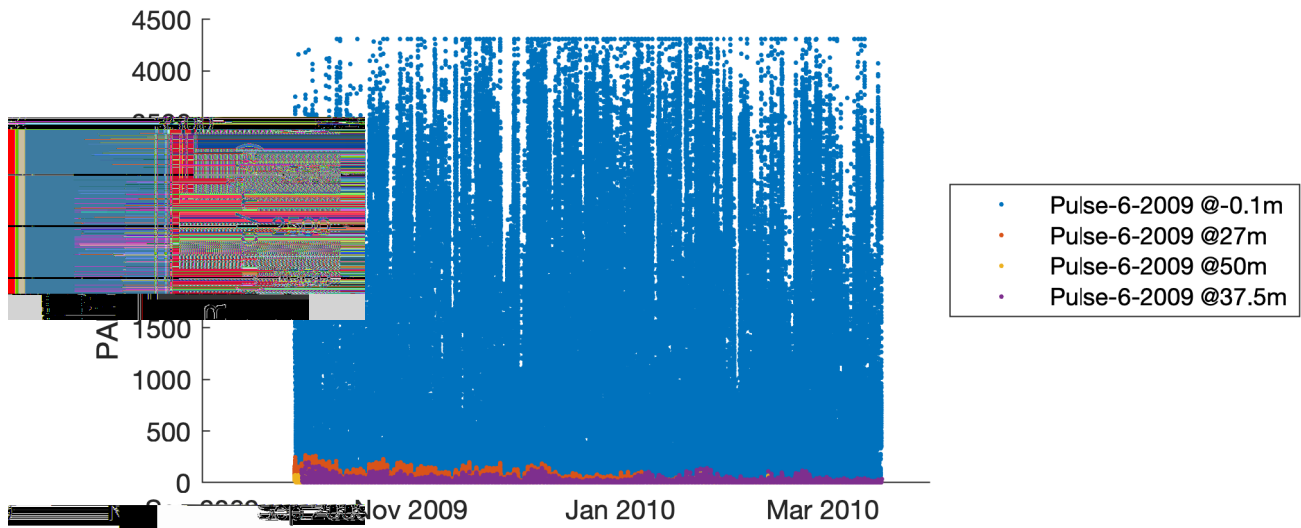
The top plots show the all the PAR sensor data.

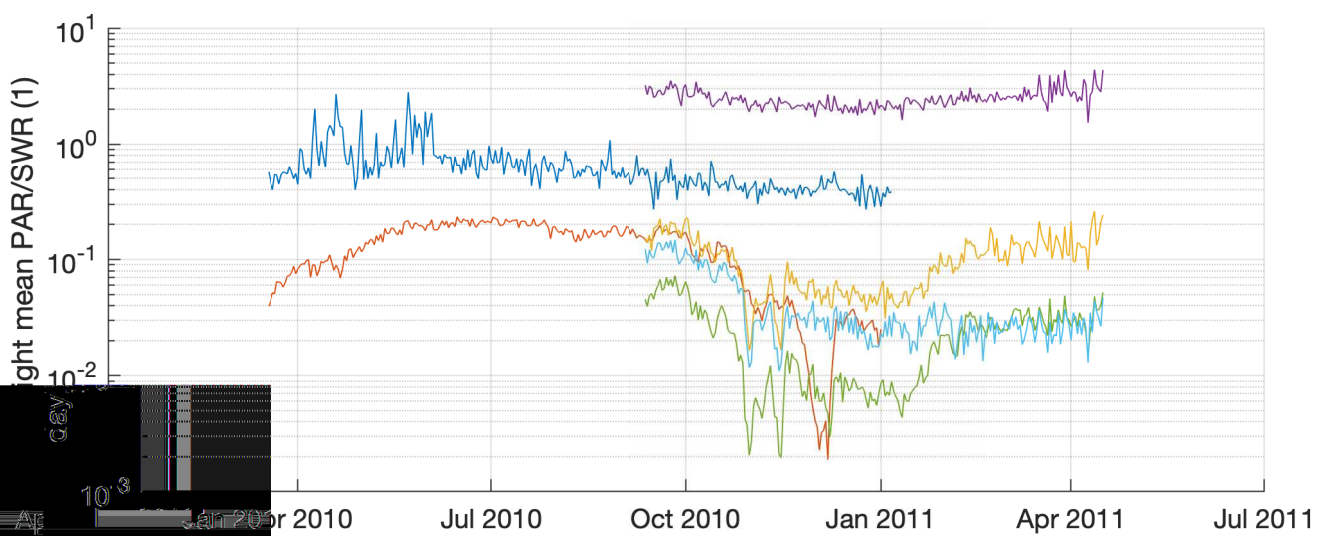
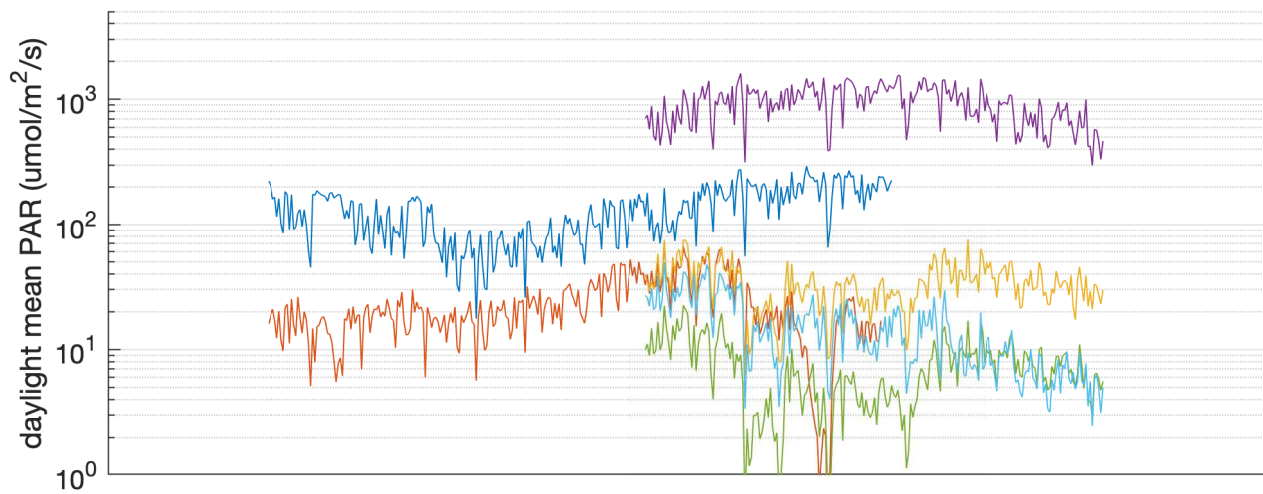
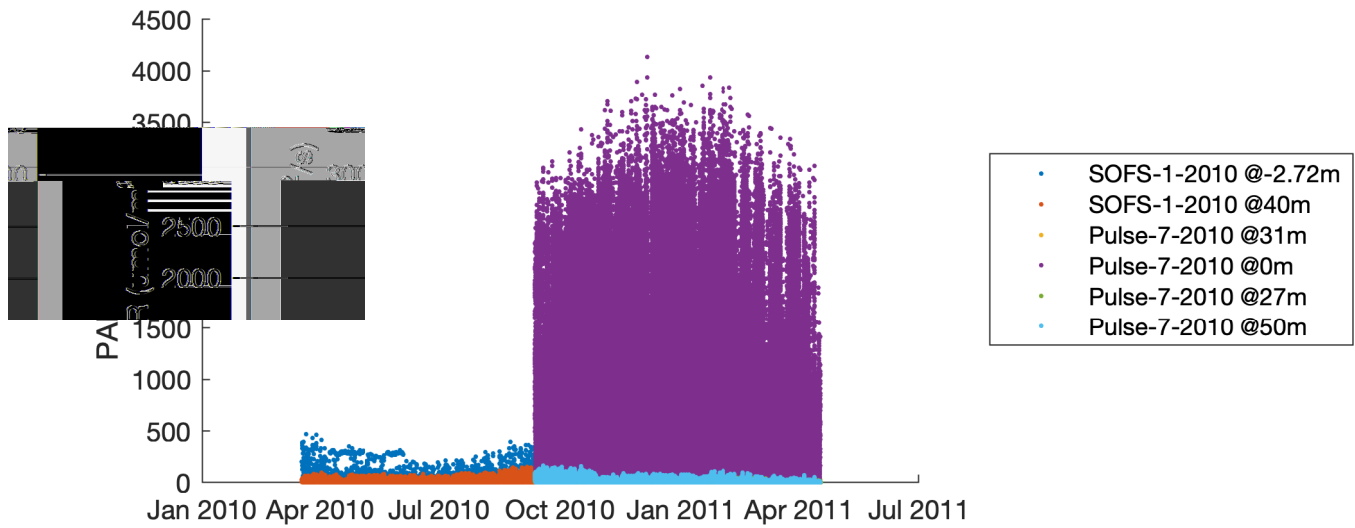
The middle plots show the daylight mean PAR values.

The bottom plots show the ratio of the daylight mean PAR values to the daylight mean ocean surface shortwave values

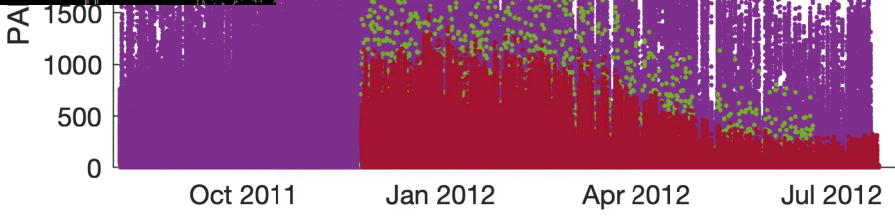
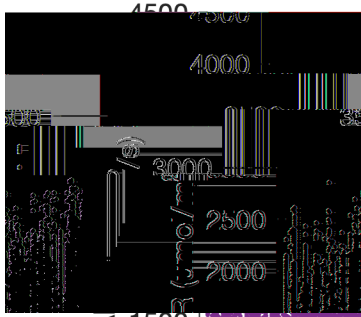
For surface PAR sensors the ratios in the bottom plots should be 1; departures from 1 are ~30-50% and indicate the approximate relative accuracies of the sensors, including differences in light collection by spherical and flat sensors. For both surface and deep sensors this ratio should be invariant with time. The observed temporal drifts in this ratio provide an indication of possible problems such as sensitivity changes or fouling.

Celestial seasonal cycles are expected at the surface, with attenuation of both the mean signal and its seasonality expected at depth.

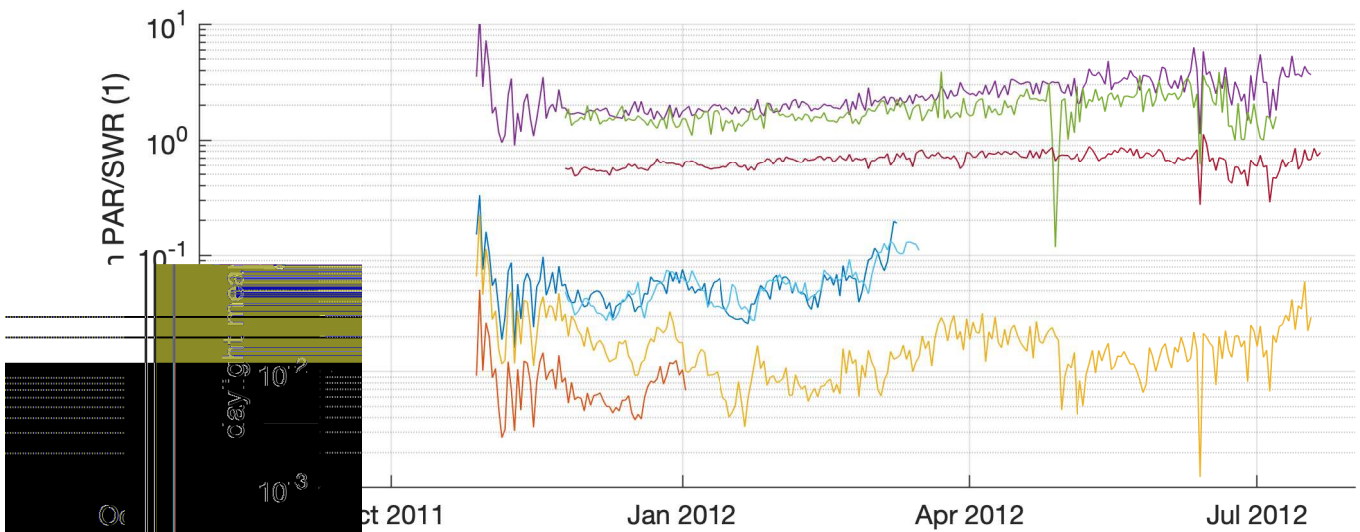
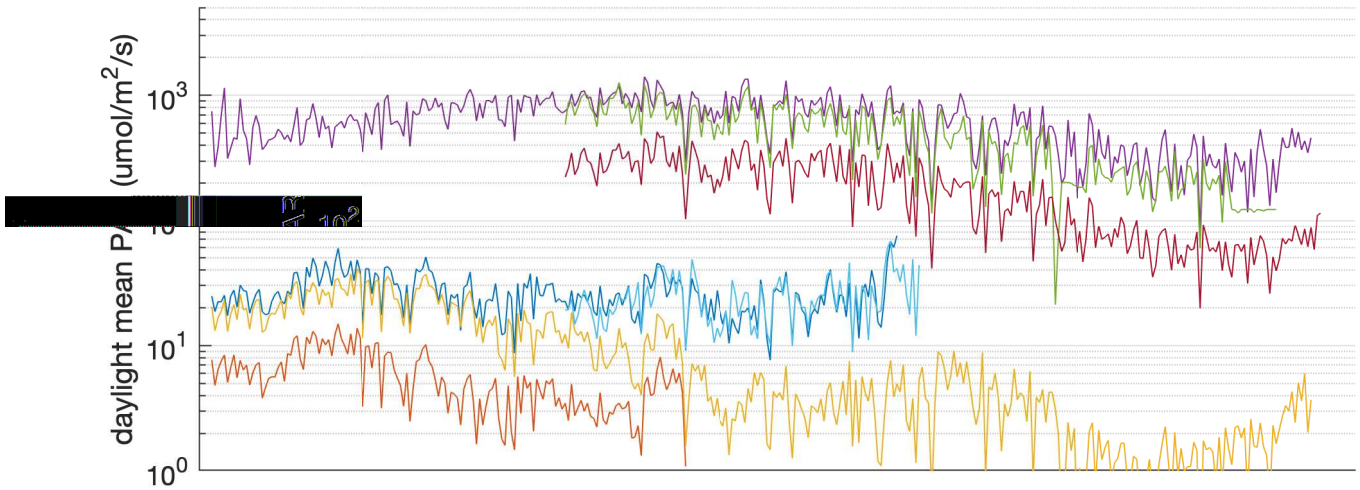


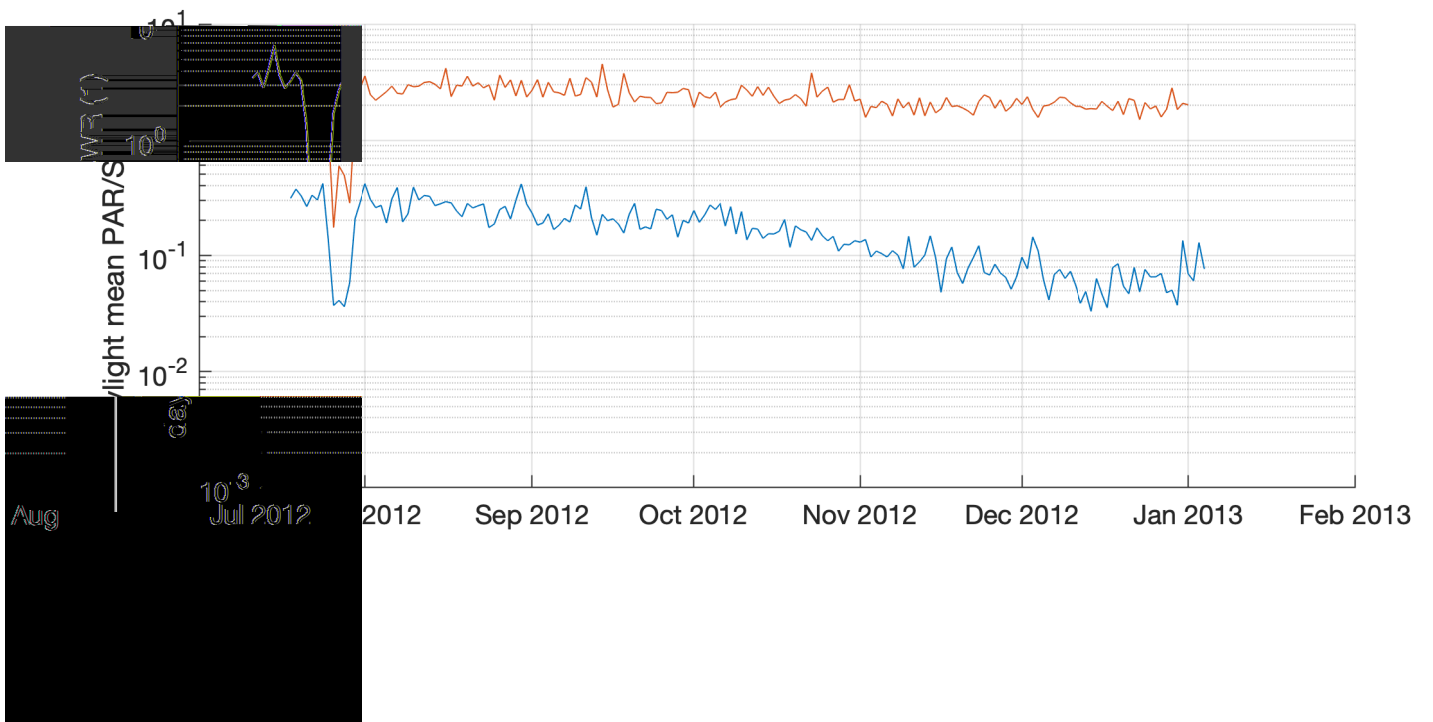
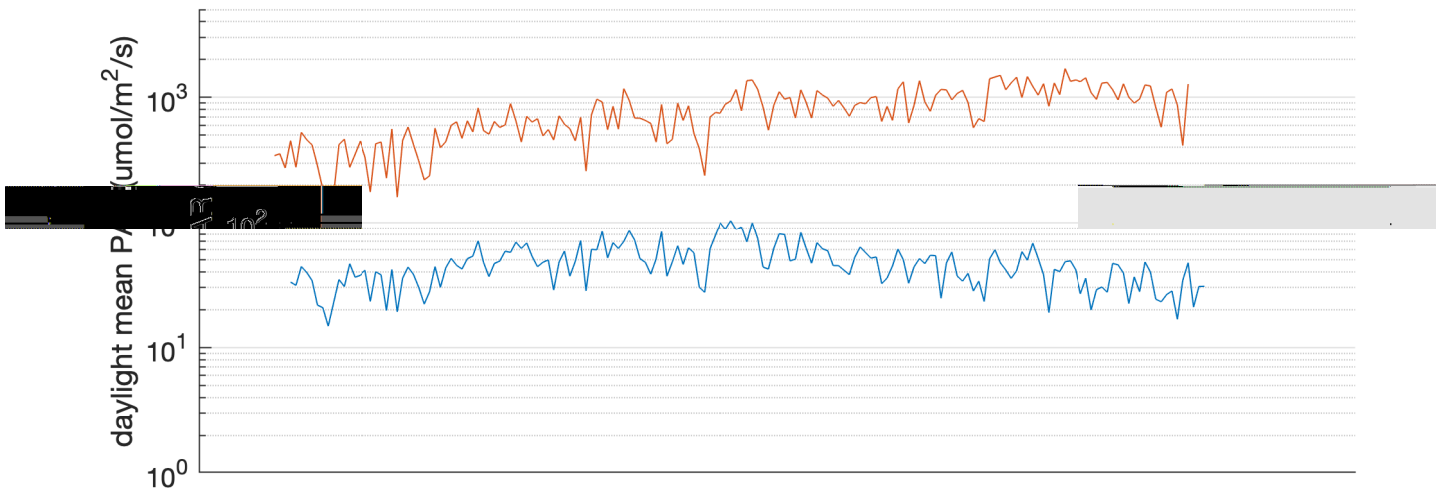
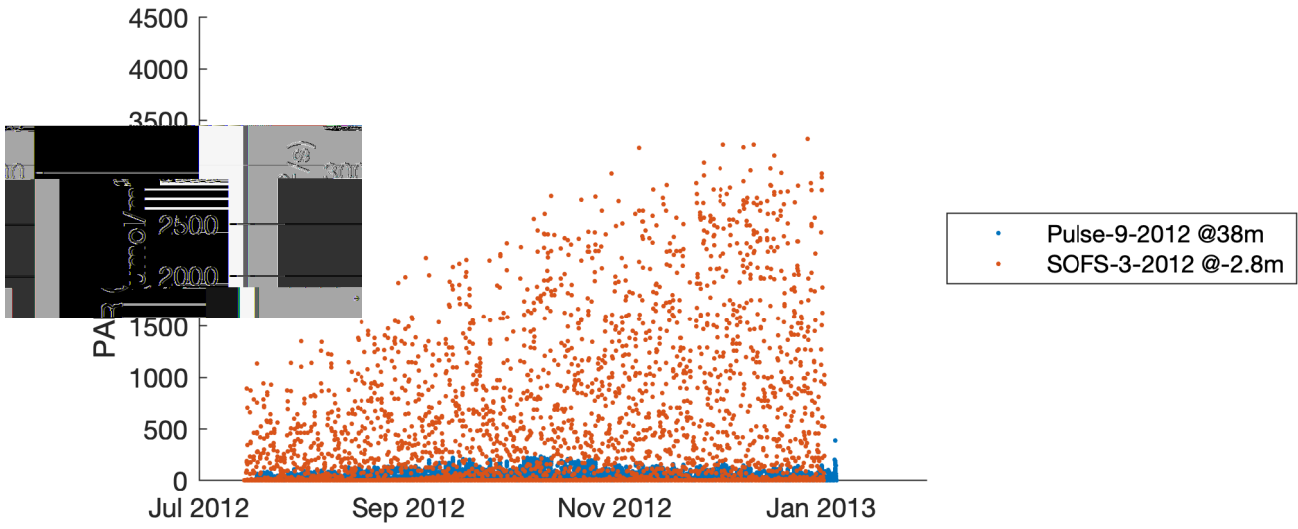


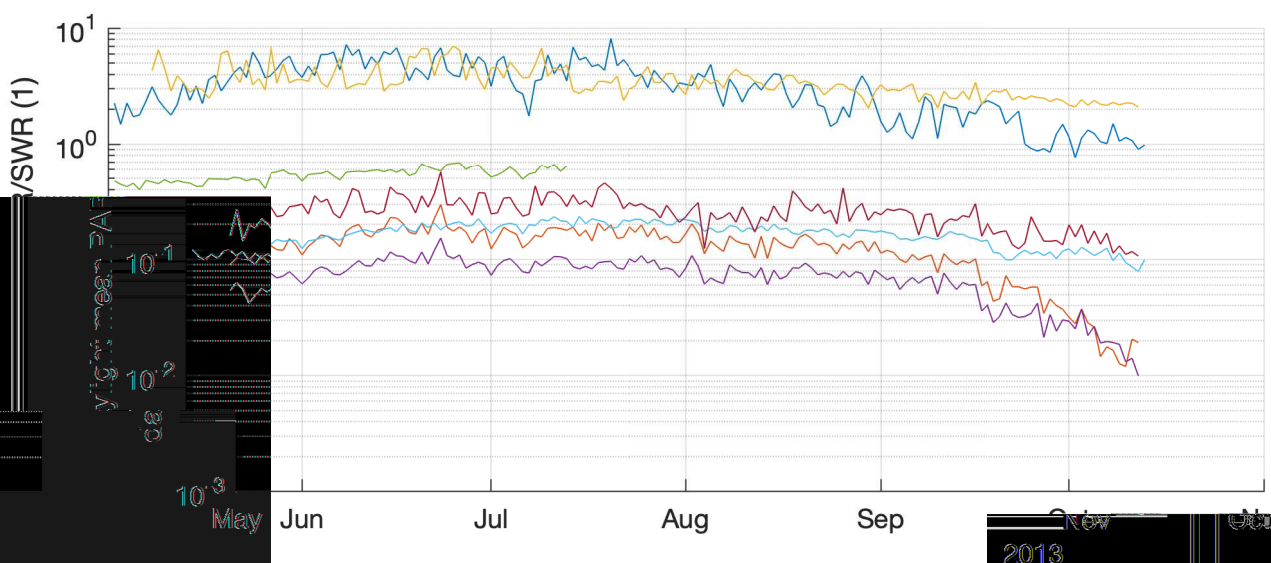
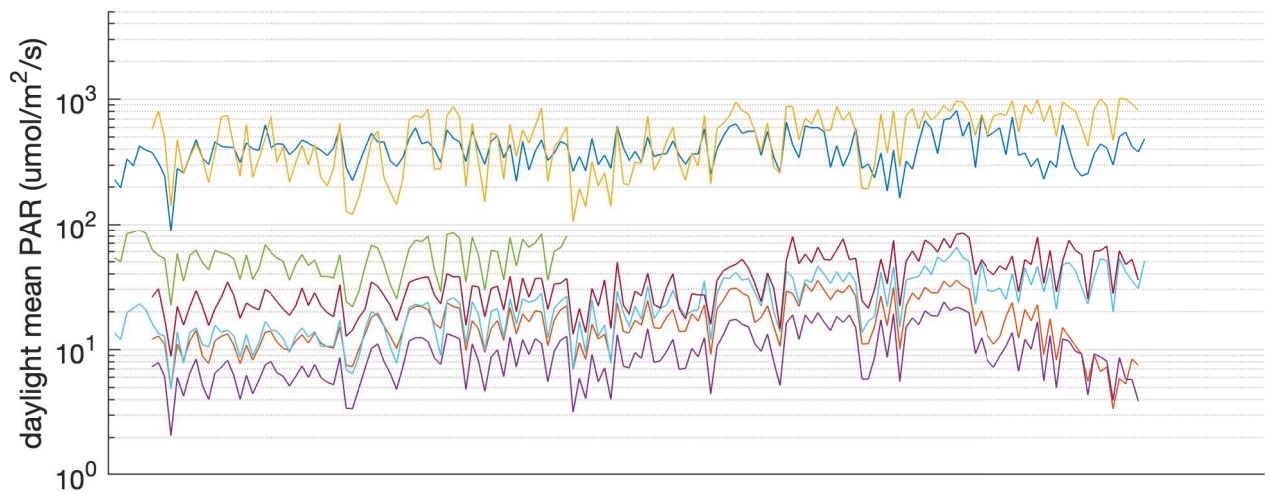
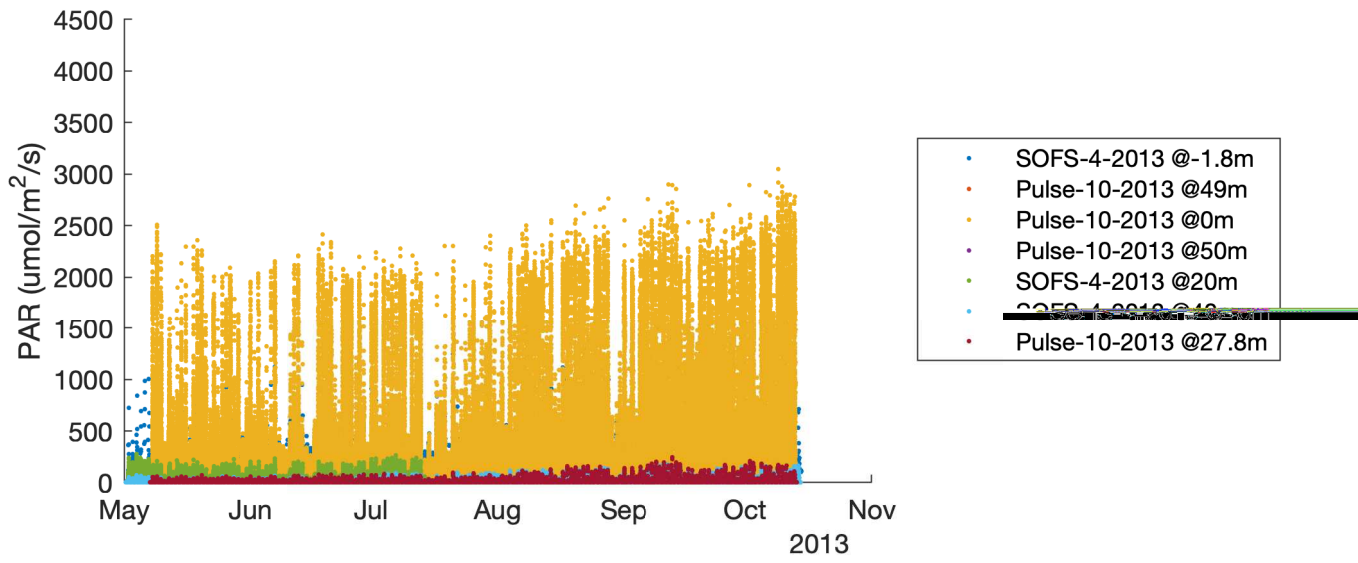


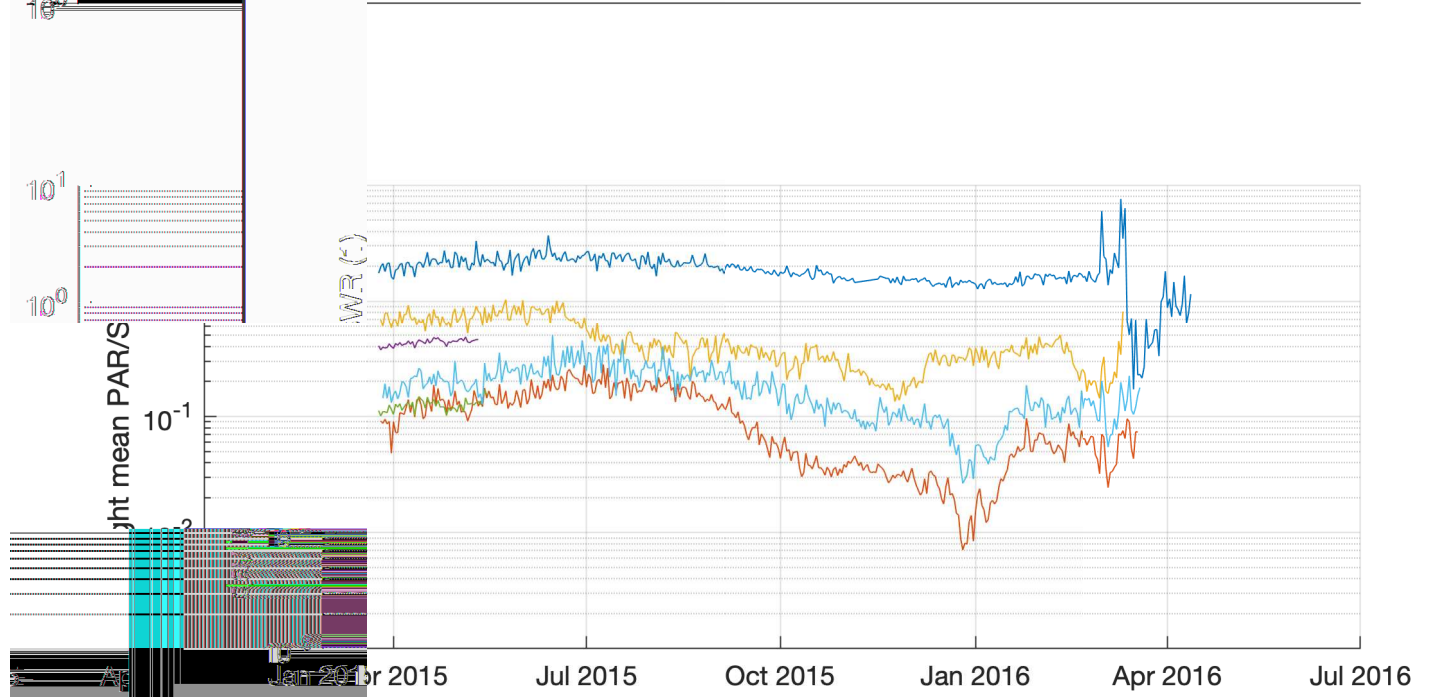
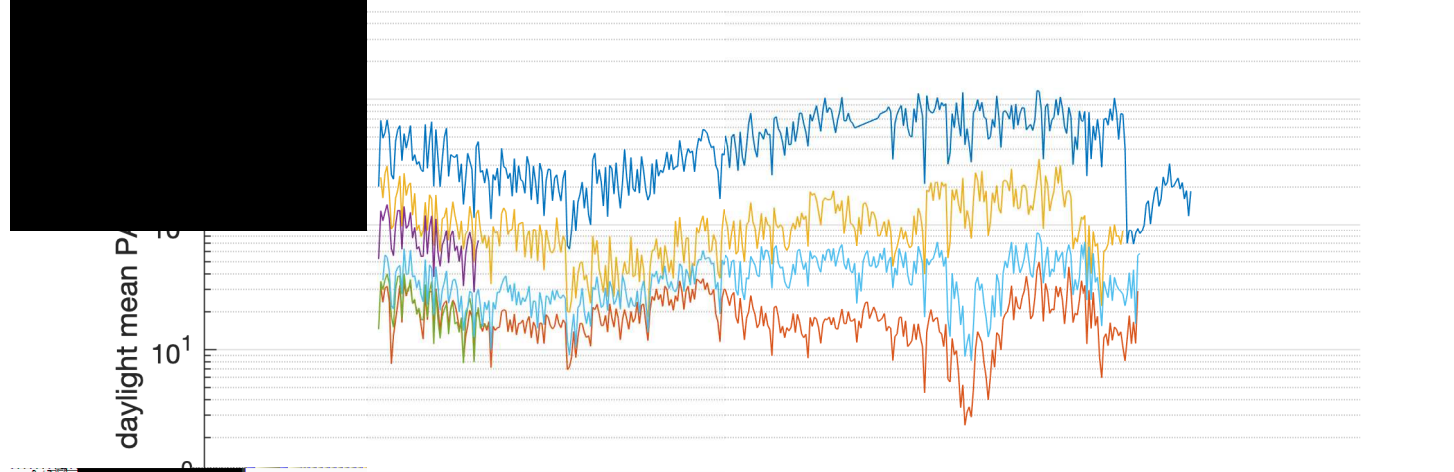
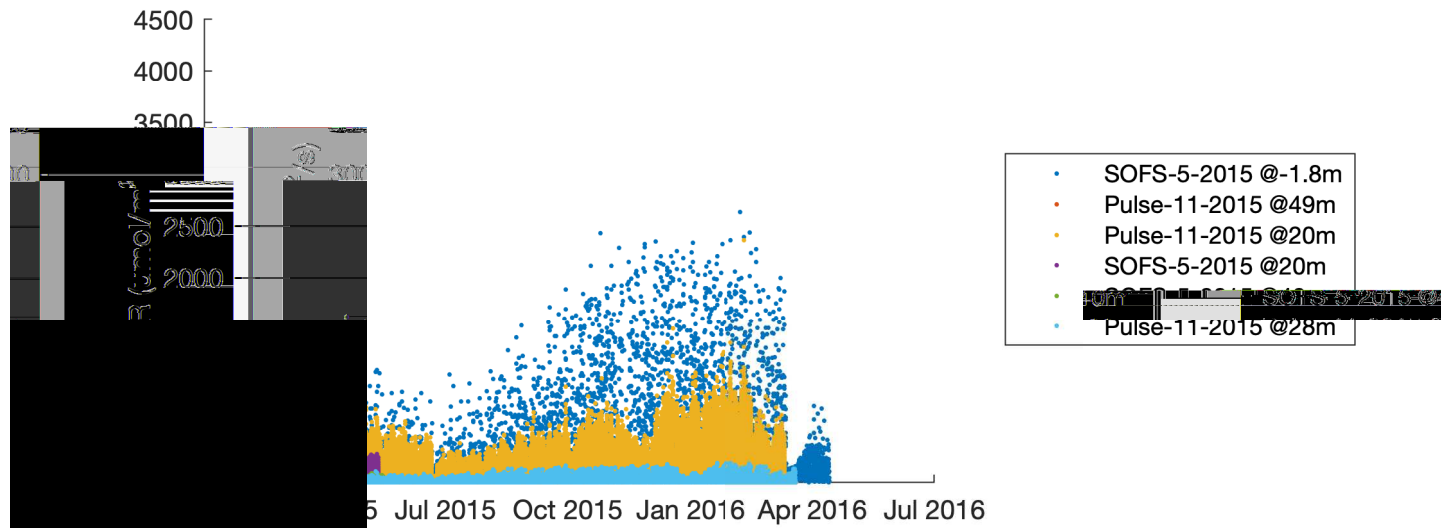


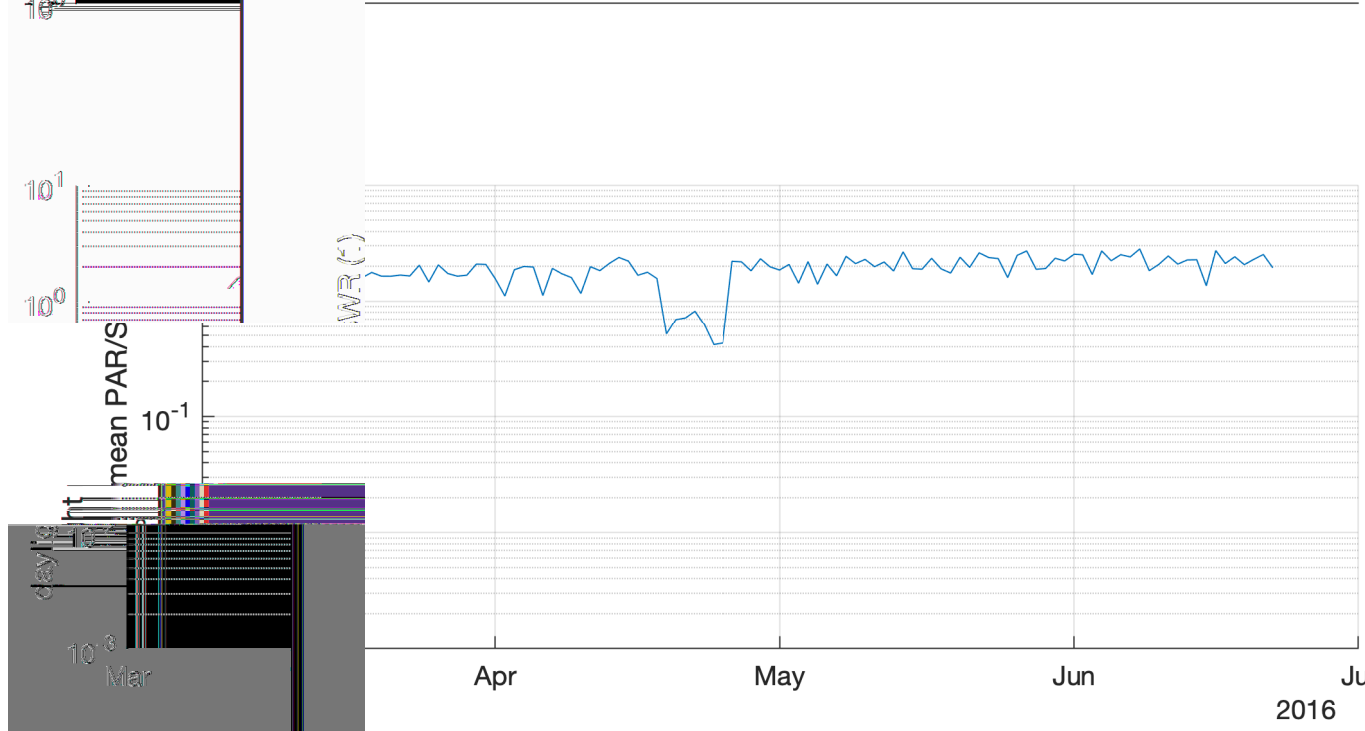
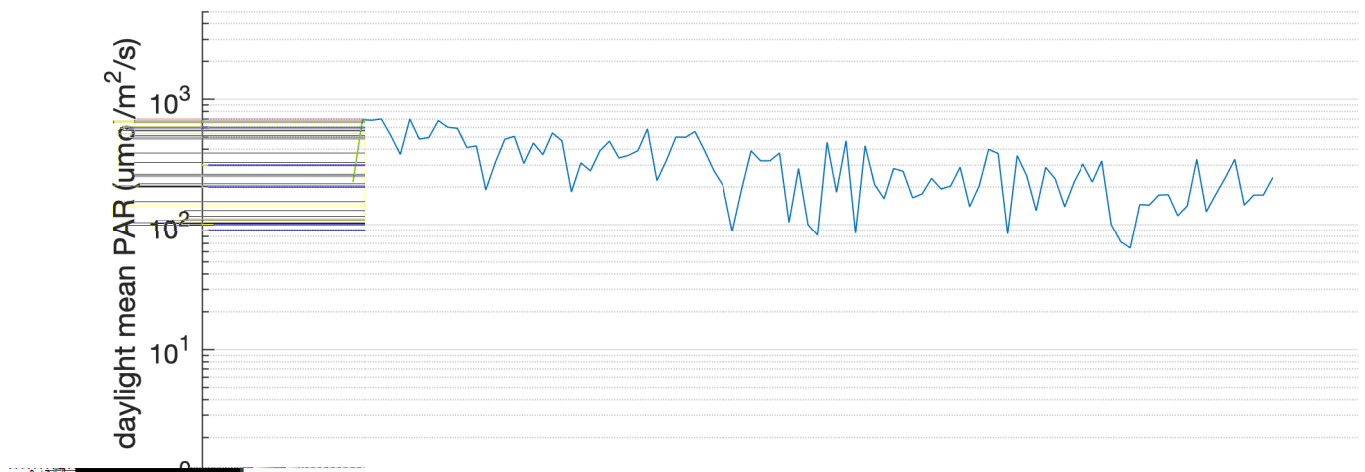
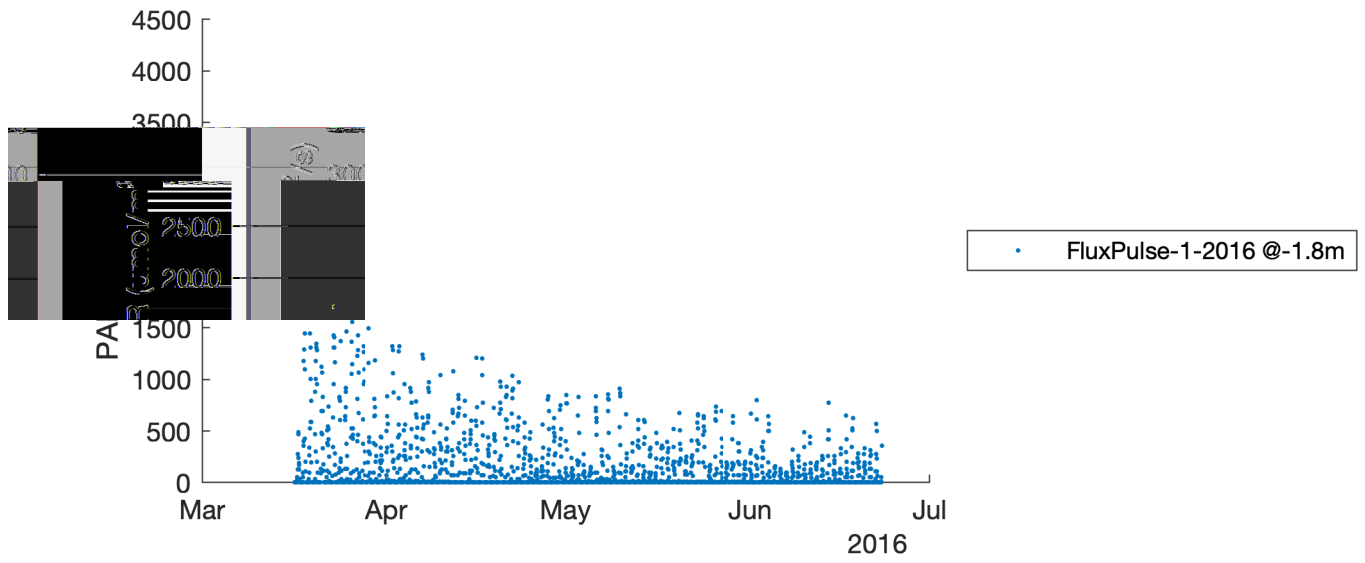
- Pulse-8-2011 @33.8m
- Pulse-8-2011 @50m
- Pulse-8-2011 @27m
- Pulse-8-2011 @10m
- SOFS-2-2011 @10m

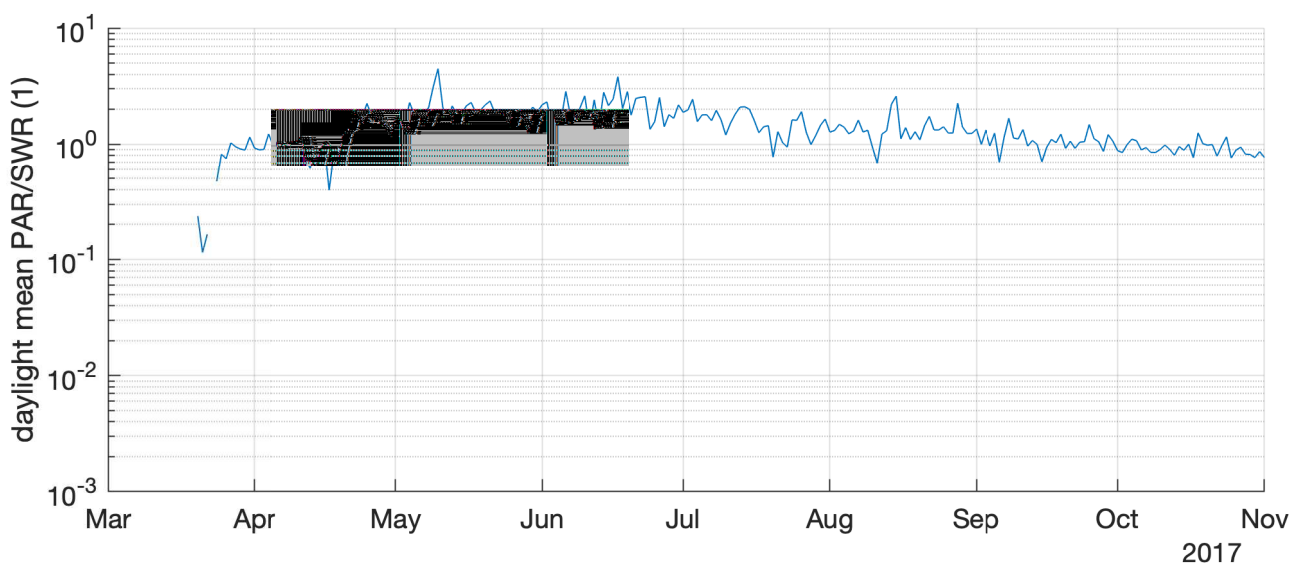
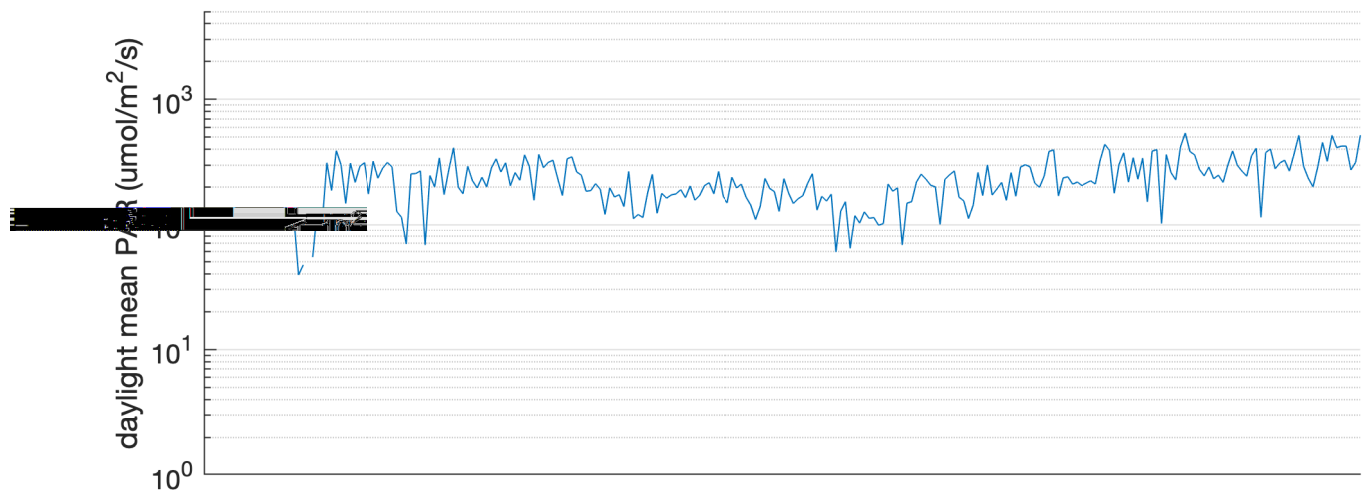
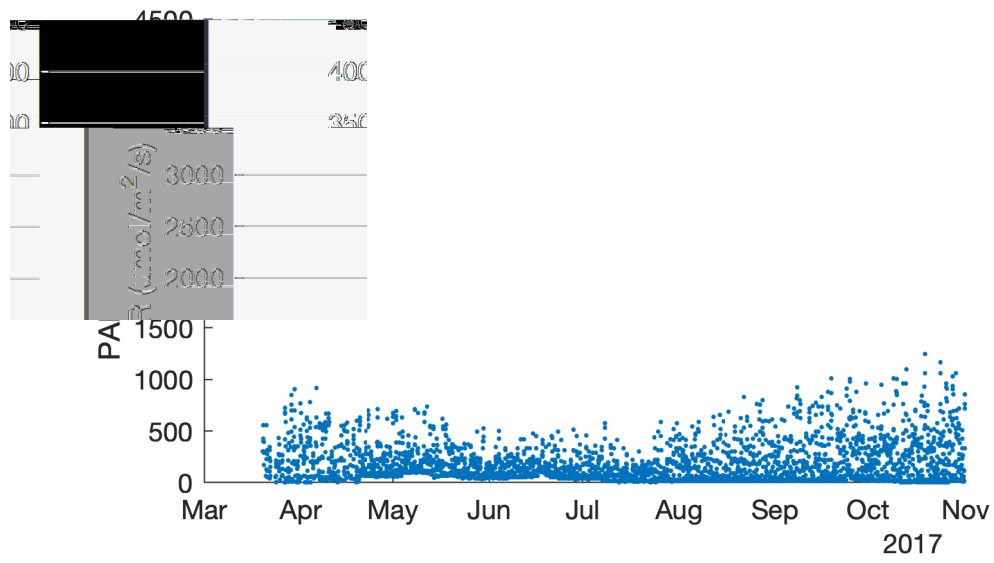


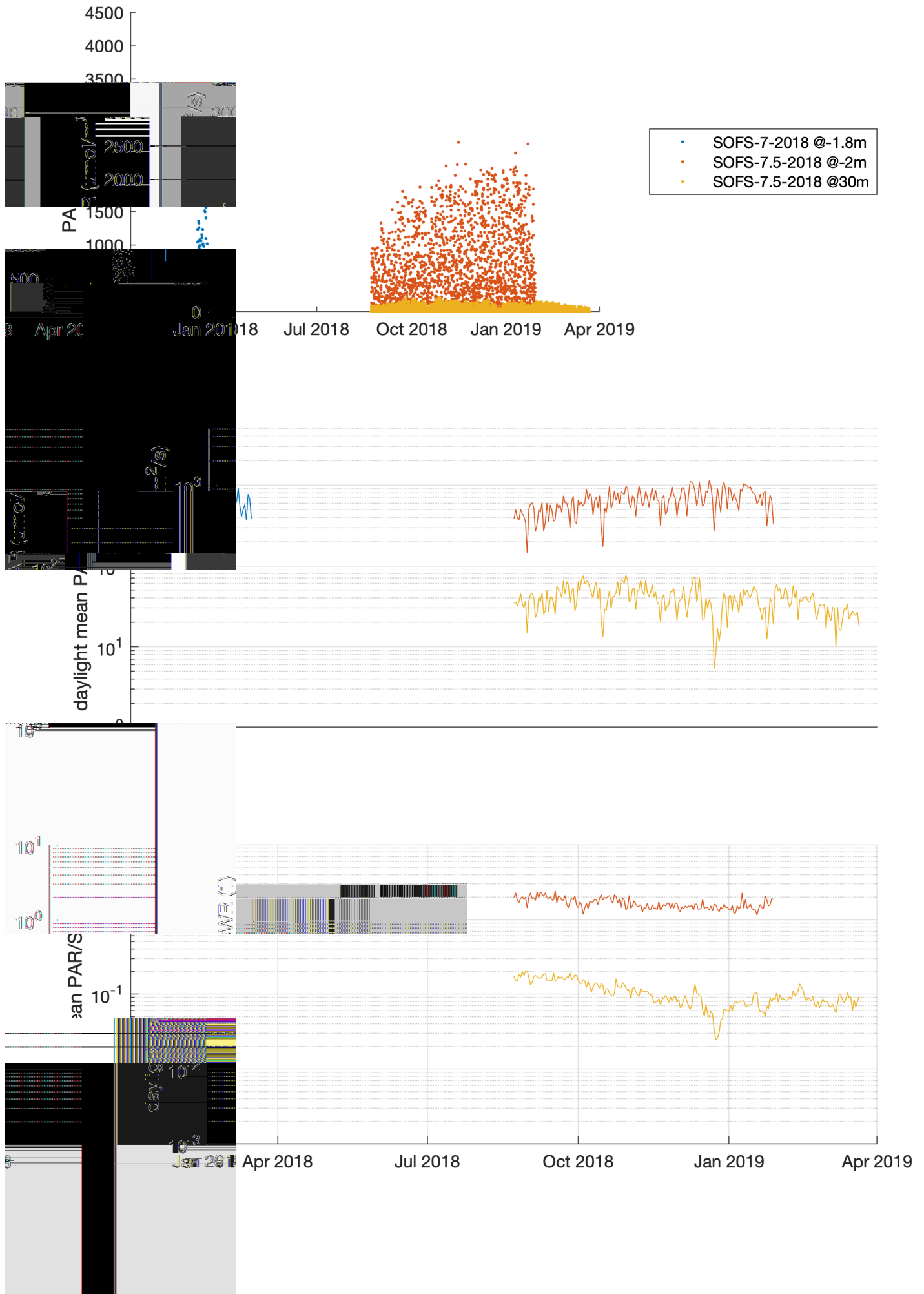












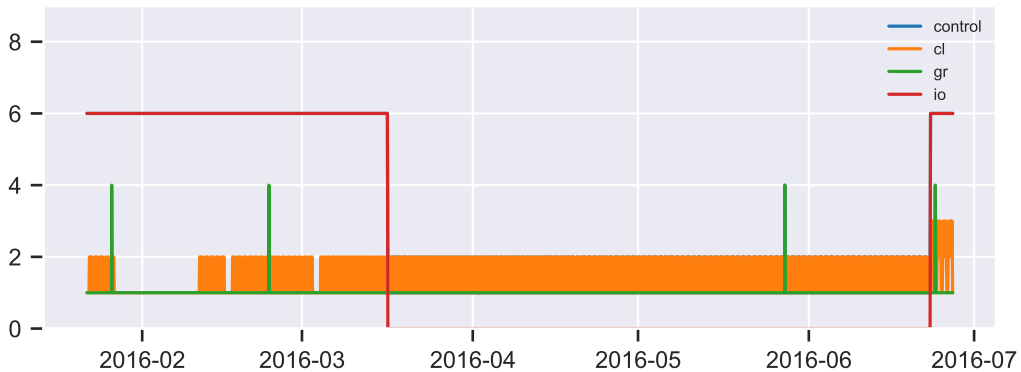
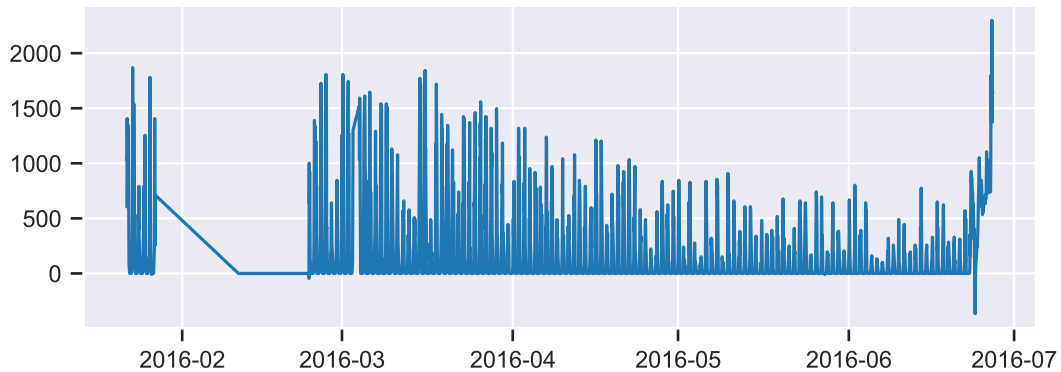
## 8 QC flag plots

Plots of data, top panel, RAW data, bottom QC flags,

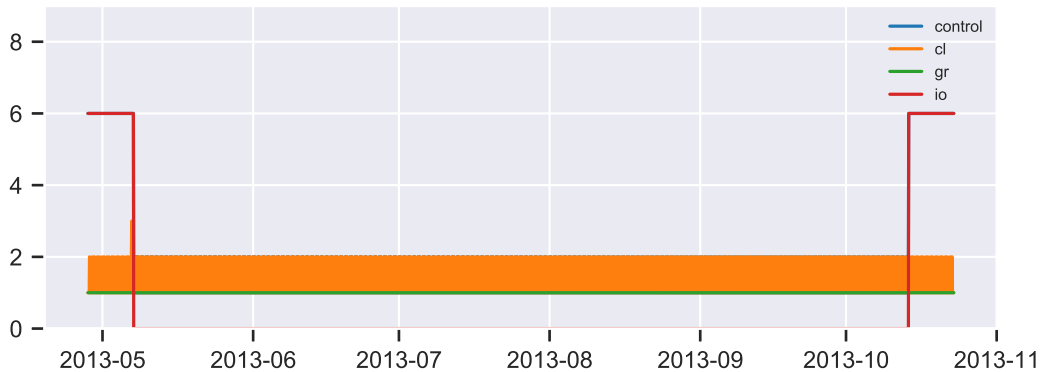
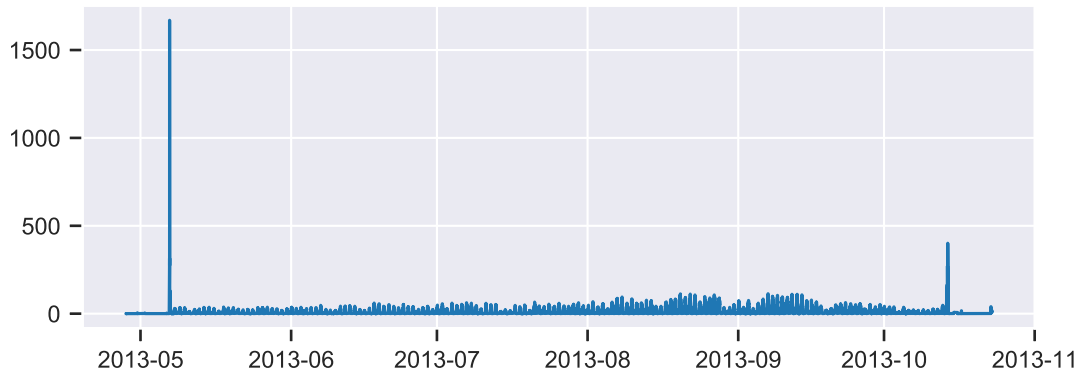
- control – overall QC flag (max of all flags)
- cl – climatology test result
- io – in/out of water flag
- gr – global range test result
- man – manual QC flag



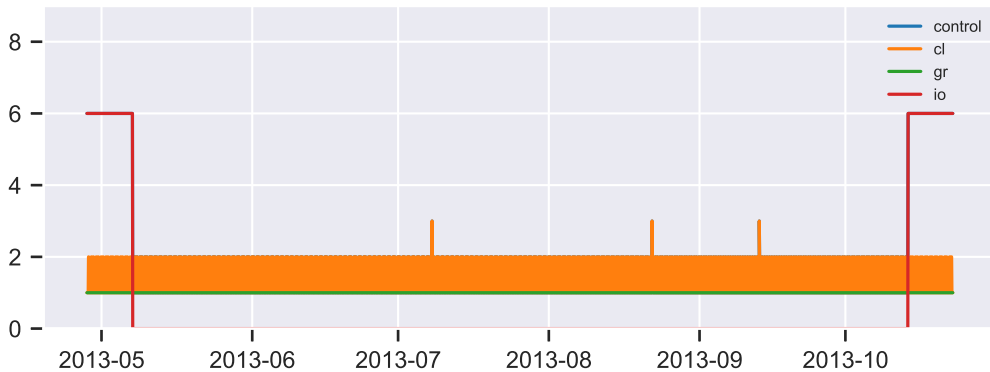
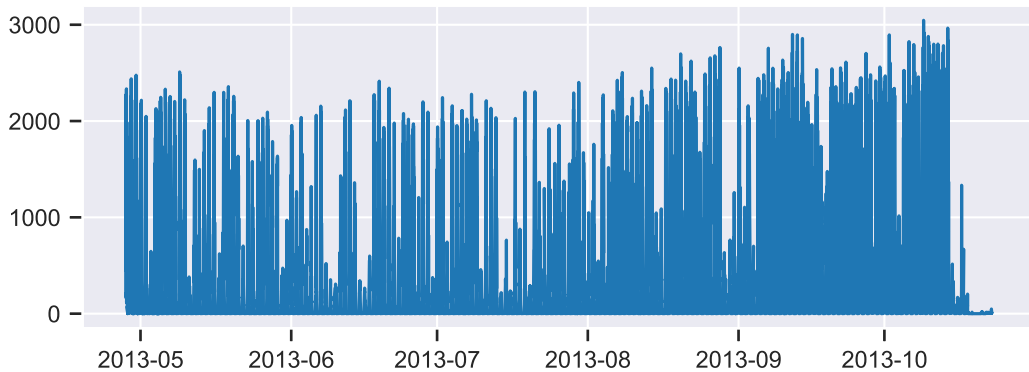
FluxPulse-1-2016 - LI-190SA:Q40966 @ -1.8



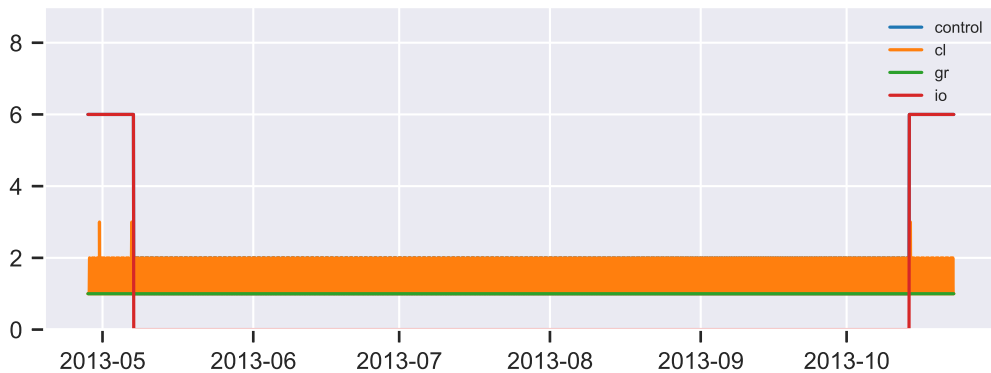
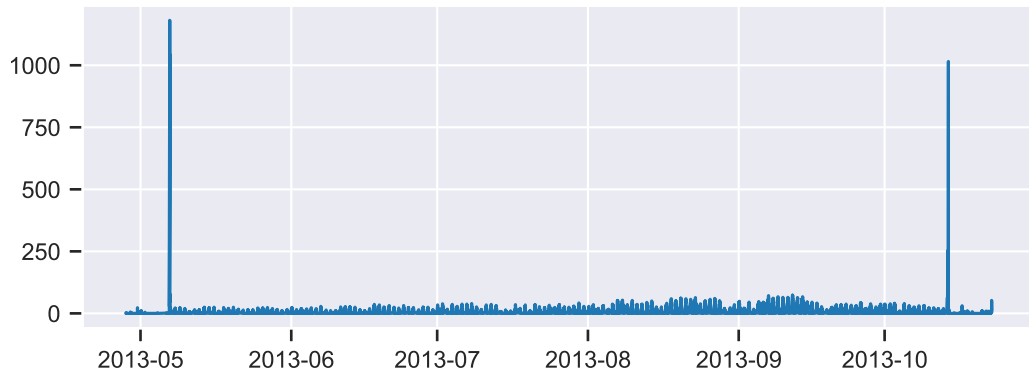
Pulse-10-2013 - DEFI-L:082V023 @ 49.0



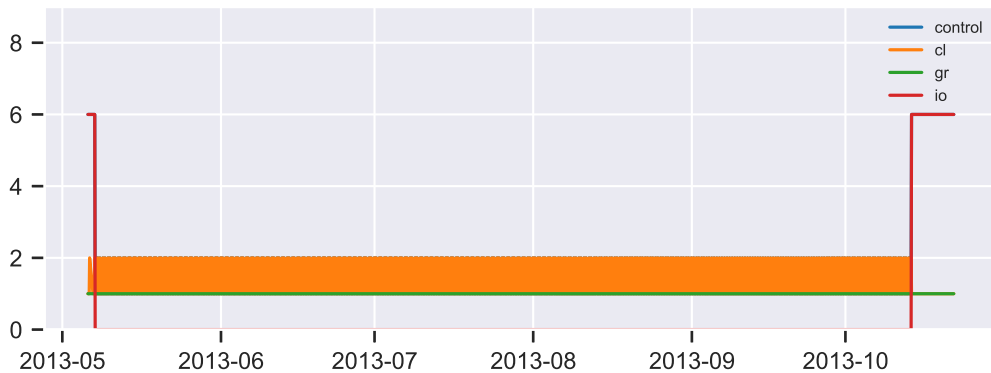
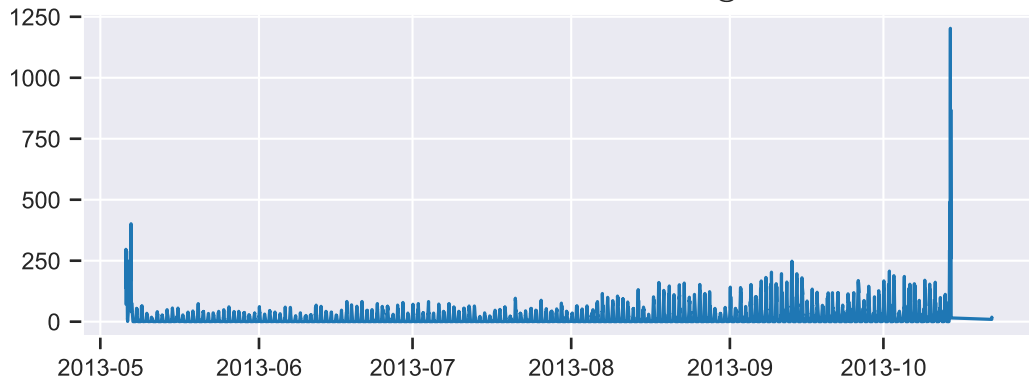
Pulse-10-2013 - MDS-MKVL:200341 @ 0.0



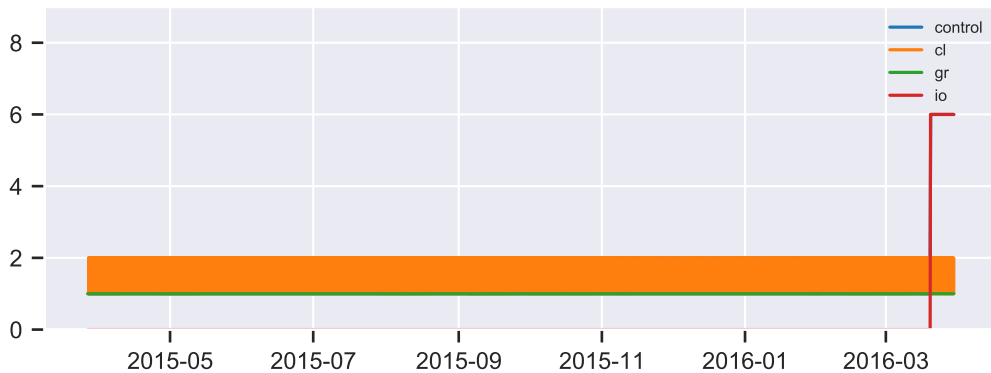
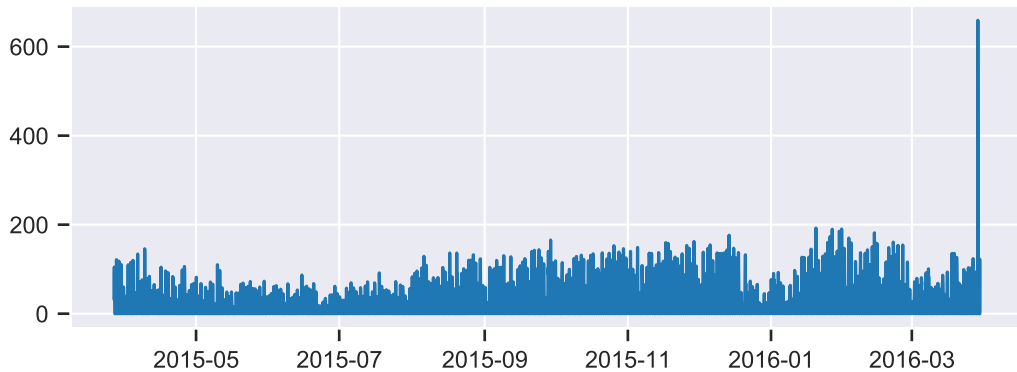
Pulse-10-2013 - MDS-MKVL:200665 @ 50.0



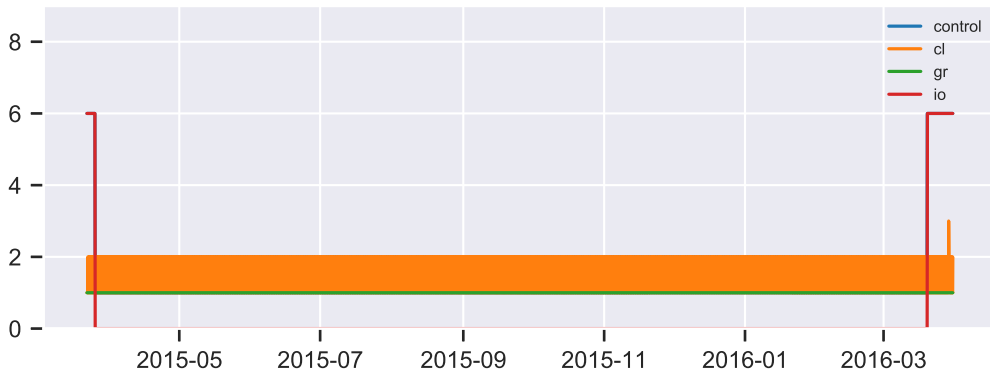
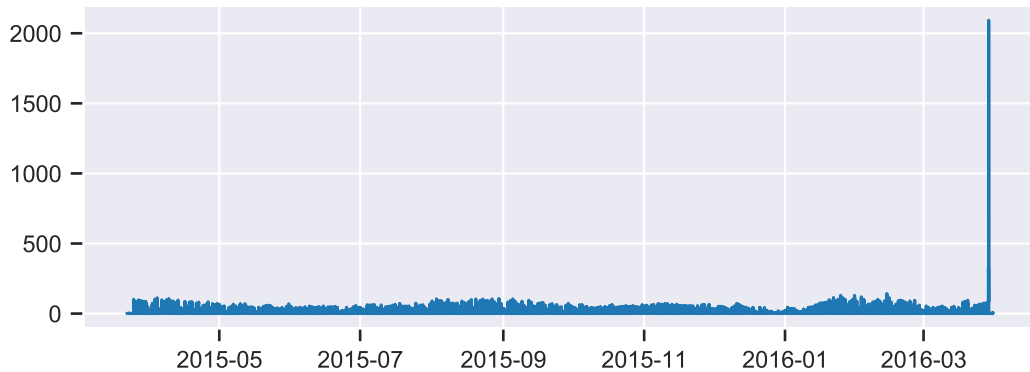
Pulse-10-2013 - ECO-PARS:PARS-134 @ 27.8



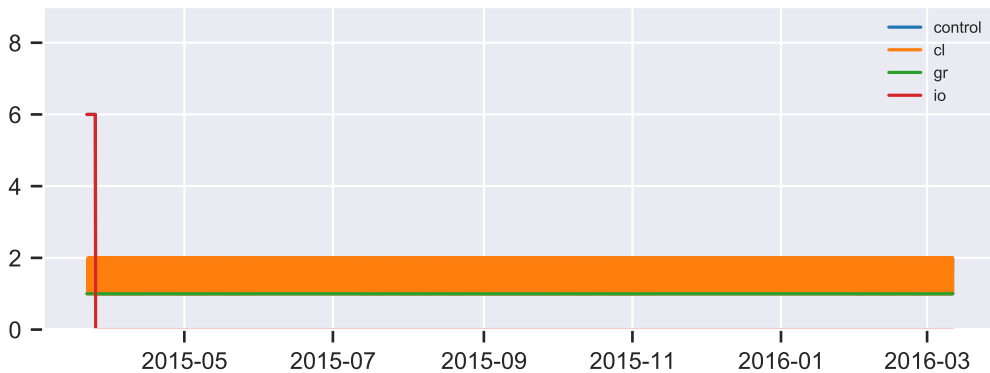
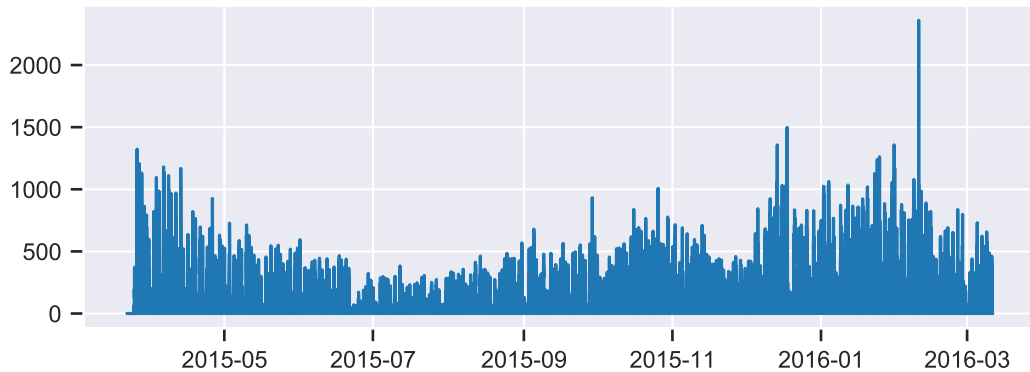
Pulse-11-2015 - ECO-PAR:PARS-134 @ 28.0



Pulse-11-2015 - DEFI-L:082V022 @ 49.0

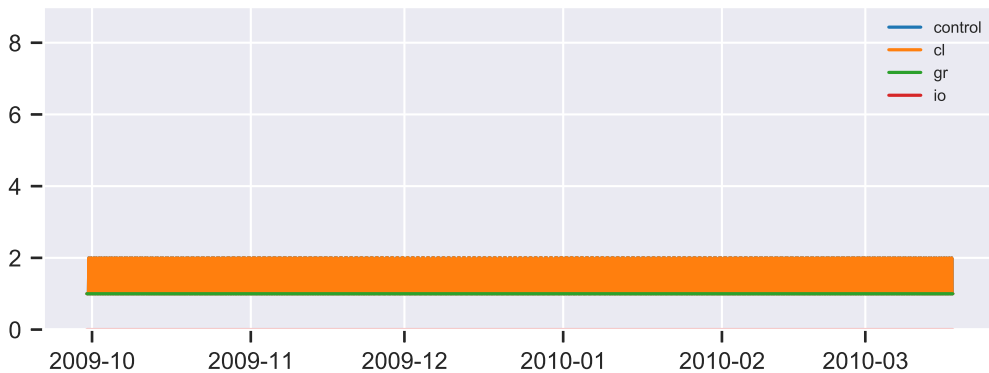
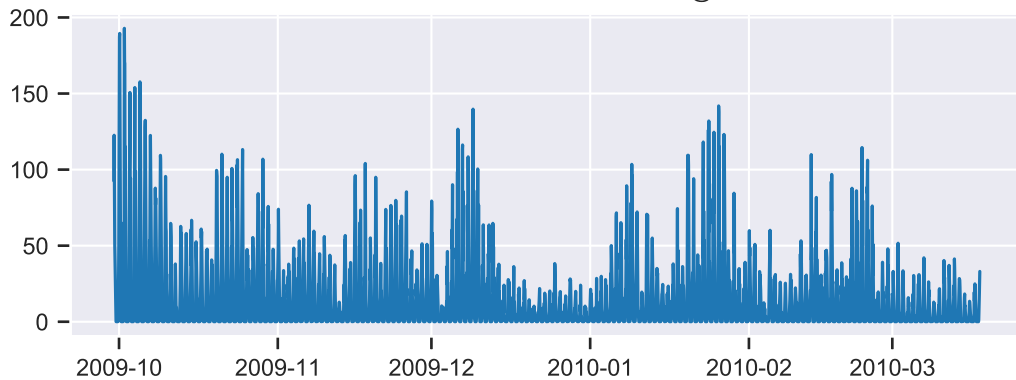


Pulse-11-2015 - MDS-MKVL:200665 @ 20.0

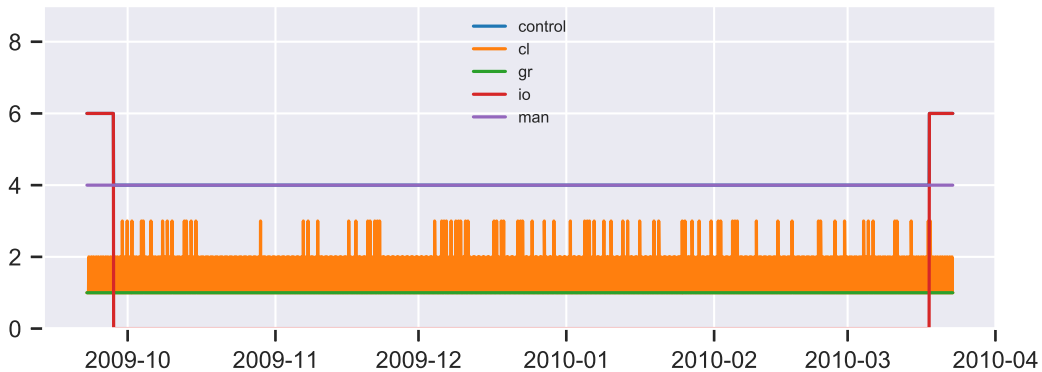
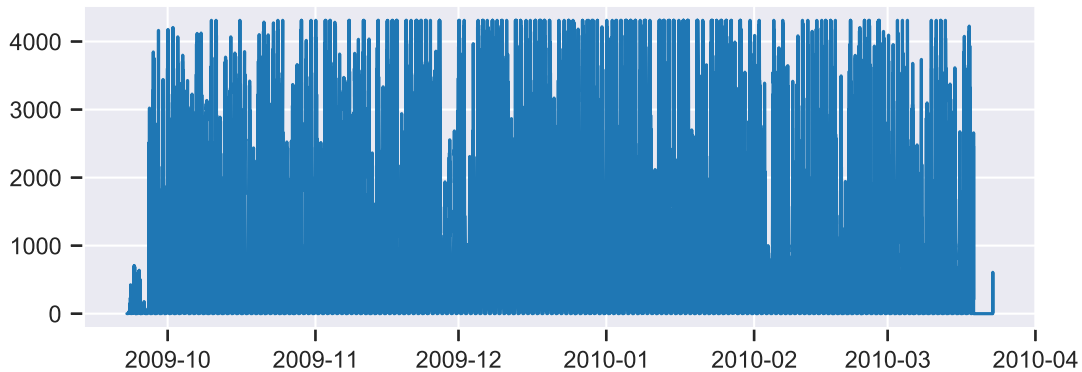




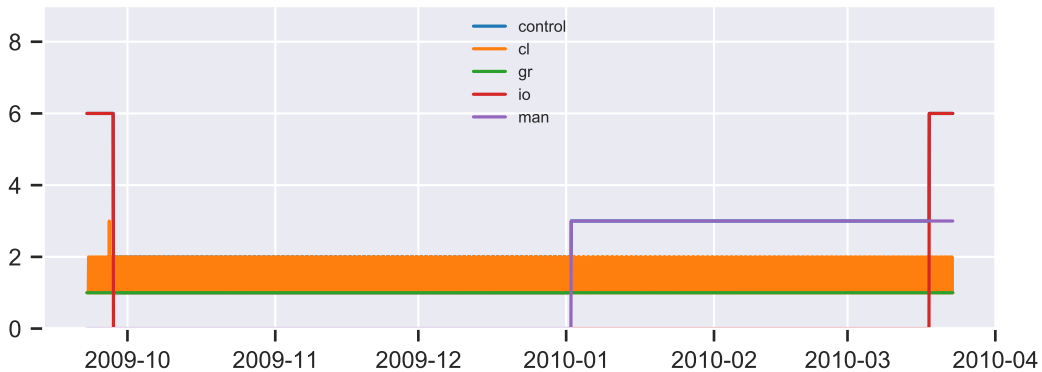
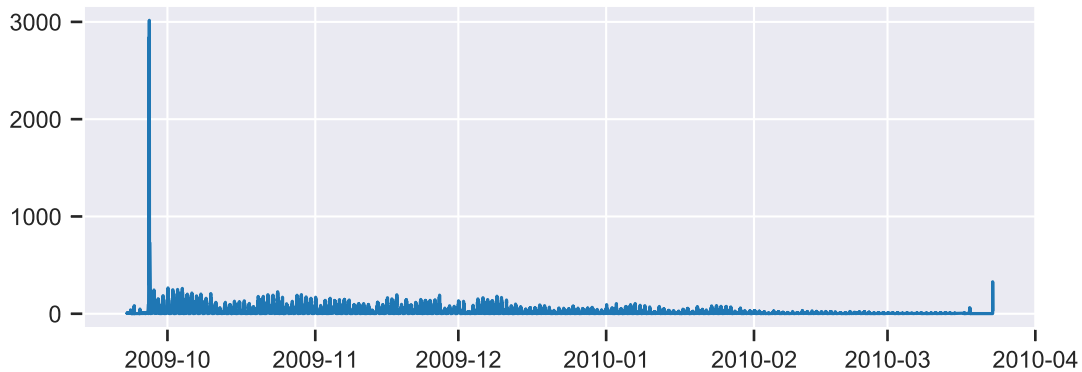
Pulse-6-2009 - ECO-PAR:PARS-134 @ 37.5



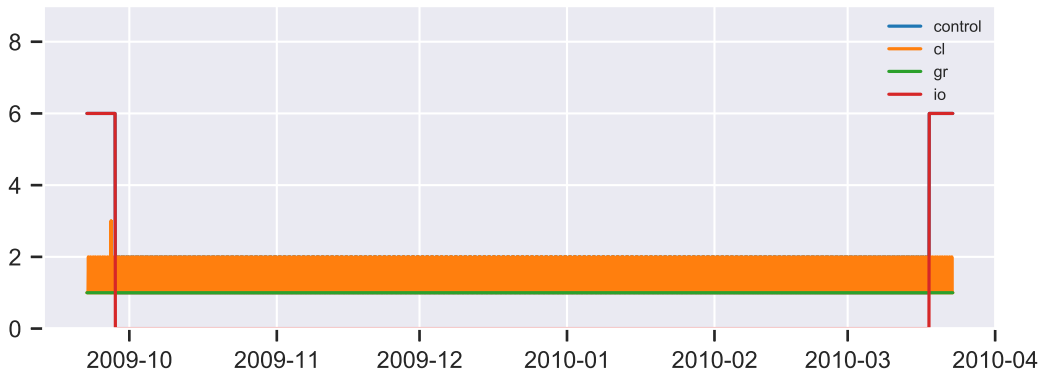
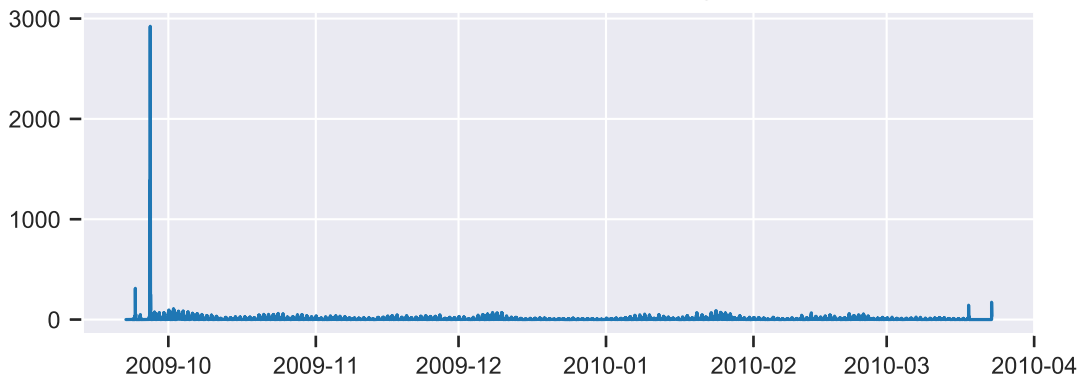
Pulse-6-2009 - MDS-MKVL:200341 @ -0.1



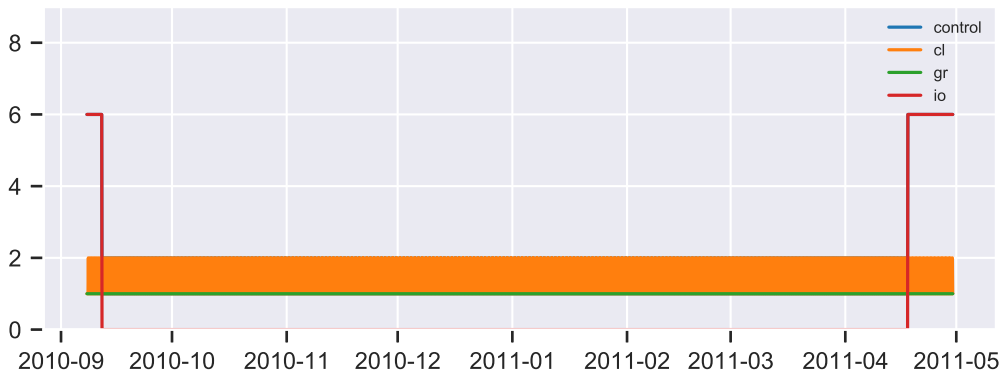
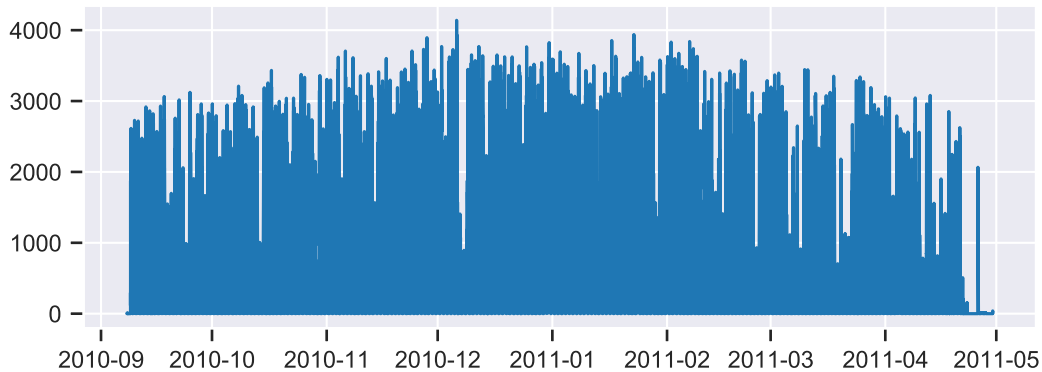
Pulse-6-2009 - MDS-MKVL:200664 @ 27.0



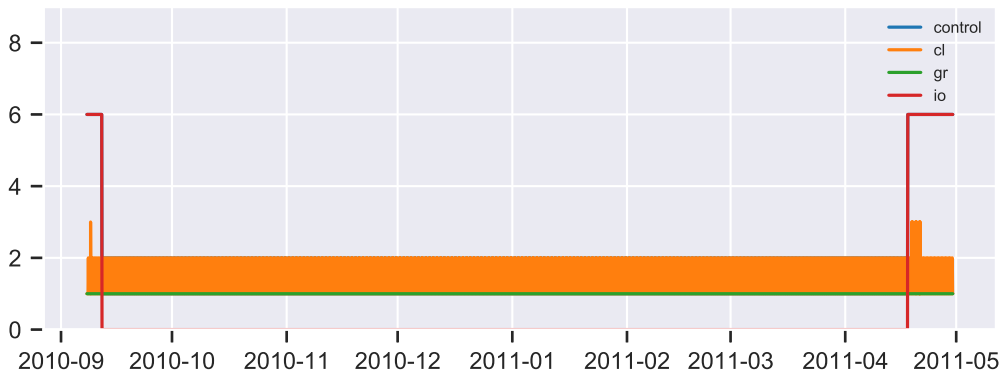
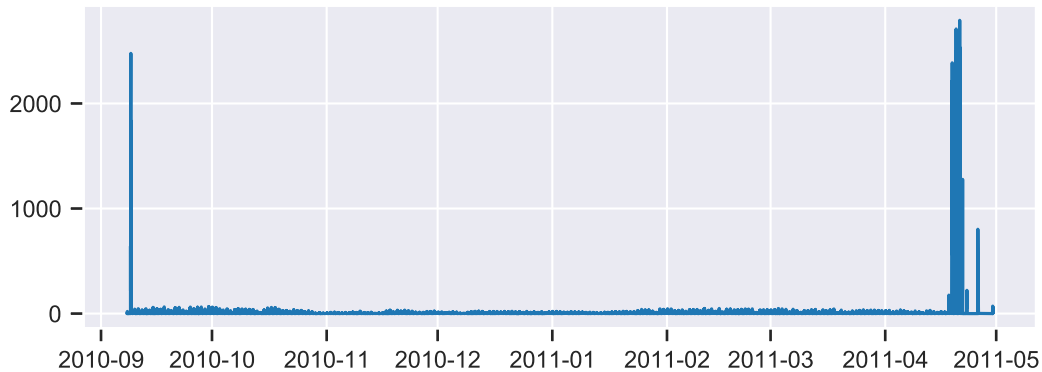
Pulse-6-2009 - MDS-MKVL:200665 @ 50.0



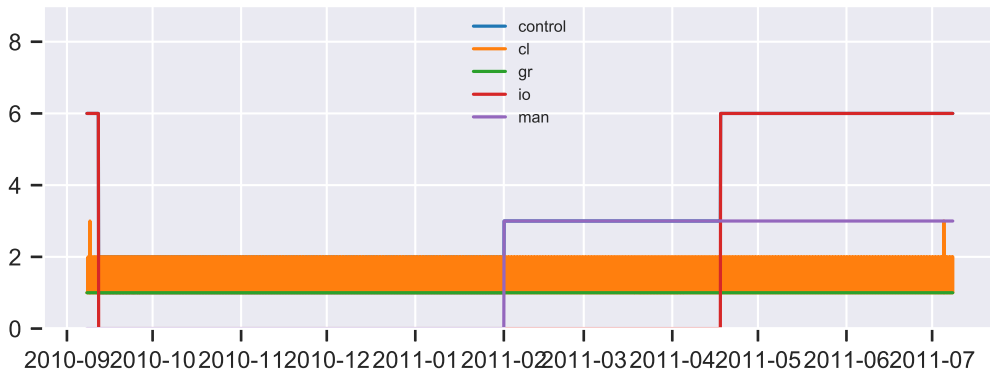
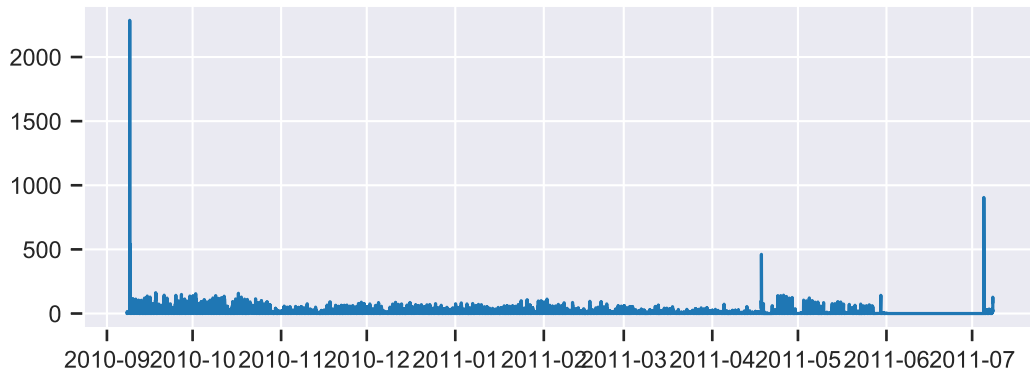
Pulse-7-2010 - MDS-MKVL:200341 @ 0.0



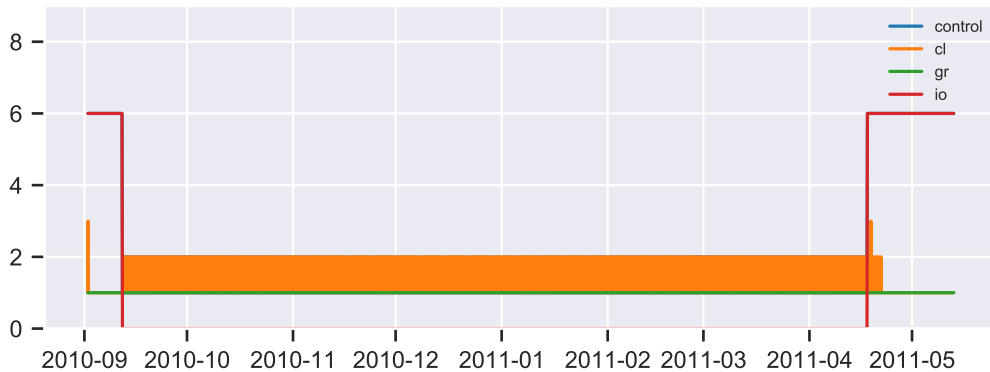
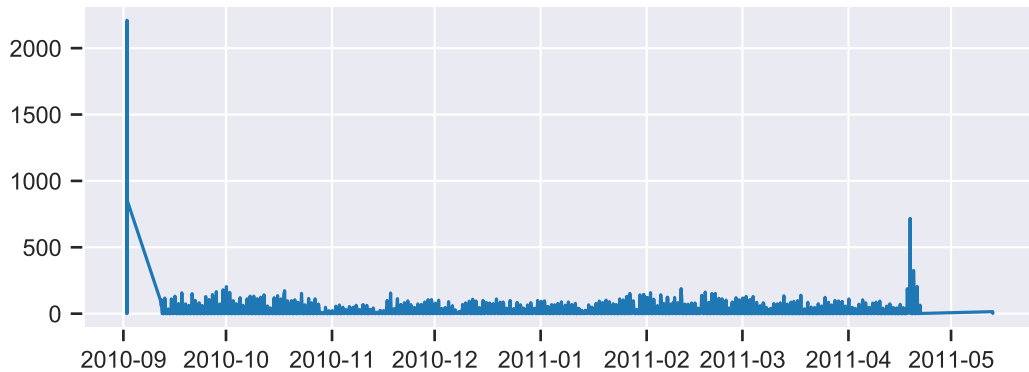
Pulse-7-2010 - MDS-MKVL:200664 @ 27.0



Pulse-7-2010 - MDS-MKVL:200665 @ 50.0

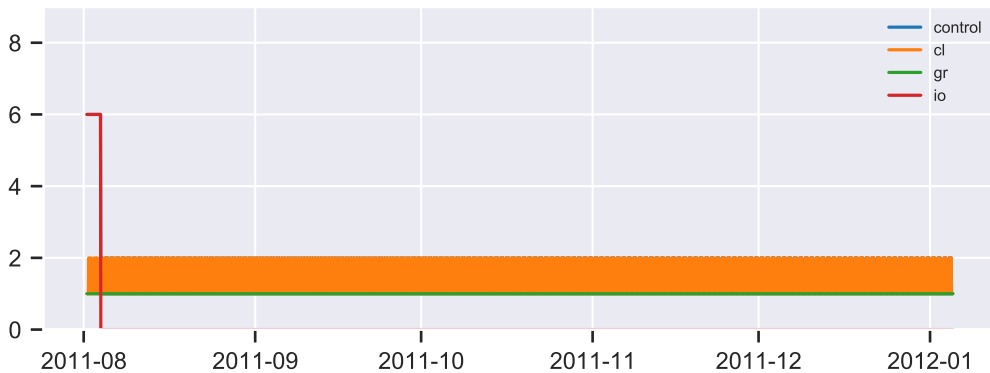
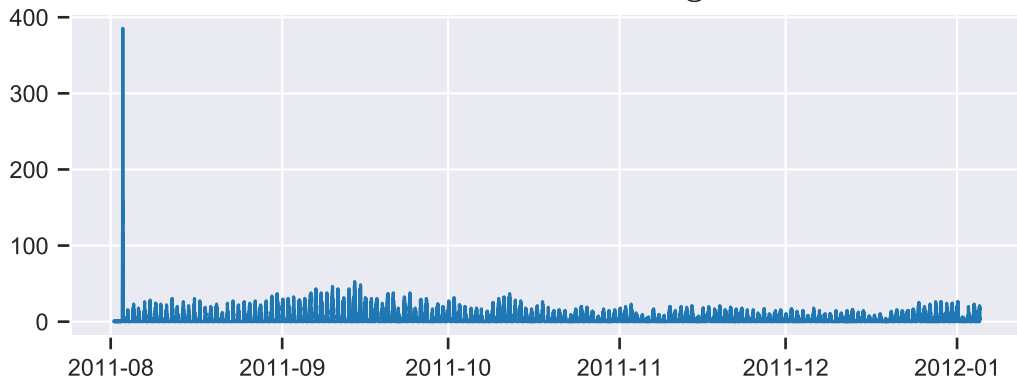


Pulse-7-2010 - ECO-PARS:PARS-135 @ 31.0

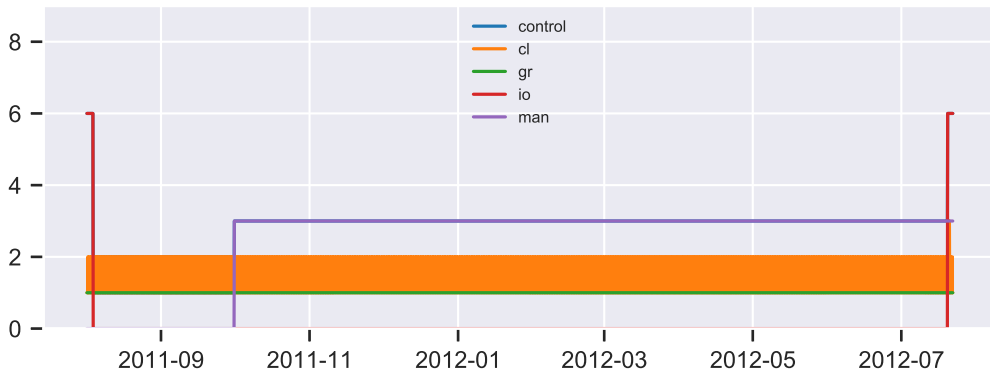
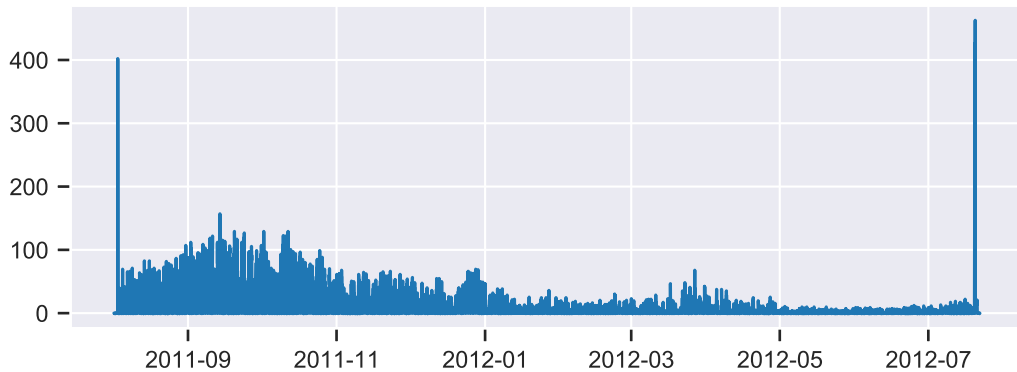




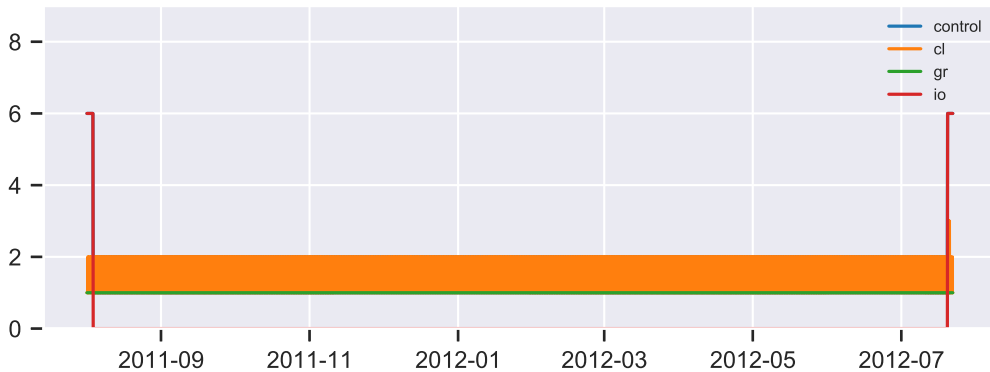
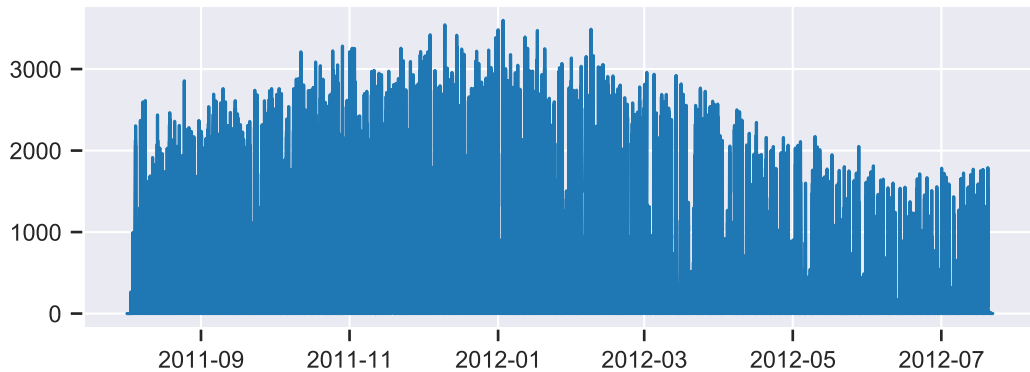
Pulse-8-2011 - MDS-MKVL:200341 @ 50.0



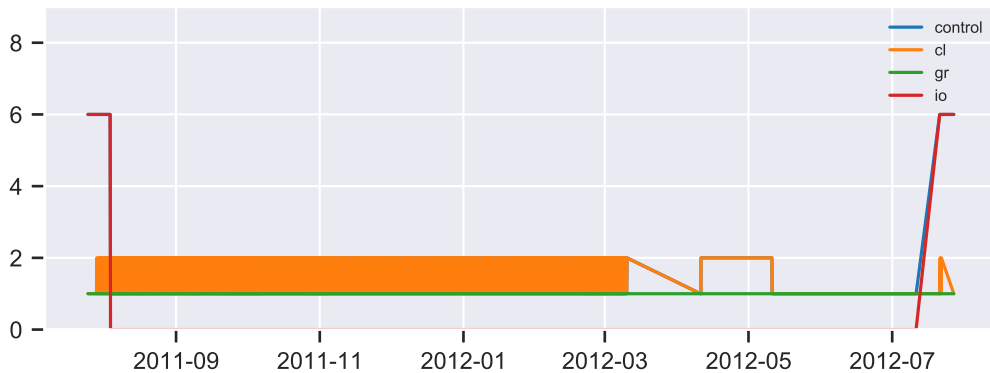
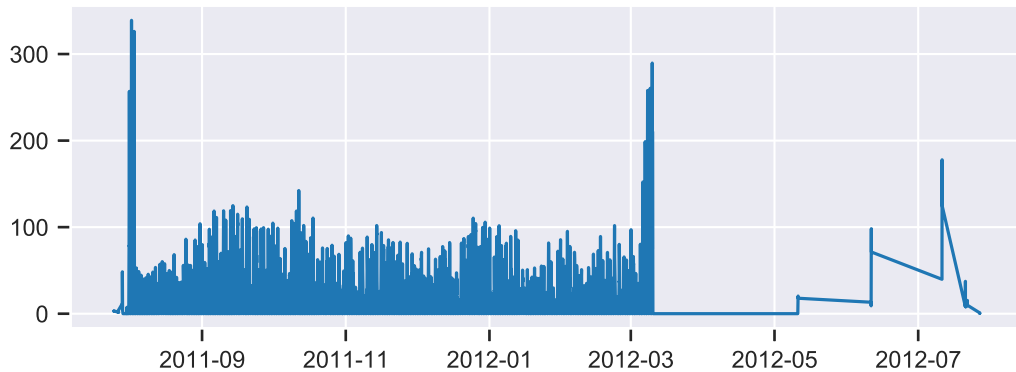
Pulse-8-2011 - MDS-MKVL:200664 @ 27.0



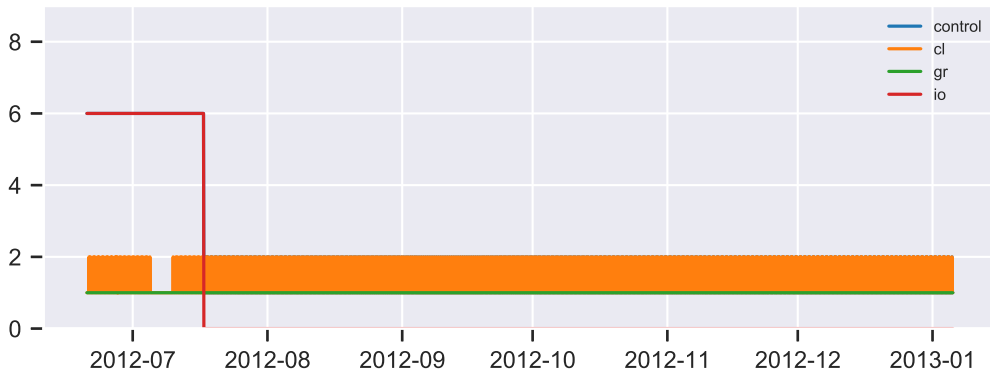
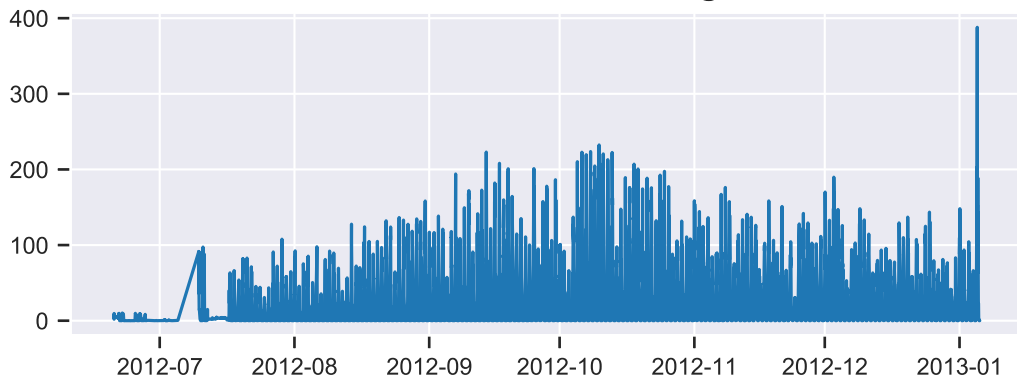
Pulse-8-2011 - MDS-MKVL:200665 @ 0.0



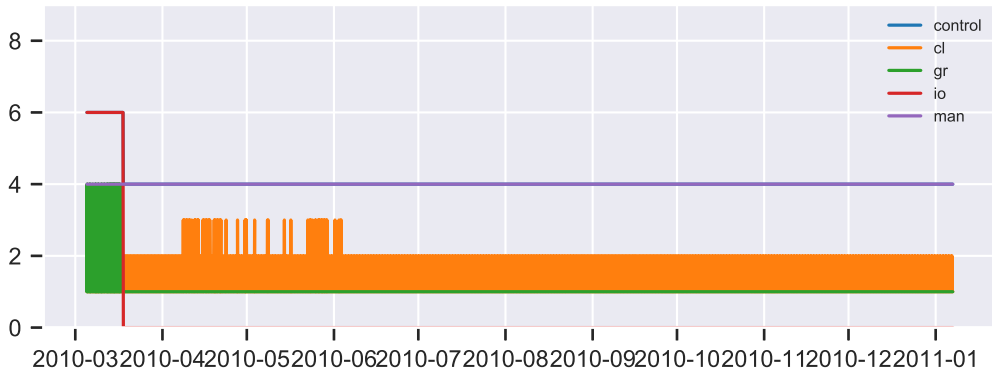
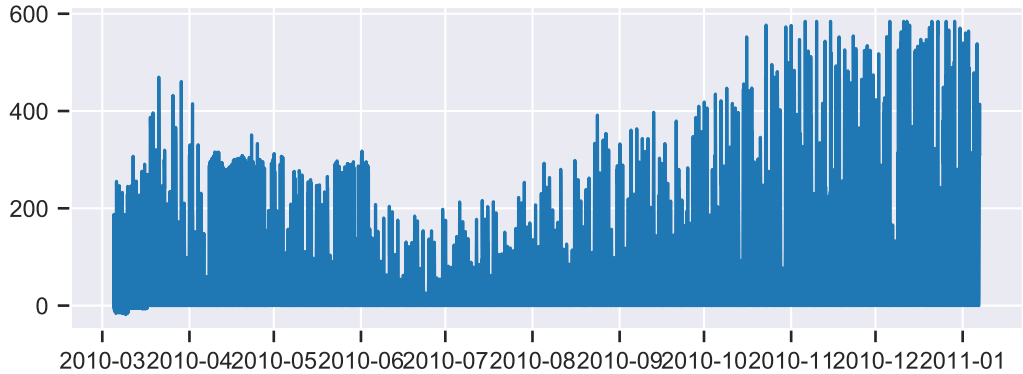
Pulse-8-2011 - ECO-PARS:PARS-134 @ 33.8



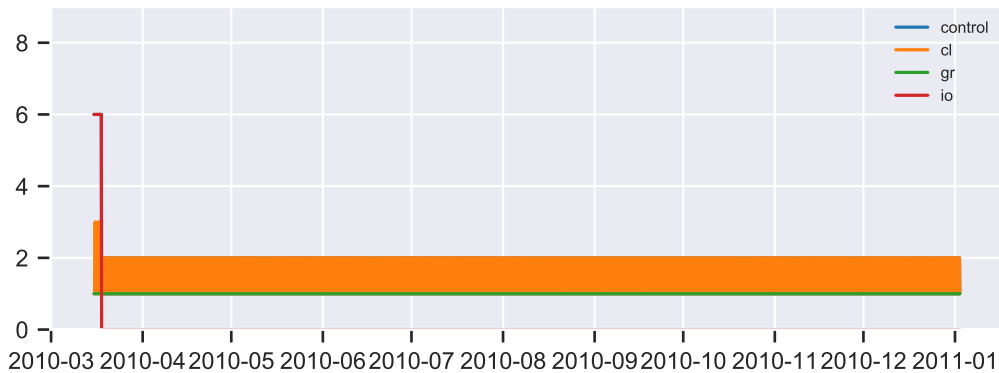
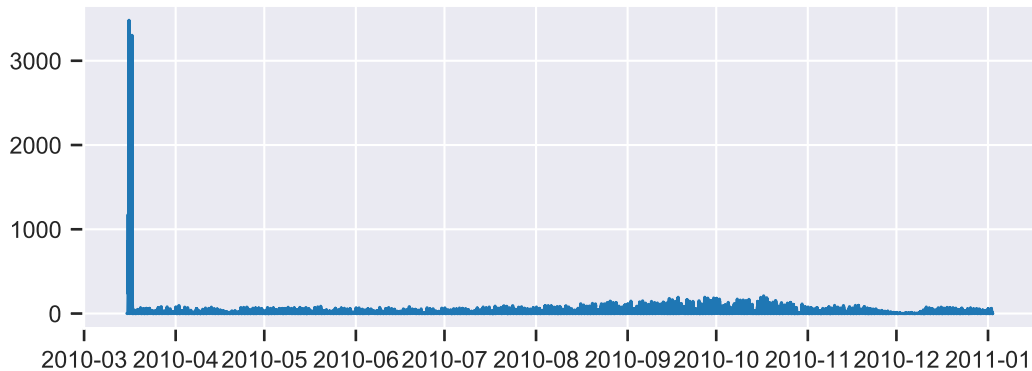
Pulse-9-2012 - ECO-PARS:PARS-135 @ 38.0



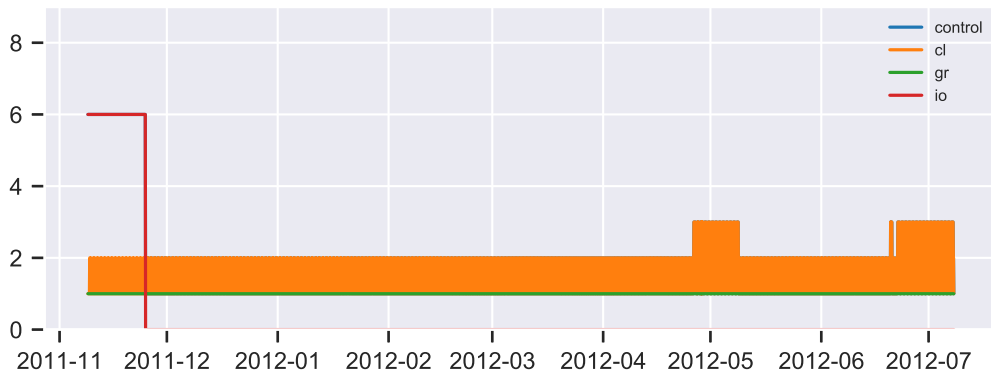
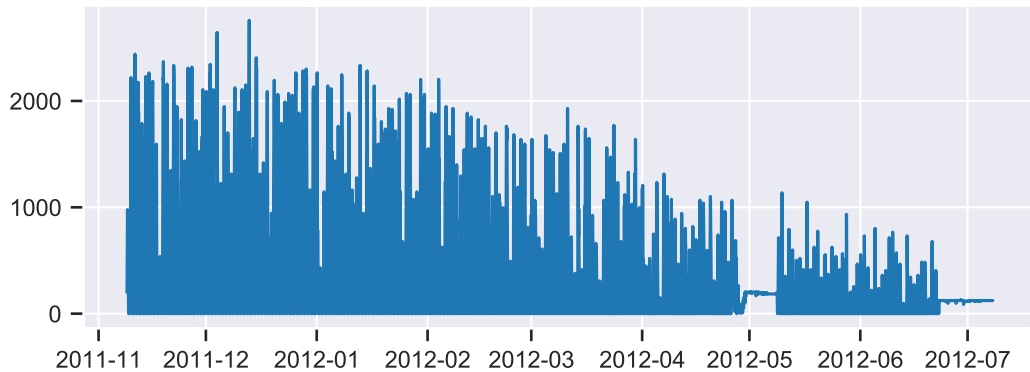
SOFS-1-2010 - LI-190SA:Q40966 @ -2.72



SOFS-1-2010 - MDS-MKVL:201318 @ 40.0

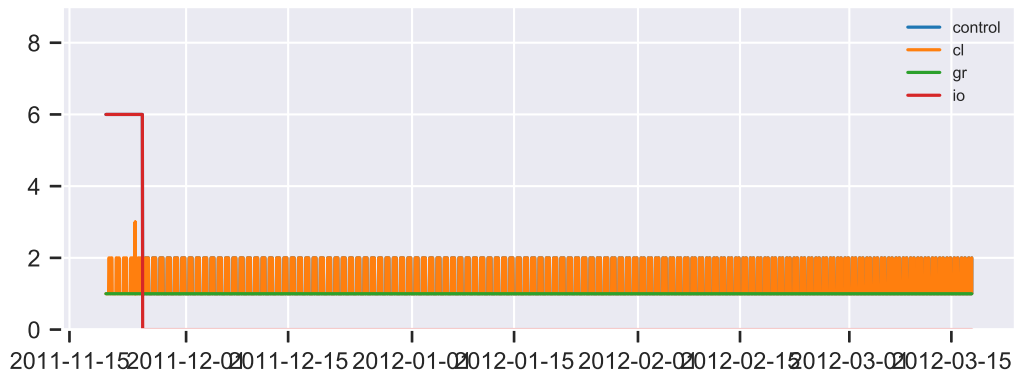
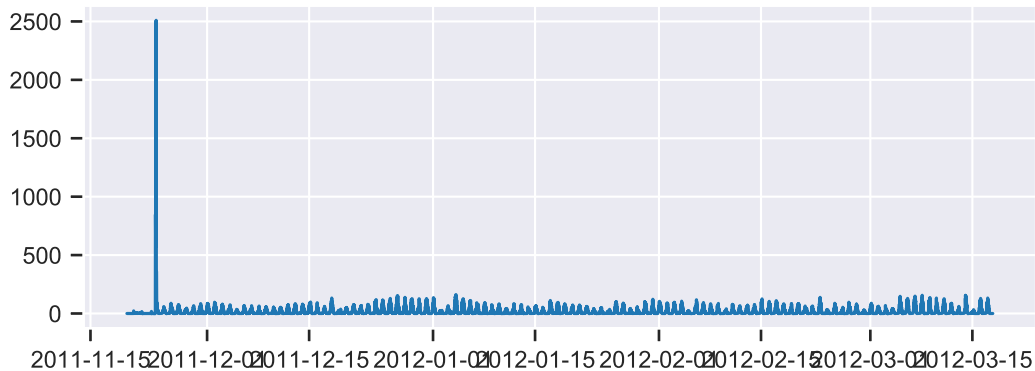


SOFS-2-2011 - LI-190SA:Q40966 @ -3.0

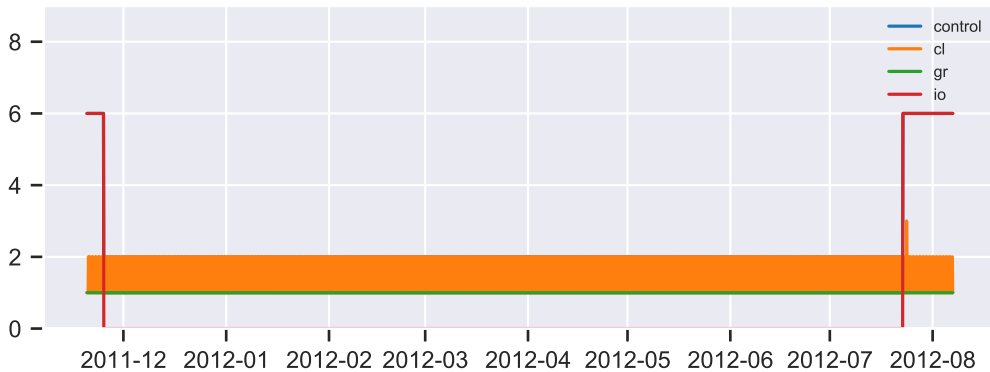
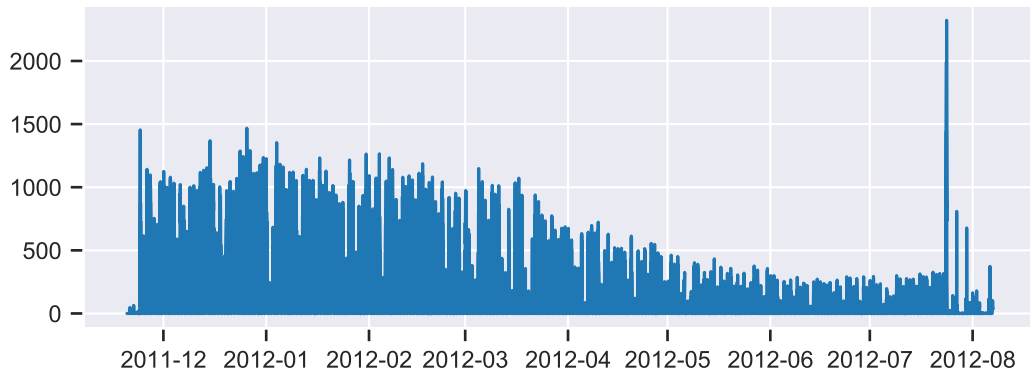




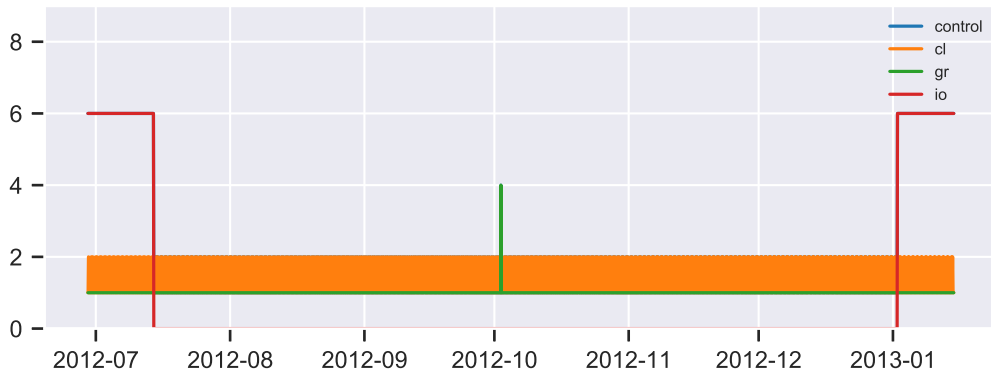
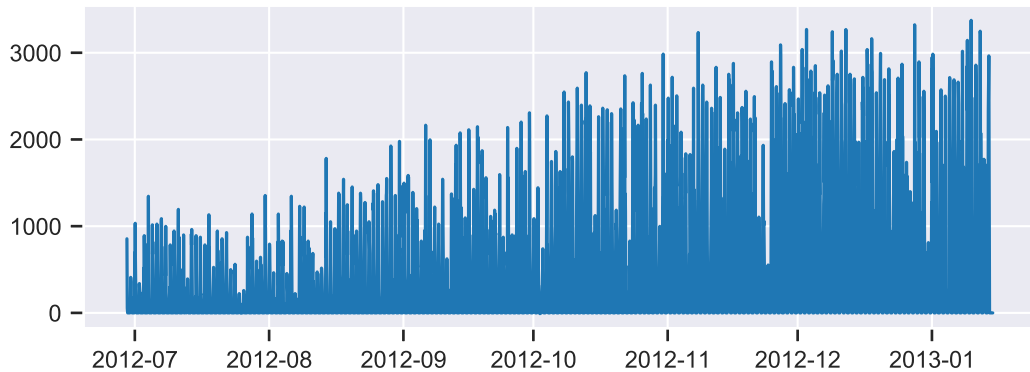
SOFS-2-2011 - MDS-MKVL:201318 @ 40.0



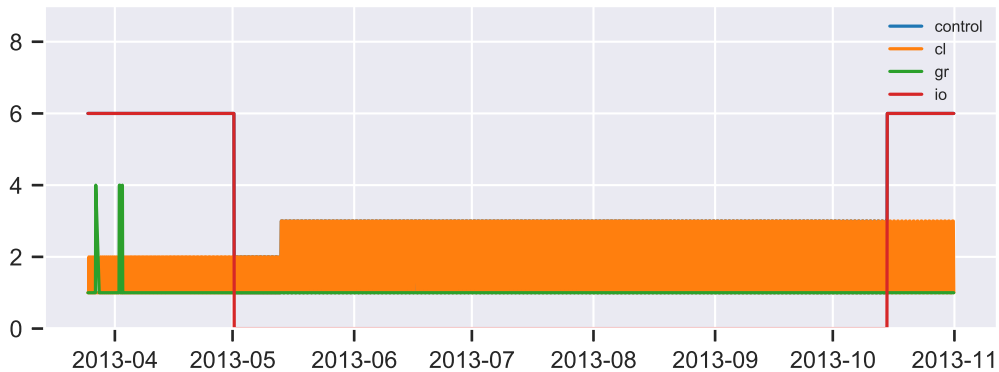
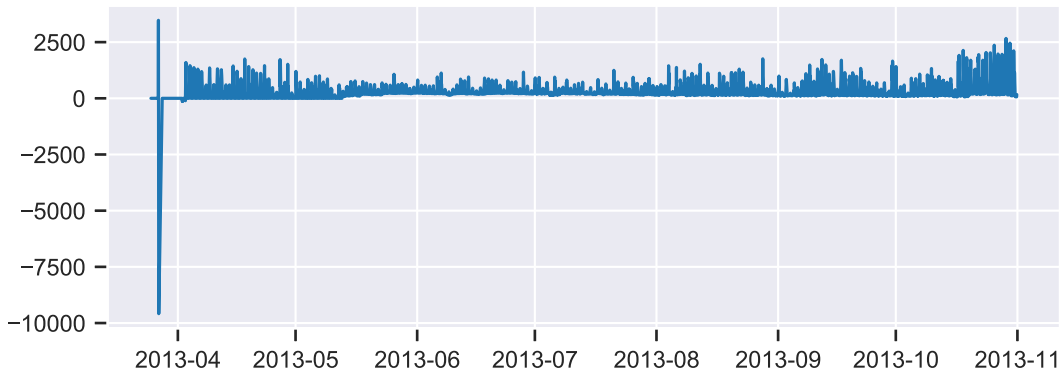
SOFS-2-2011 - MDS-MKVL:201319 @ 10.0



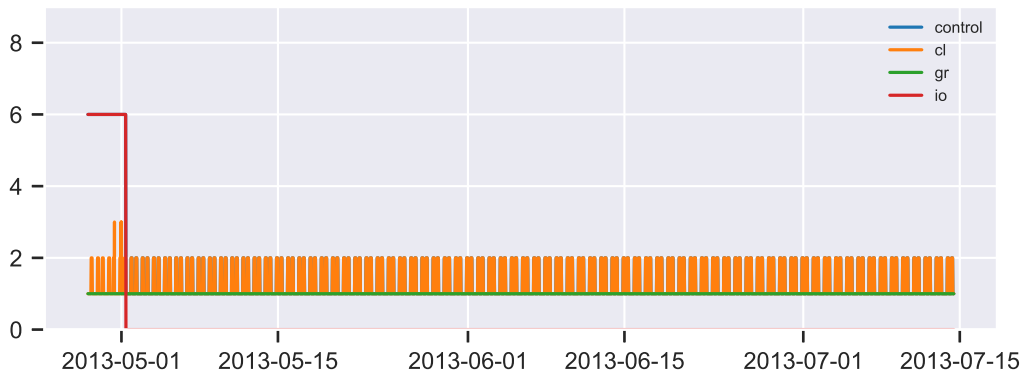
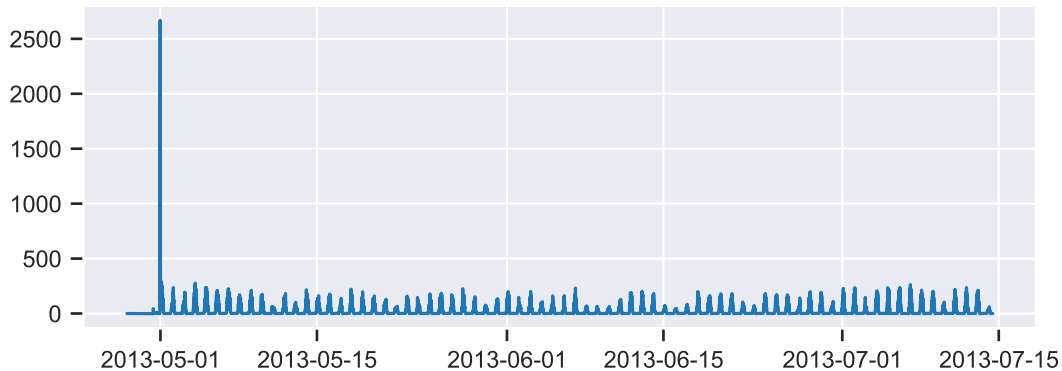
SOFS-3-2012 - LI-190SA:Q40966 @ -2.8



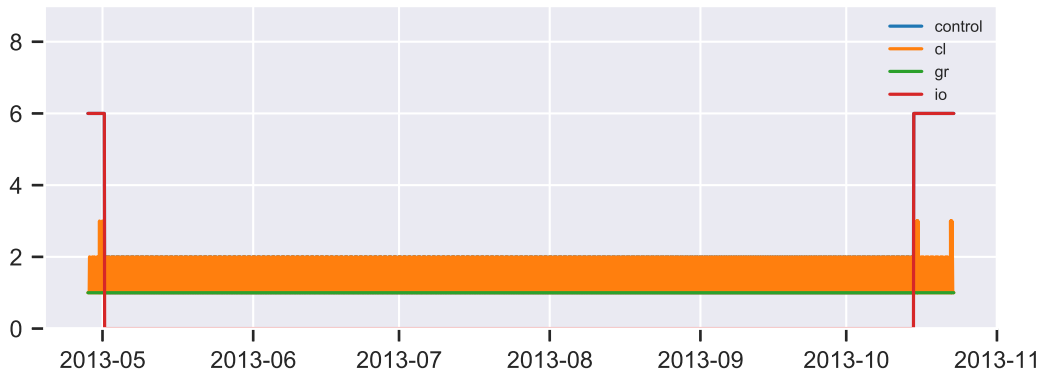
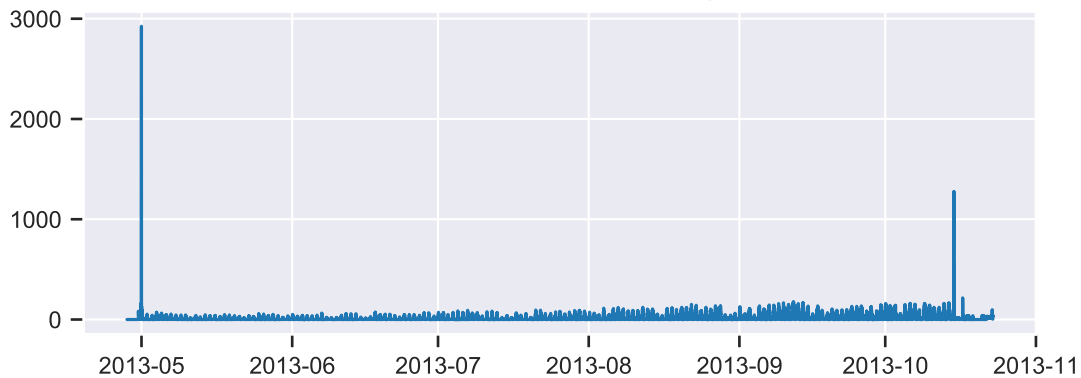
SOFS-4-2013 - LI-190SA:Q47470 @ -1.8



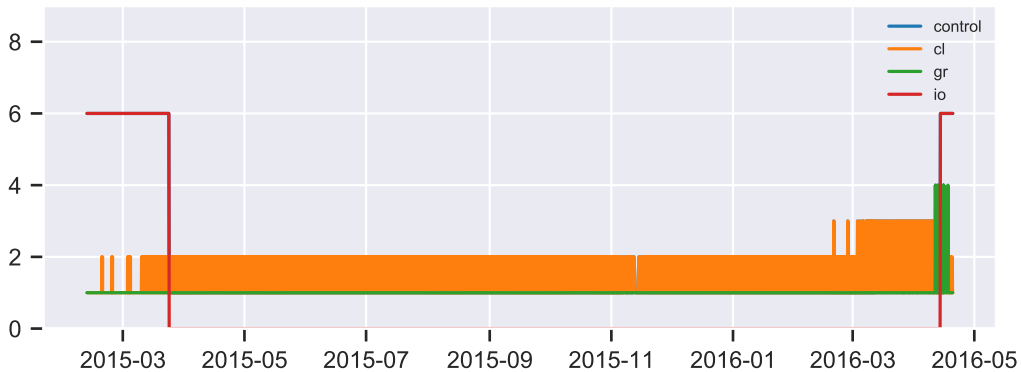
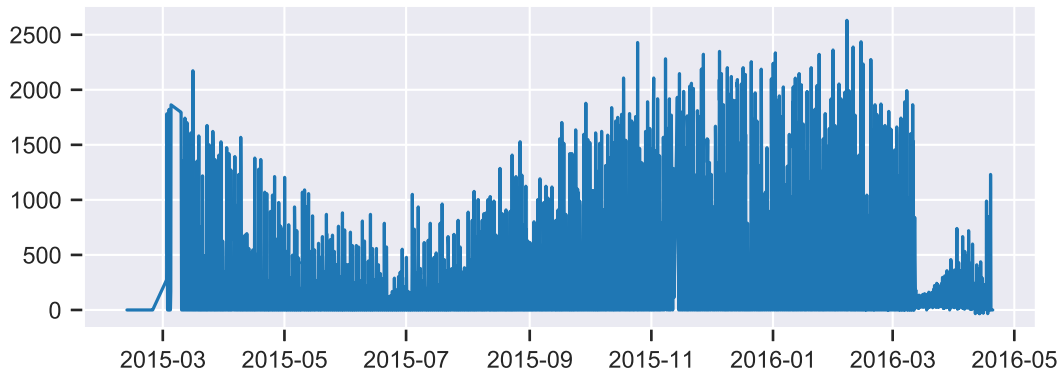
SOFS-4-2013 - MDS-MKVL:201318 @ 20.0



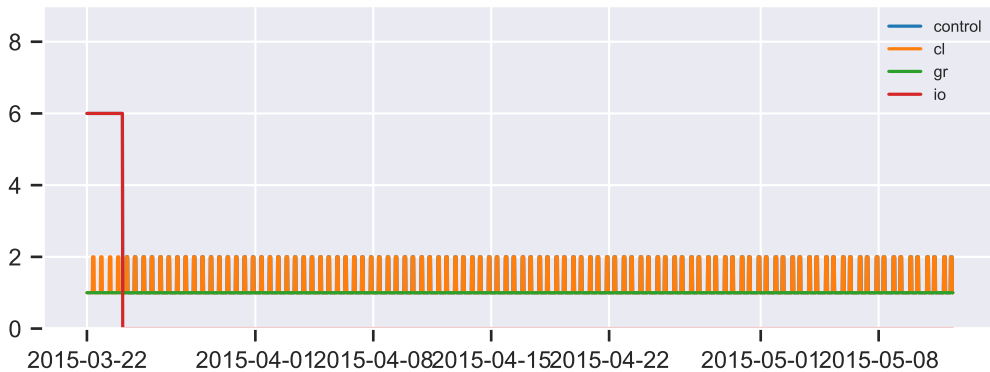
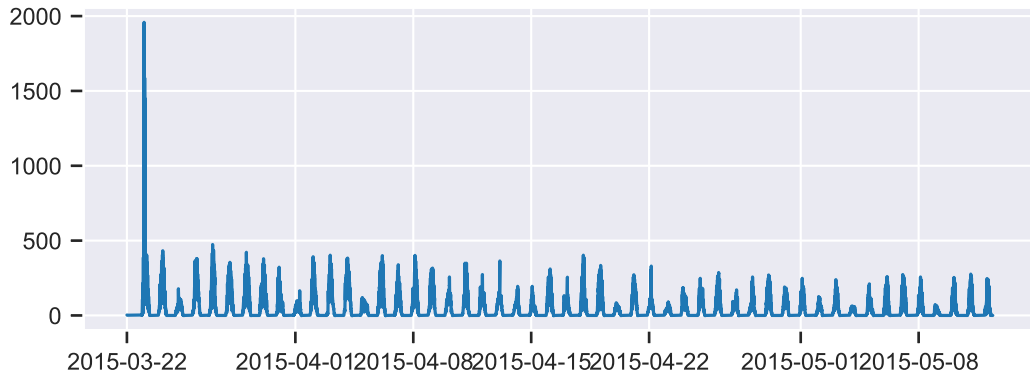
SOFS-4-2013 - MDS-MKVL:201319 @ 40.0



SOFS-5-2015 - LI-190SA:Q47470 @ -1.8

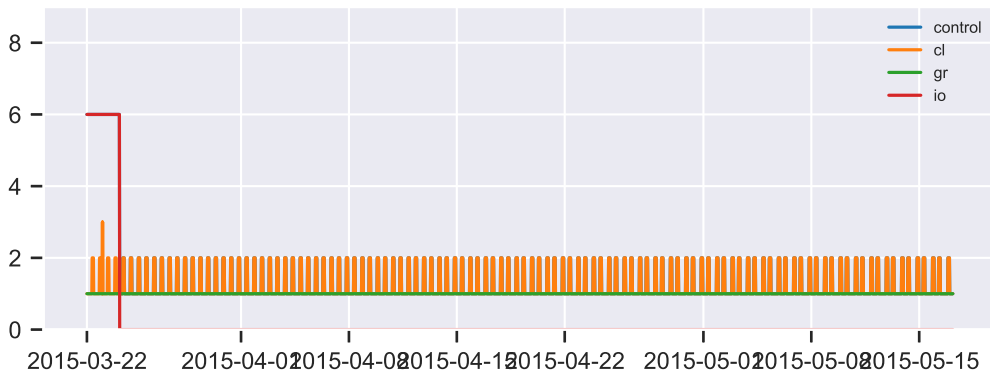
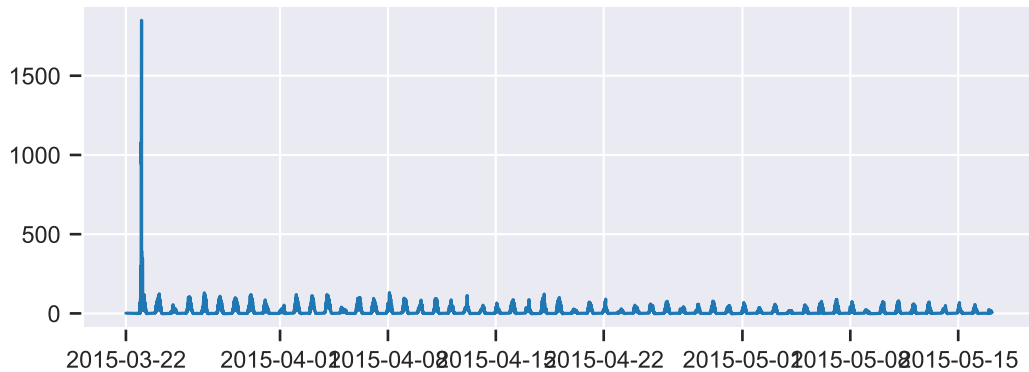


SOFS-5-2015 - MDS-MKVL:201318 @ 20.0

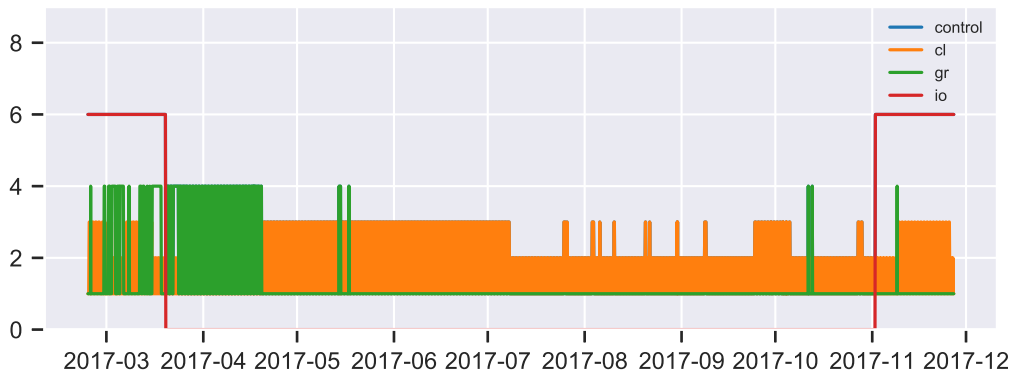
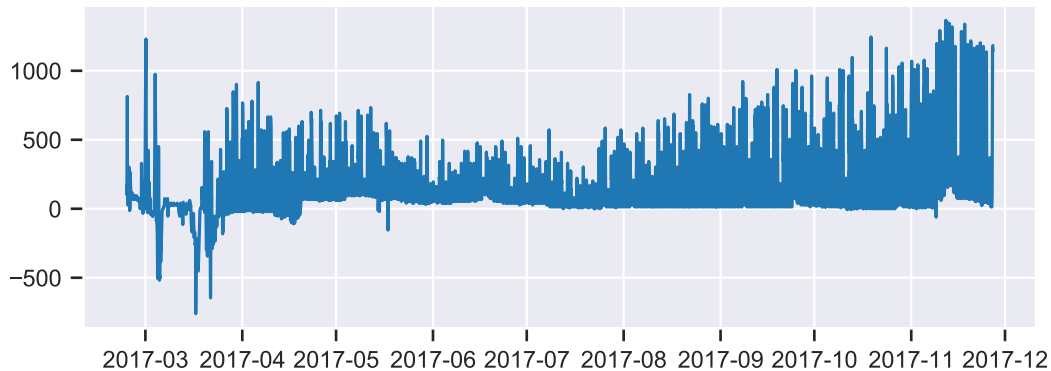




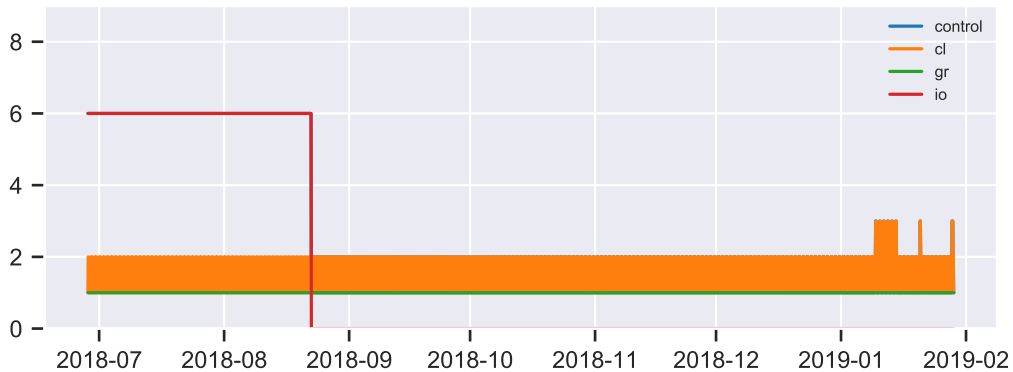
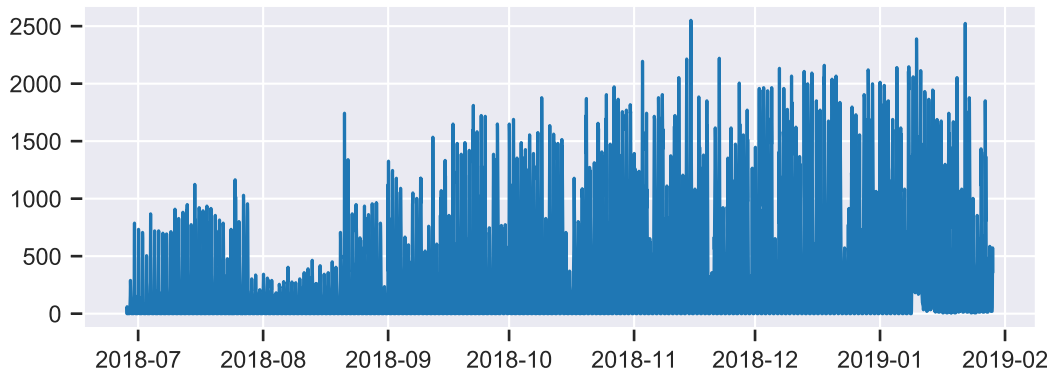
SOFS-5-2015 - MDS-MKVL:201319 @ 40.0



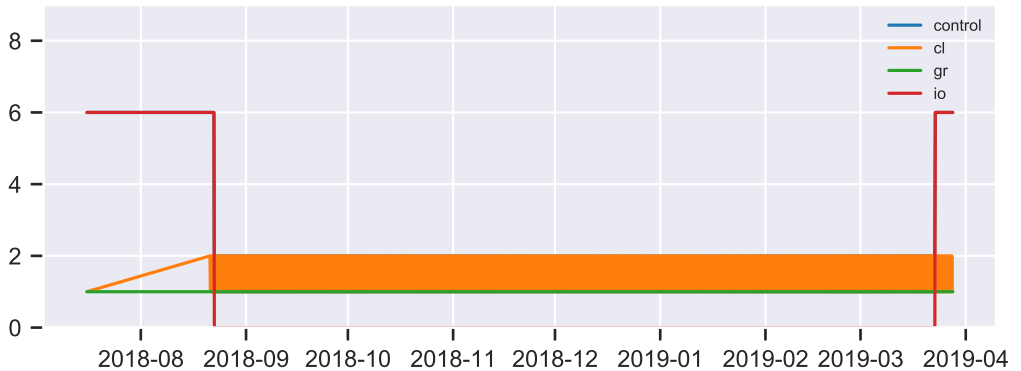
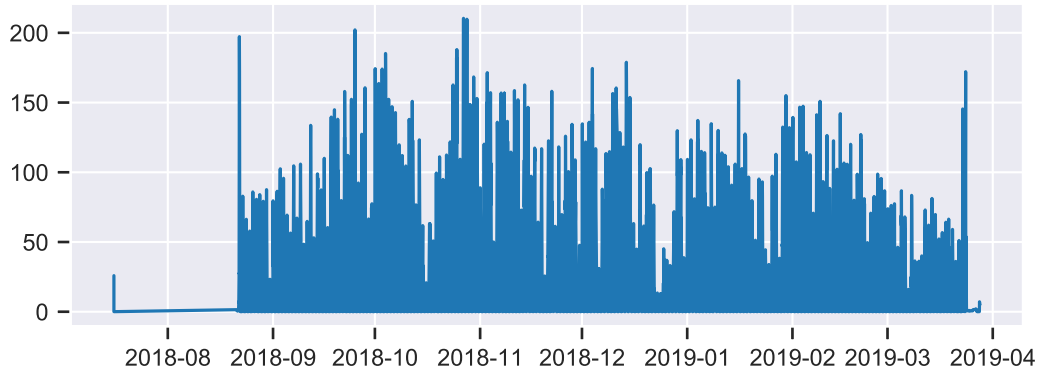
SOFS-6-2017 - LI-190SA:Q47470 @ -1.8



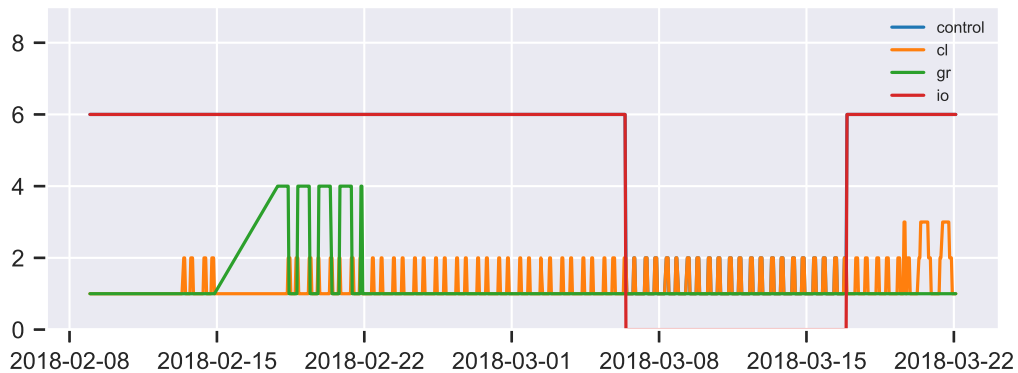
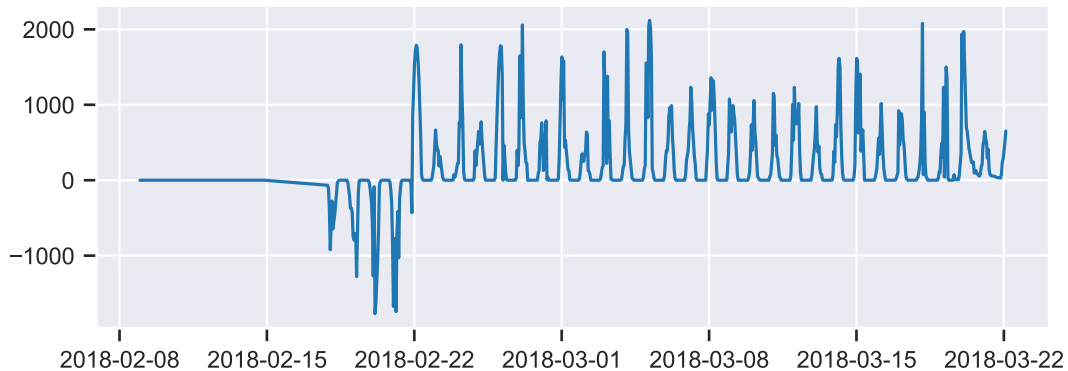
SOFS-7.5-2018 - LI-190SA:Q47470 @ -2.0



SOFS-7.5-2018 - ECO-PARS:PARSB-419 @ 30.0



SOFS-7-2018 - LI-190SA:Q47470 @ -1.8



# 9 Accessing the Data

Data are provided on-line from the Australian Ocean Data Network in CF compliant netcdf format files, with one file per deployment. We recommend using all data with flags of 1 or 2.

The URL for data access is:

<https://portal.aodn.org.au/>

## Data file structure

```
variables:
  double TIME(TIME) ;
    TIME:long_name = "time" ;
    TIME:units = "days since 1950-01-01 00:00:00 UTC" ;
    TIME:calendar = "gregorian" ;
    TIME:axis = "T" ;
    TIME:standard_name = "time" ;
    TIME:valid_max = 90000. ;
    TIME:valid_min = 0. ;
  double NOMINAL_DEPTH ;
    NOMINAL_DEPTH:axis = "Z" ;
    NOMINAL_DEPTH:long_name = "nominal depth" ;
    NOMINAL_DEPTH:positive = "down" ;
    NOMINAL_DEPTH:reference_datum = "sea surface" ;
    NOMINAL_DEPTH:standard_name = "depth" ;
    NOMINAL_DEPTH:units = "m" ;
    NOMINAL_DEPTH:valid_max = 12000. ;
    NOMINAL_DEPTH:valid_min = -5. ;
  double LATITUDE ;
    LATITUDE:axis = "Y" ;
    LATITUDE:long_name = "latitude" ;
    LATITUDE:reference_datum = "WGS84 geographic coordinate system" ;
    LATITUDE:standard_name = "latitude" ;
    LATITUDE:units = "degrees_north" ;
    LATITUDE:valid_max = 90. ;
    LATITUDE:valid_min = -90. ;
  double LONGITUDE ;
    LONGITUDE:axis = "X" ;
    LONGITUDE:long_name = "longitude" ;
    LONGITUDE:reference_datum = "WGS84 geographic coordinate system" ;
    LONGITUDE:standard_name = "longitude" ;
    LONGITUDE:units = "degrees_east" ;
    LONGITUDE:valid_max = 180. ;
    LONGITUDE:valid_min = -180. ;
  float PAR_COUNT(TIME) ;
    PAR_COUNT:sensor_SeaVoX_L22_code = "SDN:L22::T00L0676" ;
    PAR_COUNT:comment_attached_instrument = "Wet-LABS ; PARS-419" ;
    PAR_COUNT:calibration_PAR_Im = 1.3589 ;
    PAR_COUNT:calibration_PAR_digital_A1 = 2923. ;
    PAR_COUNT:calibration_PAR_digital_A0 = 4266. ;
    PAR_COUNT:calibration_PAR_date = "9/5/2014" ;
    PAR_COUNT:calibration_PAR_facility = "Satlantic" ;
    PAR_COUNT:calibration_PAR_SN = "PARSB-419" ;
  float PAR(TIME) ;
    PAR:_FillValue = NaNf ;
    PAR:sensor_SeaVoX_L22_code = "SDN:L22::T00L0676" ;
    PAR:comment_attached_instrument = "Wet-LABS ; PARS-419" ;
    PAR:calibration_PAR_Im = 1.3589 ;
    PAR:calibration_PAR_digital_A1 = 2923. ;
    PAR:calibration_PAR_digital_A0 = 4266. ;
    PAR:calibration_PAR_date = "9/5/2014" ;
    PAR:calibration_PAR_facility = "Satlantic" ;
    PAR:calibration_PAR_SN = "PARSB-419" ;
    PAR:standard_name = "downwelling_photosynthetic_photon_flux_in_sea_water" ;
    PAR:long_name = "downwelling_photosynthetic_photon_flux_in_sea_water" ;
    PAR:units = "umol/m2/s" ;
    PAR:comment_sensor_type = "cosine sensor, with integrated anti-fouling Bio-wiper" ;
    PAR:ancillary_variables = "Final Io
    Gr Cl" ;
  byte Final(TIME) ;
    Final:_FillValue = 99b ;
    Final:long_name = "quality_code for downwelling_photosynthetic_photon_flux_in_sea_water" ;
  float ALT(TIME) ;
    ALT:_FillValue = NaNf ;
    ALT:units = "degree" ;
    ALT:long_name = "sun_altitude" ;
    ALT:coordinates = "TIME LATITUDE LONGITUDE NOMINAL_DEPTH" ;
    ALT:comment = "using http://docs.pysolar.org/en/latest/ v0.8 get_altitude" ;
  float SOLAR(TIME) ;
    SOLAR:_FillValue = NaNf ;
    SOLAR:units = "W/m2" ;
    SOLAR:long_name = "incoming_solar_radiation" ;
```

```

    SOLAR:coordinates = "TIME LATITUDE LONGITUDE NOMINAL_DEPTH" ;
    SOLAR:comment = "using http://docs.pysolar.org/en/latest/ v0.8 extraterrestrial_irrad()
                    with incoming = 1361 W/m^2" ;
float ePAR(TIME) ;
    ePAR:_FillValue = NaN ;
    ePAR:units = "umol/m^2/s" ;
    ePAR:long_name = "incoming_solar_radiation converted to PAR (x2.114) attenuated by depth" ;
    ePAR:coordinates = "TIME LATITUDE LONGITUDE NOMINAL_DEPTH" ;
    ePAR:comment = "using http://docs.pysolar.org/en/latest/ v0.8 extraterrestrial_irrad()
                    with incoming = 1361 W/m^2, x 2.114, kd = 0.04" ;
byte Io(TIME) ;
    Io:_FillValue = 99b ;
    Io:long_name = "quality flag for downwelling_photosynthetic_photon_flux_in_sea_water" ;
    Io:standard_name = "downwelling_photosynthetic_photon_flux_in_sea_water_status_flag" ;
    Io:quality_control_conventions = "IMOS standard flags" ;
    Io:flag_values = 0b, 1b, 2b, 3b, 4b, 6b, 7b, 9b ;
    Io:flag_meanings = "unknown good_data probably_good_data probably_bad_data
                       bad_data not_deployed interpolated missing_value" ;
    Io:comment = "data flagged not deployed (6) when out of water" ;
byte Gr(TIME) ;
    Gr:_FillValue = 99b ;
    Gr:long_name = "quality flag for downwelling_photosynthetic_photon_flux_in_sea_water" ;
    Gr:standard_name = "downwelling_photosynthetic_photon_flux_in_sea_water_status_flag" ;
    Gr:flag_values = 0b, 1b, 2b, 3b, 4b, 6b, 7b, 9b ;
    Gr:quality_control_conventions = "IMOS standard flags" ;
    Gr:flag_meanings = "unknown good_data probably_good_data probably_bad_data
                       bad_data not_deployed interpolated missing_value" ;
    Gr:comment = "Test 4. gross range test" ;
byte Cl(TIME) ;
    Cl:_FillValue = 99b ;
    Cl:long_name = "quality flag for downwelling_photosynthetic_photon_flux_in_sea_water" ;
    Cl:standard_name = "downwelling_photosynthetic_photon_flux_in_sea_water_status_flag" ;
    Cl:quality_control_conventions = "IMOS standard flags" ;
    Cl:flag_values = 0b, 1b, 2b, 3b, 4b, 6b, 7b, 9b ;
    Cl:flag_meanings = "unknown good_data probably_good_data probably_bad_data
                       bad_data not_deployed interpolated missing_value" ;
    Cl:comment = "Test 7. climatology test" ;
    Cl:comment_note = "cosine sensor, par < (2 * SOLAR) + 15" ;
float SWR(TIME) ;
    SWR:_FillValue = NaN ;

// global attributes:
:abstract = "Oceanographic and meteorological data from the Southern Ocean Time Series observatory in
            the Southern Ocean southwest of Tasmania" ;
:acknowledgement = "Any users of IMOS data are required to clearly acknowledge the source of the material
                    derived from IMOS in the format: \"Data was sourced from the Integrated Marine
                    Observing System (IMOS) – IMOS is a national collaborative research infrastructure,
                    supported by the Australian Government.\" If relevant, also credit other organisations
                    involved in collection of this particular datastream (as listed in \"credit\" in the
                    metadata record)." ;
:author = "Jansen, Peter" ;
:author_email = "peter.jansen@csiro.au" ;
:citation = "The citation in a list of references is: \"IMOS [year-of-data-download], [Title],
            [data-access-URL], accessed [date-of-access]\"." ;
:comment = "Geospatial vertical min/max information has been filled using the NOMINAL_DEPTH." ;
:Conventions = "CF-1.6, IMOS-1.4" ;
:data_centre = "Australian Ocean Data Network (AODN)" ;
:data_centre_email = "info@aodn.org.au" ;
:deployment_code = "S0FS-7.5-2018" ;
:disclaimer = "Data, products and services from IMOS are provided \"as is\" without any warranty as
              to fitness for a particular purpose." ;
:featureType = "timeSeries" ;
:file_version_quality_control = "Raw data is defined as unprocessed data and data products that have
                                not undergone quality control. The data may be in engineering physical units, time and
                                location details can be in relative units and values can be pre-calibration measurements." ;
:geospatial_lat_max = -47.02274 ;
:geospatial_lat_min = -47.02274 ;
:geospatial_lat_units = "degrees_north" ;
:geospatial_lon_max = 142.23341 ;
:geospatial_lon_min = 142.23341 ;
:geospatial_lon_units = "degrees_east" ;
:geospatial_vertical_max = 30. ;
:geospatial_vertical_min = 30. ;
:geospatial_vertical_positive = "down" ;
:institution = "DWM-SOTS" ;
:institution_references = "http://www.imos.org.au/aodn.html" ;
:instrument = "Wet-LABS ; ECO-PARS" ;
:instrument_model = "ECO-PARS" ;
:instrument_nominal_depth = 30. ;
:instrument_serial_number = "PARSB-419" ;
:keywords_vocabulary = "IMOS parameter names.
                        See https://github.com/aodn/imos-toolbox/blob/master/IMOS/imosParameters.txt" ;
:license = "http://creativecommons.org/licenses/by/4.0/" ;
:naming_authority = "IMOS" ;
:platform_code = "S0FS" ;
:principal_investigator = "Trull, Tom" ;
:principal_investigator_email = "tom.trull@csiro.au" ;
:project = "Integrated Marine Observing System (IMOS)" ;
:references = "http://www.imos.org.au" ;
:site_code = "SOTS" ;
:site_nominal_depth = 4624. ;
:standard_name_vocabulary = "NetCDF Climate and Forecast (CF) Metadata Convention Standard Name Table 67" ;
:time_coverage_end = "2019-03-28T04:27:42Z" ;
:time_coverage_start = "2018-07-16T03:05:34Z" ;
:time_deployment_end = "2019-03-22T21:40:39Z" ;
:time_deployment_start = "2018-08-22T13:17:54Z" ;

```

```

:title = "Oceanographic mooring data deployment of SOFS at latitude -47.0 longitude 142.2 depth
30 (m) instrument WetLABs ; ECO-PARS serial PARSB-419" ;
:voyage_deployment = "http://www.cmar.csiro.au/data/trawler/survey_details.cfm?survey=IN2018_V07" ;
:voyage_recovery = "http://www.cmar.csiro.au/data/trawler/survey_details.cfm?survey=IN2019_V02" ;
:date_created = "2020-06-17T04:51:10Z" ;
:file_version = "Level 1 - Quality Controlled Data" ;
:history = "2020-05-13 created from file data/PAR/raw_files/SOFS-7.5-2018/PARSB-419.raw
2020-05-13 : attributes added from file(s) [metadata/sofs-7.5.metadata.csv,
metadata/imos.metadata.csv, metadata/sots.metadata.csv,
metadata/sofs.metadata.csv, metadata/variable.metadata.csv]
2020-05-13 : extracted from
IMOS_DWM-SOTS_R_20180716_SOFS_FV00_SOFS-7.5-2018-ECO-PARS-PARSB-419-30m_END-20190328_C-20200513.nc
2020-05-13 : added incoming radiation
2020-06-17 : quality_control variables added.
2020-06-17 : in-out water marked 795
2020-06-17 PAR global range min = -1.7 max = 10000 marked 0
2020-06-17 PAR global range min = -1.7 max = 4500 marked 0
2020-06-17 PAR climate range, marked 0"

```

#### Variables in netCDF file,

```

PAR    downwelling_photosynthetic_photon_flux_in_sea_water

ALT    sun_altitude
        At location
SOLAR  incoming_solar_radiation
        At location
ePAR   incoming_solar_radiation converted to PAR (x2.114) attenuated by depth

SWR    Short Wave radiation from nearest sensor

```



## 10 References

Biggs, William W., Principles of Radiation Measurement, LiCor,  
<https://www.licor.com/env/applications/photosynthetically.html>

Britton, C.M., Dodd, J.D. (1976), Relationships of photosynthetically active radiation and shortwave irradiance. *Agricultural Meteorology* 17: 1-7.

Eriksen, R., T. W. Trull, D. Davies, P. Jansen, A. T. Davidson, K. Westwood, and R. van den Enden (2018), Seasonal succession of phytoplankton community structure from autonomous sampling at the Australian Southern Ocean Time Series (SOTS) observatory, *Marine Ecology Progress Series*, 589, 13-31, doi:10.3354/meps12420.

Herraiz-Borreguero, L., Rintoul, S.R. (2011), Regional circulation and its impact on upper ocean variability south of Tasmania (Australia). *Deep-Sea Research II* 58: 2071-2081.

Kirk, J.T.O. (1994), *Light and Photosynthesis in Aquatic Ecosystems*. Cambridge University Press, Cambridge.

McCree, J. K. (1972), Test of current definitions of photosynthetically active radiation against leaf photosynthesis data *Agricultural Meteorology*, 10, 443-453.

Morel, A., Y. Huot, B. Gentili, P. J. Werdell, S. B. Hooker, and B. A. Franz (2007), Examining the consistency of products derived from various ocean color sensors in open ocean (Case 1) waters in the perspective of a multi-sensor approach, *Remote Sensing of Environment*, 111(1), 69-88.

Schallenberg C., Harley J.W., Jansen P., Davies D.M. and Trull T.W. (2019) Multi-Year Observations of Fluorescence and Backscatter at the Southern Ocean Time Series (SOTS) Shed Light on Two Distinct Seasonal Bio-Optical Regimes. *Front. Mar. Sci.* 6:595.doi: 10.3389/fmars.2019.00595

Trull, T.W., Bray, S.G., Manganini, S.J., Honjo, S., François, R. (2001), Moored sediment trap measurements of carbon export in the Subantarctic and Polar Frontal Zones of the Southern Ocean, south of Australia. *Journal of Geophysical Research* 106: 31489-31510.

# Appendix A Python code used for processing

Please refer to the following link for access to the R and Matlab files involved in performing the QC tests described in this report:

<https://github.com/petejan/sots>

<https://github.com/petejan/imos-tools>

## Appendix B Sensor Calibration Sheets

Attached below are the calibration sheets for all PAR sensors deployed at the SOTS site.

# Light Intensity Calibration Certificate

Model : DEFI-L  
 Serial No. : 082V022  
 Date : February 06, 2013  
 Location : Kobe Production Section  
 Method : Calibration equation is determined from linear regression of samples of the reference light quantum against A/D values. Samples are taken at approximately 0, 500, 1000, 1500, and 2000  $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ .

1. Equation Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ] = A+B × N N: A/D value

2. Coefficients A = +1.261990e+04 B = -1.945354e-01  
Immersion effect: 1.42

### 3. Calibration results

Acceptance:  $\pm 4\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	A/D value	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	OK/NG
0	64872	0.0	0.0	$\pm 200.0$	OK
534	62162	527.2	-6.8	$\pm 200.0$	OK
1017	59680	1010.0	-7.0	$\pm 200.0$	OK
1530	57010	1529.4	-0.6	$\pm 200.0$	OK
2013	54495	2018.7	5.7	$\pm 200.0$	OK

### 4. Verification

Criteria of judgement : Residual error of the instrument light quantum at arbitrary point is within the acceptance value.

Acceptance:  $\pm 4\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Judgement
1060	1085.4	25.4	$\pm 200.0$	Passed

Examined H. Yamane  
Approved T. Nishimura

JFE Advantech Co., Ltd.

# Light Intensity Calibration Certificate

Model : DEFI-L  
 Serial No. : 082V025  
 Date : February 08, 2013  
 Location : Kobe Production Section  
 Method : Calibration equation is determined from linear regression of samples of the reference light quantum against A/D values. Samples are taken at approximately 0, 500, 1000, 1500, and 2000  $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ .

1. Equation Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ] =  $A+B \times N$  N: A/D value

2. Coefficients A = +1.276023e+04 B = -1.966834e-01  
Immersion effect: 1.43

3. Calibration results

Acceptance:  $\pm 4\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	A/D value	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	OK/NG
0	64877	0.0	0.0	$\pm 200.0$	OK
558	62081	549.9	-8.1	$\pm 200.0$	OK
1042	59604	1037.1	-4.9	$\pm 200.0$	OK
1504	57240	1502.1	-1.9	$\pm 200.0$	OK
2028	54535	2034.1	6.1	$\pm 200.0$	OK

4. Verification

Criteria of judgement : Residual error of the instrument light quantum at arbitrary point is within the acceptance value.

Acceptance:  $\pm 4\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Judgement
1008	985.5	-22.5	$\pm 200.0$	Passed

Examined H. Yamane  
Approved T. Nishimura

JFE Advantech Co., Ltd.

# Light Intensity Calibration Certificate

Model : DEFI-L  
 Serial No. : 082V024  
 Date : February 08, 2013  
 Location : Kobe Production Section  
 Method : Calibration equation is determined from linear regression of samples of the reference light quantum against A/D values. Samples are taken at approximately 0, 500, 1000, 1500, and 2000  $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ .

1. Equation Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ] = A+B × N N: A/D value

2. Coefficients A = +1.233661e+04 B = -1.901802e-01  
Immersion effect: 1.38

### 3. Calibration results

Acceptance:  $\pm 4\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	A/D value	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	OK/NG
0	64868	0.0	0.0	$\pm 200.0$	OK
541	62061	533.8	-7.2	$\pm 200.0$	OK
1020	59539	1013.5	-6.5	$\pm 200.0$	OK
1540	56769	1540.3	0.3	$\pm 200.0$	OK
2030	54168	2034.9	4.9	$\pm 200.0$	OK

### 4. Verification

Criteria of judgement : Residual error of the instrument light quantum at arbitrary point is within the acceptance value.

Acceptance:  $\pm 4\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Judgement
1026	999.6	-26.4	$\pm 200.0$	Passed

Examined H. Yamane  
Approved T. Nishimura

JFE Advantech Co., Ltd.

# Light Intensity Calibration Certificate

Model : DEFI-L  
 Serial No. : 082V023  
 Date : February 06, 2013  
 Location : Kobe Production Section  
 Method : Calibration equation is determined from linear regression of samples of the reference light quantum against A/D values. Samples are taken at approximately 0, 500, 1000, 1500, and 2000  $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ .

1. Equation Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ] = A+B × N N: A/D value

2. Coefficients A = +1.191277e+04 B = -1.836407e-01  
 Immersion effect: 1.39

3. Calibration results

Acceptance:  $\pm 4\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	A/D value	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	OK/NG
0	64870	0.0	0.0	$\pm 200.0$	OK
518	62085	511.4	-6.6	$\pm 200.0$	OK
1021	59345	1014.6	-6.4	$\pm 200.0$	OK
1511	56655	1508.6	-2.4	$\pm 200.0$	OK
2025	53807	2031.6	6.6	$\pm 200.0$	OK

4. Verification

Criteria of judgement : Residual error of the instrument light quantum at arbitrary point is within the acceptance value.

Acceptance:  $\pm 4\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Judgement
1036	1001.2	-34.8	$\pm 200.0$	Passed

Examined H. Yamane  
 Approved T. Nishimura

JFE Advantech Co., Ltd.

# Light Intensity Calibration Certificate

Model : DEFI2-L  
 Serial No. : 0AAO010  
 Date : December 16, 2015  
 Location : Production Section  
 Method : Calibration equation is determined from linear regression of samples of the reference light quantum against A/D values. Samples are taken at approximately 0, 500, 1000, 1500, and 2000  $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ .

1. Equation Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ] = A+B × N N: A/D value

2. Coefficients A = +9.755507e+03 B = -1.503739e-01  
Immersion effect: 1.40

### 3. Calibration results

Acceptance:  $\pm 0.9\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	A/D value	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	OK/NG
0	64875	0.0	0.0	$\pm 45.0$	OK
513	61465	512.8	-0.2	$\pm 45.0$	OK
1012	58174	1007.7	-4.3	$\pm 45.0$	OK
1515	54787	1517.0	2.0	$\pm 45.0$	OK
2009	51510	2009.7	0.7	$\pm 45.0$	OK

### 4. Verification

Criteria of judgement : Residual error of the instrument light quantum at arbitrary point is within the acceptance value.

Acceptance:  $\pm 3.5\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Judgement
1913	1915.3	2.3	$\pm 175.0$	Passed

Examined R. Shimozato

Approved A. FukuoKa

JFE Advantech Co., Ltd.



# Light Intensity Calibration Certificate

Model : DEFI2-L  
 Serial No. : 0AAO011  
 Date : December 16, 2015  
 Location : Production Section  
 Method : Calibration equation is determined from linear regression of samples of the reference light quantum against A/D values. Samples are taken at approximately 0, 500, 1000, 1500, and 2000  $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ .

1. Equation Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ ] =  $A+B \times N$  N: A/D value

2. Coefficients A = +9.428665e+03 B = -1.453336e-01  
 Immersion effect: 1.39

### 3. Calibration results

Acceptance:  $\pm 0.9\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ ]	A/D value	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ ]	OK/NG
0	64876	0.0	0.0	$\pm 45.0$	OK
513	61313	517.8	4.8	$\pm 45.0$	OK
1014	57937	1008.5	-5.5	$\pm 45.0$	OK
1513	54489	1509.6	-3.4	$\pm 45.0$	OK
2013	50997	2017.1	4.1	$\pm 45.0$	OK

### 4. Verification

Criteria of judgement : Residual error of the instrument light quantum at arbitrary point is within the acceptance value.

Acceptance:  $\pm 3.5\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ ]	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2 \cdot \text{s})$ ]	Judgement
1908	1885.0	-23.0	$\pm 175.0$	Passed

Examined R. Shimozato

Approved A. Fukuda

JFE Advantech Co., Ltd.

# Light Intensity Calibration Certificate

Model : DEF12-L  
 Serial No. : 0AQH011  
 Date : August 02, 2017  
 Location : Production Section  
 Method : Calibration equation is determined from linear regression of samples of the reference light quantum against A/D values. Samples are taken at approximately 0, 500, 1000, 1500, and 2000  $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ .

1. Equation Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ] = A+B × N N: A/D value

2. Coefficients A = +9.617790e+03 B = -1.482488e-01  
Immersion effect: 1.43

### 3. Calibration results

Acceptance:  $\pm 0.9\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	A/D value	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	OK/NG
0	64876	0.0	0.0	$\pm 45.0$	OK
546	61184	547.3	1.3	$\pm 45.0$	OK
1004	58073	1008.5	4.5	$\pm 45.0$	OK
1486	54828	1489.6	3.6	$\pm 45.0$	OK
2121	50603	2116.0	-5.0	$\pm 45.0$	OK

### 4. Verification

Criteria of judgement : Residual error of the instrument light quantum at arbitrary point is within the acceptance value.

Acceptance:  $\pm 3.5\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Judgement
2132	2104.0	-28.0	$\pm 175.0$	Passed

Examined M. Kano

Approved A. Fukuoka

JFE Advantech Co., Ltd.

# Light Intensity Calibration Certificate

Model : DEF12-L  
 Serial No. : 0AQH012  
 Date : August 09, 2017  
 Location : Production Section  
 Method : Calibration equation is determined from linear regression of samples of the reference light quantum against A/D values. Samples are taken at approximately 0, 500, 1000, 1500, and 2000  $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ .

1. Equation Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ] = A+B × N N: A/D value

2. Coefficients A = +9.933032e+03 B = -1.530985e-01  
Immersion effect: 1.42

### 3. Calibration results

Acceptance:  $\pm 0.9\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	A/D value	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	OK/NG
0	64880	0.0	0.0	$\pm 45.0$	OK
528	61363	538.4	10.4	$\pm 45.0$	OK
989	58400	992.1	3.1	$\pm 45.0$	OK
1464	55294	1467.6	3.6	$\pm 45.0$	OK
2089	51279	2082.3	-6.7	$\pm 45.0$	OK

### 4. Verification

Criteria of judgement : Residual error of the instrument light quantum at arbitrary point is within the acceptance value.

Acceptance:  $\pm 3.5\%$  of full scale

Reference light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Instrument light quantum [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Residual error [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Acceptance [ $\mu\text{ mol}/(\text{m}^2\cdot\text{s})$ ]	Judgement
2060	1945.0	-115.0	$\pm 175.0$	Passed

Examined M. Kano  
Approved A. Fukuoaka

JFE Advantech Co., Ltd.

# CERTIFICATE OF CALIBRATION

Model Number: **LI-190SA QUANTUM SENSOR**

Serial Number: Q40966

Calibration Constant: 6.26

Calibration Multiplier: 159.74

Units: microamps per 1000  $\mu\text{mol s}^{-1} \text{m}^{-2}$

Units:  $\mu\text{mol s}^{-1} \text{m}^{-2}$  per microamp

Please consult the instruction manual for further information on the calibration constant and calibration multiplier. Recalibration is recommended every two years.

Date of Calibration: May 21, 2009

By: Cameron Deschane

**LI-COR**<sup>®</sup>

Biosciences

4421 Superior Street • P.O. Box 4425 • Lincoln, Nebraska 68504 USA  
Phone: 402-467-3576 • FAX: 402-467-2819  
Toll-free 1-800-447-3576 (U.S. & Canada)  
E-mail: envsales@licor.com  
www.licor.com

# CERTIFICATE of CALIBRATION

## for LI-COR SENSOR

Quantum Sensor  
Model Number: LI-190

Serial Number: Q47470

Calibration Date: **March 02, 2012**  
Manufacture Date: **March 01, 2012**

### Calibration Constant:

Output: 8.19 microamps per 1000  $\mu\text{mol s}^{-1} \text{m}^{-2}$

### For use with LI-COR handheld meters:

Multiplier: -122.04  $\mu\text{mol s}^{-1} \text{m}^{-2}$  per microamp

### For use with LI-COR 2290 (604 ohm) Millivolt Adapter:

Multiplier: -202.05  $\mu\text{mol s}^{-1} \text{m}^{-2}$  per millivolt

### If this is an SL sensor:

Multiplier: -200.0  $\mu\text{mol s}^{-1} \text{m}^{-2}$  per millivolt

**IMPORTANT:** Read the appropriate instruction manual (<http://www.licor.com/TSM>) before using this sensor.

**IMPORTANT:** It is recommended that sensors be recalibrated every two years.

Calibration Technician: *Aaron Qeshome*

Calibration standard used: Working standard lamp 797H.

Calibration traceable to the National Institute of Standards and Technologies (NIST) through NIST-calibration lamp number F-226.  
(NBS Test No. 534/237689-86)

**LI-COR**<sup>®</sup>

Biosciences

LI-COR Biosciences • Environmental • 4421 Superior Street • P.O. Box 4425 • Lincoln, NE 68504 USA  
Phone: (1) 402-467-3576 • Fax: 402-467-2819 • Toll-free: 800-447-3576 (USA & Canada)  
[envsales@licor.com](mailto:envsales@licor.com) • [envsupport@licor.com](mailto:envsupport@licor.com) • [www.licor.com](http://www.licor.com)  
Manual: <http://www.licor.com/TSM>

## Light Intensity

**MODEL** : MDS MKV/L

**SERIAL No** : 200341

**DATE** : 21-May-2010

**Location** : Calibration office of manufacture department at Kobe

**Method** : Light sensor is calibrated by 4 levels of light intensity ranging from 0 to 3000  $\mu\text{mol}/\text{m}^2\text{s}$  with each level difference about 1000  $\mu\text{mol}/\text{m}^2\text{s}$ . The outputs are computed by a linear regression against their corresponding reference readings from a standard light quantum meter.

**Reference device** : Light quantum meter ("LI-COR" Model: LI-189)

**Formula** : Light quantum ( $\mu\text{mol}/\text{m}^2\text{s}$ ) =  $A + B \times N$

$$A = \underline{-1.05326E+00}$$

$$B = \underline{1.05326E+00}$$

Immersion effect 0.00


Reference ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Output N	Calculated ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Error ( $\mu\text{mol}/\text{m}^2\text{s}$ )
0.0	1	0.0	0.0
503.0	462	485.6	-17.4
1036.0	962	1012.2	-23.8
2045.0	1934	2036.0	-9.0
3060.0	2922	3076.6	16.6

**Criteria for acceptability** :

1. The errors in above form must be within  $\pm 4\%$  FS
2. After writing the calibration coefficients into instrument, one point check at any level of light must agree with the accuracy declared by the instrument.

Reference ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Output ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Error ( $\mu\text{mol}/\text{m}^2\text{s}$ )
1440	1426	-14

**Judgement** : **Good**

Calibration group, 

Manufacture department at Kobe

JFE Advantech Co., LTD



## Light Intensity

**MODEL** : MDS MKV/L

**SERIAL No** : 200665

**DATE** : 21-May-2010

**Loaction** : Calibration office of manufacture department at Kobe

**Method** : Light sensor is calibrated by 4 levels of light intensity ranging from 0 to 3000  $\mu\text{mol}/\text{m}^2\text{s}$  with each level difference about 1000  $\mu\text{mol}/\text{m}^2\text{s}$ . The outputs are computed by a linear regression against their corresponding reference readings from a standard light quantum meter.

**Reference device** : Light quantum meter ("LI-COR" Model: LI-189)

**Formula** : Light quantum ( $\mu\text{mol}/\text{m}^2\text{s}$ ) =  $A + B \times N$

$$A = \underline{-1.13690\text{E}+00}$$

$$B = \underline{1.13690\text{E}+00}$$

Immersion effect 0.00

Reference ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Output N	Calculated ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Error ( $\mu\text{mol}/\text{m}^2\text{s}$ )
0.0	1	0.0	0.0
500.0	429	486.6	-13.4
1090.0	940	1067.5	-22.5
2033.0	1782	2024.8	-8.2
3100.0	2741	3115.1	15.1

**Criteria for acceptability** :

1. The errors in above form must be within  $\pm 4\%$  FS
2. After writing the calibration coefficients into instrument, one point check at any level of light must agree with the accuracy declared by the instrument.

Reference ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Output ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Error ( $\mu\text{mol}/\text{m}^2\text{s}$ )
1262	1251	-11

**Judgement** : **Good**

Calibration group,



Manufacture department at Kobe



JFE Advantech Co., LTD

## Light Intensity

**MODEL** : MDS MKV/L

**SERIAL No** : 200664

**DATE** : 21-May-2010

**Loaction** : Calibration office of manufacture department at Kobe

**Method** : Light sensor is calibrated by 4 levels of light intensity ranging from 0 to 3000  $\mu\text{mol}/\text{m}^2\text{s}$  with each level difference about 1000  $\mu\text{mol}/\text{m}^2\text{s}$ . The outputs are computed by a linear regression against their correspondir reference readings from a standard light quantum meter.

**Referece device** : Light quantum meter ("LI-COR" Model: LI-189)

**Formula** : Light quantum ( $\mu\text{mol}/\text{m}^2\text{s}$ ) =  $A + B \times N$

$$A = \underline{-8.17469E-01}$$

$$B = \underline{8.17469E-01}$$

Immersion effect 0.00

Reference ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Output N	Calculated ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Error ( $\mu\text{mol}/\text{m}^2\text{s}$ )
0.0	1	0.0	0.0
500.0	591	482.3	-17.7
1041.0	1261	1030.0	-11.0
2003.0	2445	1997.9	-5.1
3027.0	3716	3036.9	9.9

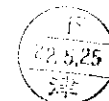
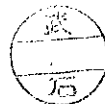
**Criteria for acceptability** :

1. The errors in above form must be within  $\pm 4\%$  FS
2. After writing the calibration coefficients into instrument, one point check at any level of light must agree with the accuracy declared by the instrument.

Reference ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Output ( $\mu\text{mol}/\text{m}^2\text{s}$ )	Error ( $\mu\text{mol}/\text{m}^2\text{s}$ )
1626	1612	-14

**Judgement** : **Good**

Calibration group,  
Manufacture department at Kobe



JFE Advantech Co., LTD



## PARs Calibration Sheet

Date: Mar. 27, 2009

Customer: SeaBird Elec.

S/N#: PARS-135

### Calibration Coefficients

	Analog	Digital
$I_m$	= 1.3589	= 1.3589
$a_1$	= 0.8946	= 2943.4639
$a_0$	= 1.3285	= 4374.0529

Equations:  $y = I_m * 10^{\frac{x-a_0}{a_1}}$  , if the sensor is immersed in water

$y = 1.0 * 10^{\frac{x-a_0}{a_1}}$  , if the sensor is not immersed

where,

PAR is  $y$ ,  $[y] = \mu\text{mol photons/m}^2/\text{s}$

Count is  $x$ ,  $[x] = \text{counts}$

For users of SEASOFT, Sea-Bird Electronics' data processing software, calibration coefficients are converted in accordance with Sea-Bird Electronics application note No. 11 QSP-L. The corresponding coefficients for use in SEASOFT are:

multiplier = 1.0 (in air)  
multiplier = 1.3589 (in water)

$M = 0.8946$

$B = 1.3285$

Calibration\_const =  $1.0 * 10^9$

offset = 0

PO Box 518  
620 Applegate St.  
Philomath OR 97370



(541) 929-5650  
Fax (541) 929-5277  
<http://www.wetlabs.com>

## PARs Calibration Sheet

Date: Mar. 27, 2009

Customer: SeaBird Elec.

S/N#: **PARS-134**

### Calibration Coefficients

	Analog	Digital
Im	= 1.3589	= 1.3589
a <sub>1</sub>	= 0.8902	= 2923.6435
a <sub>0</sub>	= 1.3145	= 4260.0842

Equations:  $y = Im * 10^{\frac{x-a_0}{a_1}}$ , if the sensor is immersed in water

$y = 1.0 * 10^{\frac{x-a_0}{a_1}}$ , if the sensor is not immersed

where,

PAR is  $y$ , [y] =  $\mu\text{mol photons/m}^2/\text{s}$

Count is  $x$ , [x] = counts

For users of SEASOFT, Sea-Bird Electronics' data processing software, calibration coefficients are converted in accordance with Sea-Bird Electronics application note No. 11 QSP-L. The corresponding coefficients for use in SEASOFT are:

multiplier = 1.0 (in air)

multiplier = 1.3589 (in water)

M = 0.8902

B = 1.3145

Calibration\_const =  $1.0 * 10^9$

offset = 0



PO Box 518  
620 Applegate St.  
Philomath, OR 97370



(541) 929-5650  
Fax (541) 929-5277  
[www.wetlabs.com](http://www.wetlabs.com)

## PARs Calibration Sheet

Date: 9/5/2014

S/N: PARSB-419

### PAR Scale Factor

**PAR =  $I_m \cdot 10((x - a_0)/a_1)$ , if the sensor is immersed in water**

**PAR =  $1.0 \cdot 10((x - a_0)/a_1)$ , if the sensor is not immersed**

Where,

PAR =  $\mu\text{mol photons/m}^2/\text{s}$

x

= counts

	Analog	Digital
<b><math>I_m</math></b>	1.3589	1.3589
<b><math>a_1</math></b>	0.893	2923
<b><math>a_0</math></b>	1.309	4266

For users of SEASOFT, Sea-Bird Electronics' data processing software, calibration coefficients are converted in accordance with Sea-Bird Electronics application note No. 11 QSP-L. The corresponding coefficients for use in SEASOFT are:

<b>multiplier</b>	<b>1</b>	In Air
<b>multiplier</b>	<b>1.359</b>	In Water
<b>M</b>	<b>0.893</b>	
<b>B</b>	<b>1.309</b>	
<b>Calibration_const</b>	<b><math>1.0 \cdot 10^9</math></b>	
<b>offset</b>	<b>0</b>	





# PAR Calibration Sheet

Date: 4/9/2020

S/N: PARSB-419

## PAR Scale Factor

$PAR = I_m * 10^{(x-a_0)/a_1}$  if the sensor is immersed in water

$PAR = 1.0 * 10^{(x-a_0)/a_1}$  if the sensor is not immersed

Where,

PAR =  $\mu\text{mol photons/m}^2/\text{s}$

x = counts

	Analog	Digital
<b>I<sub>m</sub></b>	1.3589	1.3589
<b>a<sub>1</sub></b>	0.886	2902
<b>a<sub>0</sub></b>	1.364	4442

For users of SEASOFT, Sea-Bird Electronics' data processing software, calibration coefficients are converted in accordance with Sea-Bird Electronics application note No. 11 QSP-L. The corresponding coefficients for use in SEASOFT are:

<b>multiplier</b>	<b>1</b>	In Air
<b>multiplier</b>	<b>1.359</b>	In Water
<b>M</b>	<b>0.886</b>	
<b>B</b>	<b>1.364</b>	
<b>Calibration_const</b>	<b>1.0*10^9</b>	
<b>offset</b>	<b>0</b>	

## Document Version Control and Change Register

<b>Version</b>	<b>Date</b>	<b>Change Description</b>	<b>Revision Authors</b>
1.0	13 June 2019	Original version	Harley et al.
2.0	18 Dec. 2020	Processed data through 2019 modified the Neighbour Test added comparison to FLNTUS chlorophyll added calculation of PAR Kd values	Peter Jansen and Tom Trull

## CONTACT US

**t** 1300 363 400  
+61 3 9545 2176  
**e** [csiroenquiries@csiro.au](mailto:csiroenquiries@csiro.au)  
**w** [www.csiro.au](http://www.csiro.au)

AT CSIRO, WE DO THE  
EXTRAORDINARY EVERY DAY

We innovate for tomorrow and help  
improve today – for our customers, all  
Australians and the world.

Our innovations contribute billions of  
dollars to the Australian economy  
every year. As the largest patent holder  
in the nation, our vast wealth of  
intellectual property has led to more  
than 150 spin-off companies.

With more than 5,000 experts and a  
burning desire to get things done, we are  
Australia's catalyst for innovation.

CSIRO. WE IMAGINE. WE COLLABORATE.  
WE INNOVATE.

## FOR FURTHER INFORMATION

**Oceans and Atmosphere**  
Peter Jansen  
**t** +61 3 6232 5094  
**e** [Peter.Jansen@csiro.au](mailto:Peter.Jansen@csiro.au)

**Oceans and Atmosphere**  
Thomas Trull  
**t** +61 3 6232 5069  
**e** [Tom.Trull@csiro.au](mailto:Tom.Trull@csiro.au)