



Inversion of marine gravity anomalies over southeastern China seas from multi-satellite altimeter vertical deflections



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ABSTRACT

The accuracy and resolution of marine gravity field derived from satellite altimetry mainly depends on the range precision and dense spatial distribution. This paper aims at modeling a regional marine gravity field with improved accuracy and higher resolution ($1' \times 1'$) over Southeastern China Seas using additional data from CryoSat-2 as well as new data from AltiKa. Three approaches are used to enhance the precision level of satellite-derived gravity anomalies. Firstly we evaluate a suite of published retracking algorithms and find the two-step retracker is optimal for open ocean waveforms. Secondly, we evaluate the filtering and resampling procedure used to reduce the full 20 or 40 Hz data to a lower rate having lower noise. We adopt a uniform low-pass filter for all altimeter missions and resample at 5 Hz and then perform a second editing based on sea surface slope estimates from previous models. Thirdly, we selected WHU12 model to update the corrections provided in geophysical data record. We finally calculated the $1' \times 1'$ marine gravity field model by using EGM2008 model as reference field during the remove/restore procedure. The root mean squares of the discrepancies between the new result and DTU10, DTU13, V23.1, EGM2008 are within the range of 1.8–3.9 mGal, while the verification with respect to shipboard gravity data shows that the accuracy of the new result reached a comparable level with DTU13 and was slightly superior to V23.1, DTU10 and EGM2008 models. Moreover, the new result has a 2 mGal better accuracy over open seas than coastal areas with shallow water depth.

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1. Introduction

Marine gravity anomalies are important data sources to construct Earth's gravity model and investigate global tectonics and continental margin structure, which can be derived from radar altimeter measurements of ocean surface height (Rapp, 1979; Haxby et al., 1983) or slope (Sandwell and Smith, 1997; Andersen and Knudsen, 1998; Hwang, 1998). The development of marine gravity field model mainly relies on the accuracy and resolution of accumulated multi-satellite altimeter data. The Southeastern China Seas, especially the South China Sea, have relatively complex seafloor topography, and these areas are both attractive for oceanographers and geodetic scientists. Over the past two decades, several regional marine gravity models over Southeastern China Seas have been constructed from satellite altimetry data (HSU et al., 1999; Li et al., 2001; Huang et al., 2001, 2006; Yang et al., 2008). However, the optimal resolution of inverted models was $2' \times 2'$, which is lower than the resolution of latest global mainstream models ($1' \times 1'$) such as DTU13 (Andersen et al., 2014)

and V23.1 (Sandwell et al., 2014). Moreover, these global models are not always optimal in coastal areas and complex regions with islands as it is well known that the quality of satellite-derived gravity data degrades close to the coast.

The quality of marine gravity field model derived from satellite altimeter is manifested on two aspects as accuracy and resolution, which mainly depends on the following factors: (1) the altimeter range precision (2) the spatial track density and along-track sampling rate (3) the diverse track orientation (4) the accuracy of modeled ocean tide corrections, especially over the coastal areas and (5) the low-pass filters applied to the profile data. The accuracy of altimeter observations can be improved through waveform retracking and careful low-pass filtering. Moreover, the requirement for density and diversity can be satisfied through along-track resampling and new data supplement with geodetic mission or different orbital parameters.

In recent years, the algorithms for retracking altimeter waveforms have gone through considerable development (Garcia et al., 2014), which provides great opportunity for improving the precision of existing altimeter data. Meanwhile, CryoSat-2 has accumulated large amount of observations for several complete 369 d cycles with different track orientations. Jason-1 implemented geodetic mission (GM) for

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Table 1
Correlation coefficient of range correction sequences for different retracking methods.

| MLE | OCOG | Threshold | Improved threshold | Beta-5 | WLS-1st-step | WLS-2nd-step |
|--------------------|------|-----------|--------------------|--------|--------------|--------------|
| MLE | 1 | 0.646 | 0.978 | 0.938 | 0.980 | 0.951 |
| OCOG | 1 | 0.656 | 0.622 | 0.641 | 0.667 | 0.640 |
| Threshold | | 1 | 0.959 | 0.962 | 0.945 | 0.967 |
| Improved threshold | | | 1 | 0.923 | 0.914 | 0.928 |
| Beta-5 | | | | 1 | 0.934 | 0.944 |
| WLS-1st-step | | | | | 1 | 0.963 |
| WLS-2nd-step | | | | | | 1 |

almost a complete 406.5 d period at the end of its operation stage as planned. Both the missions achieved the goal of dense spatial track, while the corresponding range precision is superior over the data of previous geodetic missions, such as Geosat and ERS-1. In addition, the measurements of SARAL/AltiKa have better range precision and higher resolution by increasing the operating frequency, pulse repetition frequency, bandwidth and reducing the beamwidth of the antenna pattern (Raney and Phalippou, 2011; Zhang and Sandwell, 2016). Combined with the existing altimeter data set, the new supplements of CryoSat-2, Jason-1 GM and SARAL/AltiKa in recent years provide a great opportunity of modeling improved marine gravity field due to

their diversified spatial track distribution and enhanced range precision (Sandwell et al., 2013; Smith, 2015; Zhang and Sandwell, 2016).

Therefore, this paper addresses the following questions over the Southeastern China Seas (100°–140°E, 0°–40°N): (1) Which retracker is optimal for range precision over the open ocean? (2) Which tidal model is more reliable? (3) Can one adjust processing and editing parameters to construct a regional marine gravity field with better accuracy and higher resolution than previous solutions? Eight high-precision radar altimeter missions (Geosat 1985–1989, ERS-1 1991–1998, T/P 1992–2006, ERS-2 1995–2011, Jason-1 2001–2013, Envisat 2002–2012, CryoSat-2 2010–present, SARAL/AltiKa 2013–present)

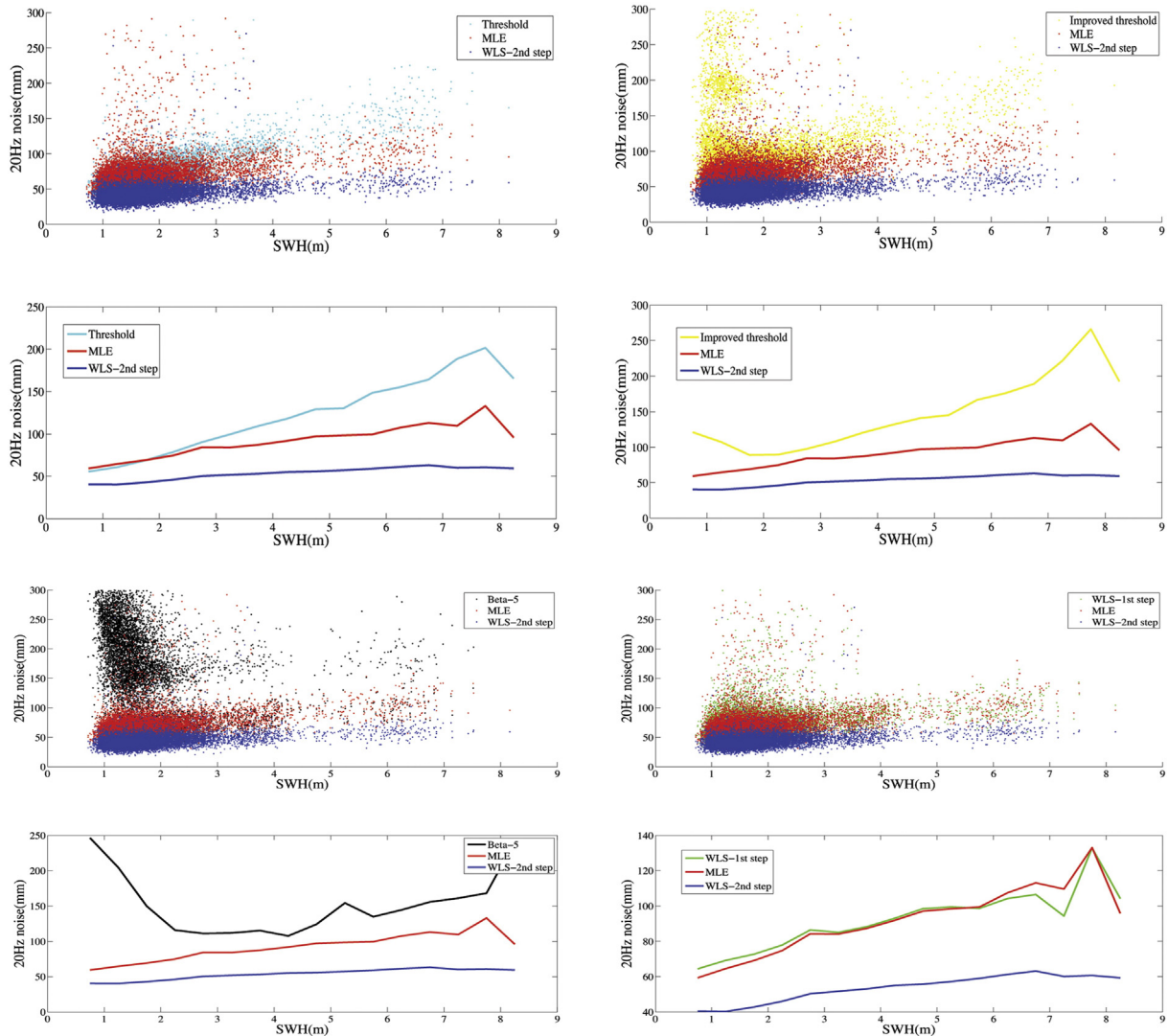


Fig. 1. Statistics of along-track standard deviation for different retracking methods (Threshold – cyan; MLE provided in SGDR – red; WLS-2nd step – blue Improved threshold – yellow; Beta-5 – black; WLS-1st step – green). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

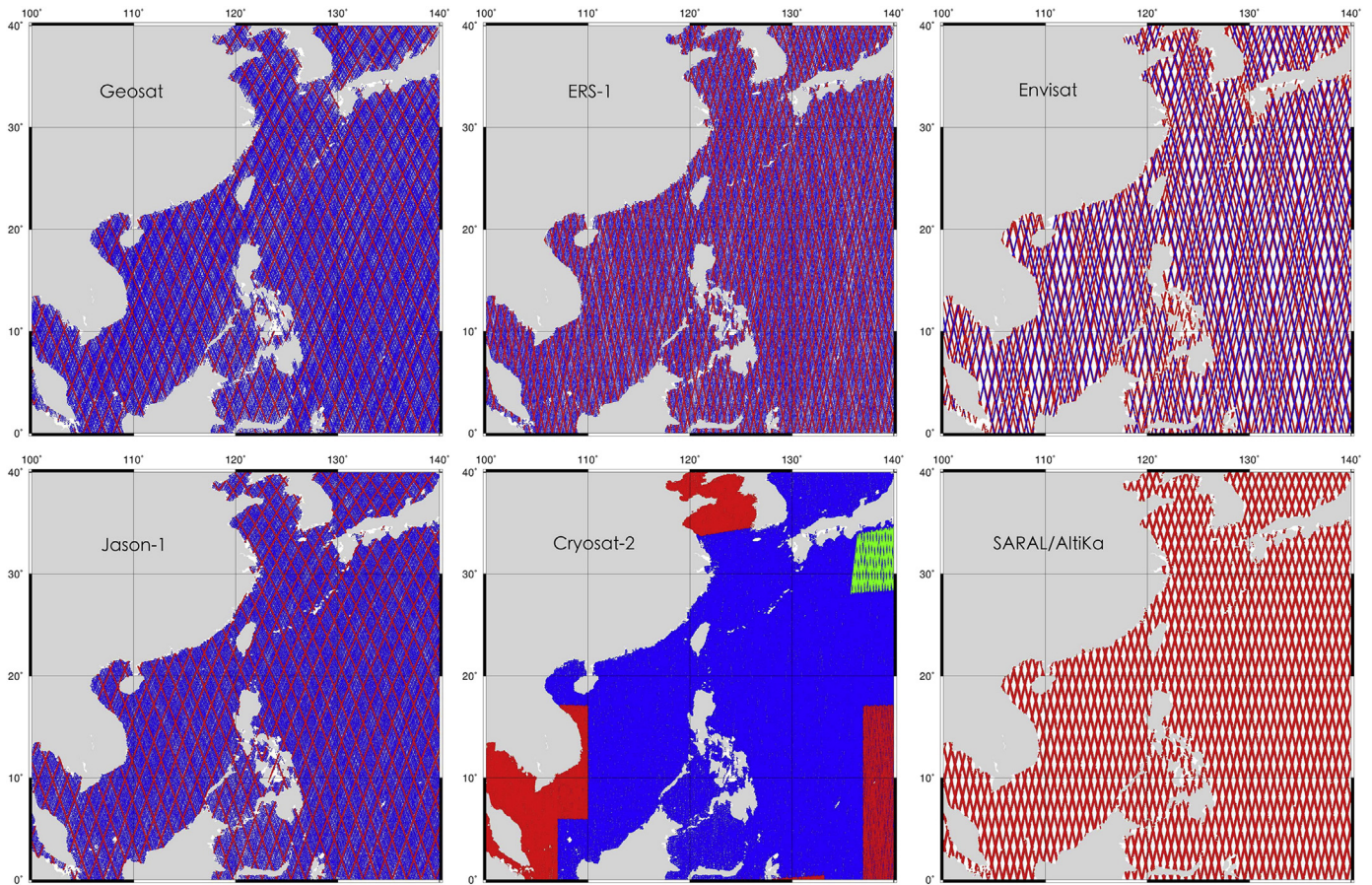


Fig. 2. Distribution of multi-satellite altimeter data in the research area.

have accumulated large amount of sea surface height (SSH) measurements. Based on the available altimeter data mentioned above, a new regional gravity model with $1' \times 1'$ resolution will be constructed and validated in the research area.

2. Retracker selection

A satellite altimeter measures the range to the land, ice, or ocean surface by emitting a series of frequency-modulated chirp signals designed to act like brief Gaussian-shaped radar pulses. These pulses interact with the surface and the received power of the reflected signal is recorded by the satellite altimeter over a short observation window equivalent to ~ 60 m of range. Averages of the power received from many echoes are referred to as altimeter waveforms. The leading edge of the waveform is crudely tracked onboard the satellite to keep the return pulse near the center of the window. The leading edge can be estimated more accurately (i.e. retracked) in post processing. A variety of waveform retracking algorithms have been proposed and the optimal algorithm depends on the slope and roughness of the reflective surface (land, ice, or ocean). The models can be purely empirical or based on physics (Sarrailh et al., 1997; Gommenginger et al., 2011). Here we evaluate a number of retracking algorithms to compare their

performance over open ocean surfaces. We expect the retracker that are optimized for land or ice will perform poorly over the ocean and our analysis confirms that expectation and provides an objective basis for the selection of the optimal retracker. Nevertheless we use these suboptimal retracker to provide a first estimate of the leading edge of the waveform to improve the convergence of the numerically slower Brown-model type retracker (Brown, 1977).

We begin with retracker that are optimized for ice and land surfaces, which are commonly rough and can have significant slope within the beamwidth of the radar footprint. The offset center of gravity (OCOG) algorithm was developed by Wingham et al. (1986) to achieve robust retracking and its goal is to find the center of gravity for each waveform based on the power levels within the gates. The threshold retracker was developed by Davis (1993) and this algorithm uses a prescribed threshold value with respect to the OCOG amplitude or the maximum waveform amplitude to determine the objective gate and improve the estimation of range. The improved threshold retracker has been developed in the case of complex waveforms to identify sub-waveforms within the measured waveform and select the best ranging gate (Hwang et al., 2006; Chang et al., 2006; Guo et al., 2010). The Beta-5 parameter retracker was developed by Martin et al. (1983) to retrieve ranges from the single-ramp return waveforms by fitting a 5-

Table 2
Parameters for Sandwell retracking method for multi-satellites altimeter data.

| Satellite mission | Geosat | ERS-1 | Envisat | T/P Jason-1 | CryoSat-2 LRM | CryoSat-2 SAR | CryoSat-2 SIN | SARAL/ AltiKa |
|-------------------|---------|---------|---------|----------------|------------------|------------------|------------------|------------------|
| α | 0.006 | 0.022 | 0.09 | 0.0058 | 0.013 | 0.00744 | 0.00744 | 0.0351 |
| Gate spacing/mm | 468.257 | 454.067 | 468.257 | 468.257 | 428.12 | 428.12 | 428.12 | 312.284 |

Note that α is the best trailing edge decay parameter in units of gates⁻¹.

parameter functional model. These purely empirical retrackerers perform well over surfaces where the shape of the return waveform is highly variable.

Over the open ocean the waveform shape is well approximated by a Brown-type model (Brown, 1977) which consists of a sharp error-function step in power with a more gradual decay in the trailing edge due to the finite beam width of the projected antenna pattern (Brown, 1977; Amarouche et al., 2004). For example, the maximum likelihood

estimator (MLE) is a statistical retracking method to fit the theoretical Brown model return power to the measured return power (Challenor and Scrocosz, 1989). This algorithm can use a 4-parameter Brown-type model to estimate arrival time, rise time, waveform amplitude and the rate of the decay of the trailing edge of the waveform and it is called MLE4. The MLE4 retracker is used to generate the standard product in the sensor geophysical data records (SGDR) of Jason-1. A modification of this algorithm was proposed by (Sandwell and Smith,

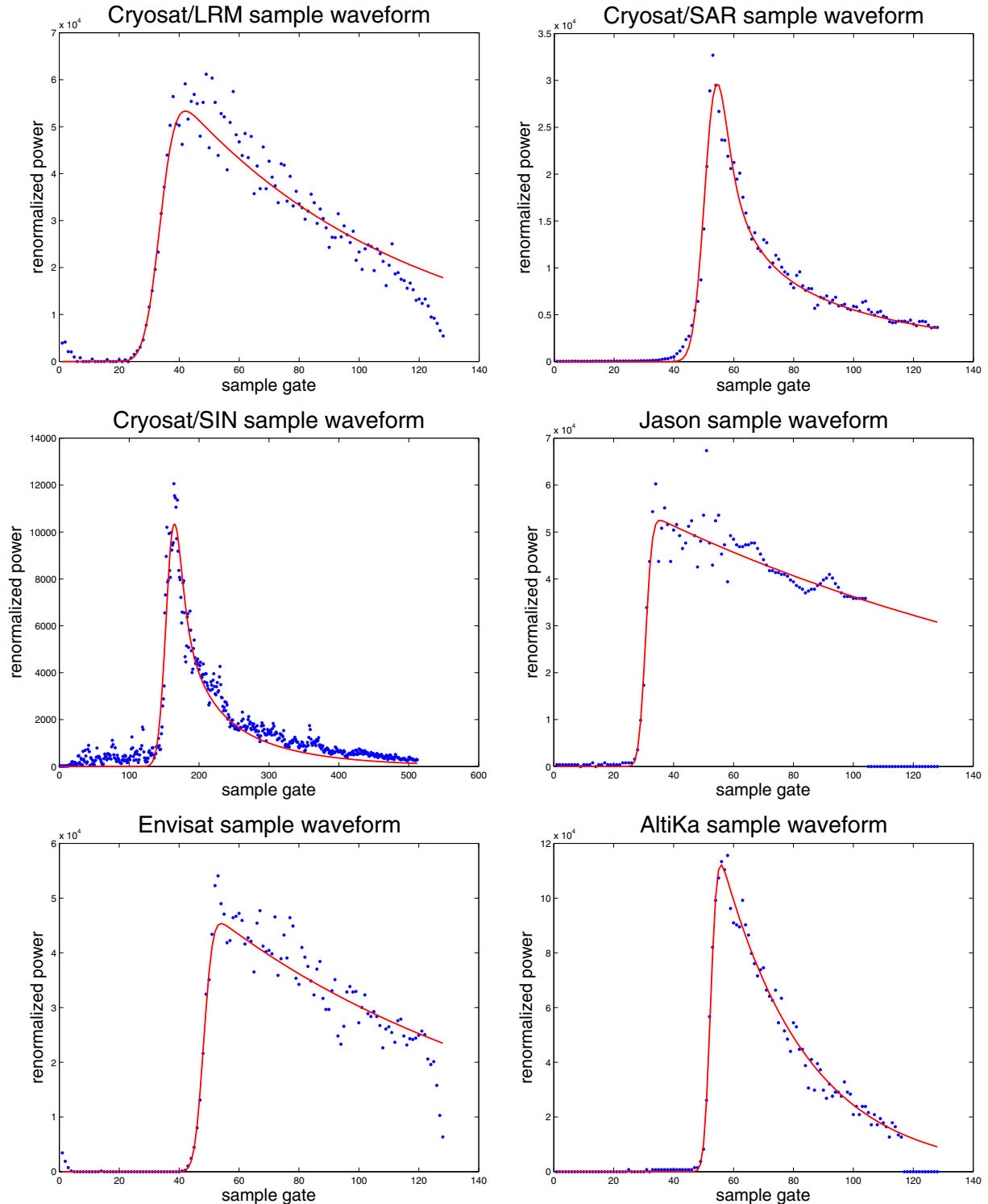


Fig. 3. Fitting results of typical waveforms using two-step WLS retracker for CryoSat-2, Jason-1, Envisat and SARAL/AltiKa. Note the CryoSat-2 SAR and SIN waveforms were retracked using a SAR waveform model (Garcia et al., 2014).

2005) to decouple the correlation between arrival time and significant wave height that occurs in the MLE4 algorithm. The decoupling is achieved by first performing a 3-parameter retracking assuming a constant trailing edge decay; we'll call this WLS-1st-step. Then the parameter representing the rise time (i.e. significant wave height or SWH) of the leading edge is smoothed over a $\frac{1}{2}$ wavelength of 45 km. A second retracking is performed using this smoothed rise time as a known parameter so the second-pass has only two parameters. This two-step approach has proved effective for most of the conventional radar altimeters (Garcia et al., 2014).

Two approaches were used to select the optimal retracking algorithm for recovery of the ocean surface height and slope. We evaluate all the retrackers using the 501st cycle of Jason-1 GM data. First we perform a regression between the arrival time of each pair of the 7 retrackers discussed above and calculate the correlation coefficient. The results are provided in Table 1. In general the arrival times from all the retrackers except the OCOG are highly correlated (>0.91). The 2-step, weighted least squares retracker (WLS-2nd) shows the best correlation with all the other retrackers suggesting it is optimal.

Second evaluation approach is to calculate the standard deviation of the 20 Hz range correction in 1 s bins for each of the 6 best retrackers (OCOG was not evaluated). After removal of the range from the EGM2008 model, the range correction should be constant over this short interval. These standard deviations should increase with increasing SWH as shown in Fig. 1. This process was repeated for retracked results of threshold (cyan dots), improved threshold (yellow dots), Beta-5 (black dots) and WLS-1st step (green dots) algorithms in contrast with results of WLS-2nd step (blue dots) and MLE (red dots) methods. The smoothed curves in Fig. 1 represent the average values of statistical standard deviations corresponding to the 0.5 m bins of SWH. The lowest value of the standard deviations derived from WLS-2nd step retracker (blue dots and blue line) means the minimum noise level comparing with other retracking algorithms, which proves the advantage of the two-step WLS retracker for constraining noise level and recovering optimal gravity field. Besides, this two-step WLS retracker is suitable for all the conventional altimeter data and brings obvious improvements in range precision (Sandwell and Smith, 2005, 2009; Garcia et al., 2014; Zhang and Sandwell, 2016). Therefore, the two-step WLS retracker is selected for waveforms of different altimeter missions to construct gravity field model in this paper.

3. Gravity field model construction

The main objective of our analysis is to construct a grid of marine gravity anomalies from satellite altimeter profiles of ocean surface height. The ocean surface is a close approximation to the geoid height (gravitational potential) and the gravity anomaly is the vertical derivative of the geoid. Since we are not interested in constructing the geoid, we perform the derivative directly on the raw altimeter profiles. These along-track slopes are combined in a biharmonic spline analysis to construct east and north grids of sea surface slope and then into gravity anomalies using Laplace's equation (e.g., Sandwell, 1984;

Table 3
Along-track standard deviation for retracked altimeter data under sea state conditions of 2 m (typical) and 6 m Unit: mm.

| Satellite mission | 1st step@2 m | 2nd step@2 m | 1st step/2nd step@2 m | 2nd step@6 m |
|-------------------|--------------|--------------|-----------------------|--------------|
| Geosat | 88.0 | 57.0 | 1.54 | 105.4 |
| ERS-1 | 93.6 | 61.8 | 1.51 | 111.8 |
| Envisat | 78.9 | 51.8 | 1.52 | 88.6 |
| Jason-1 | 75.9 | 46.4 | 1.63 | 64.2 |
| CryoSat-2/LRM | 64.7 | 42.7 | 1.51 | 71.7 |
| CryoSat-2/SAR | 49.5 | 49.7 | 0.996 | 110.9 |
| CryoSat-2/SIN | 138.5 | 138.7 | 0.998 | 148.6 |
| SARAL/AltiKa | 45.8 | 26.3 | 1.74 | 46.2 |

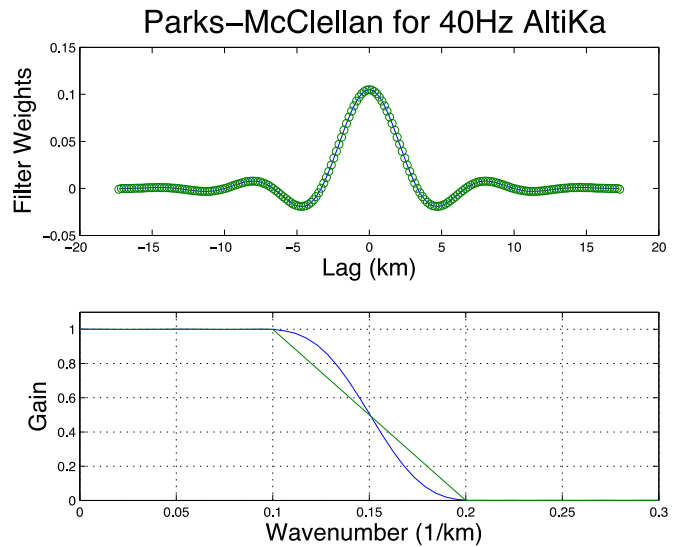


Fig. 4. Low-pass filter designed for SARAL/AltiKa and its impulse response in space domain.

Hwang, 1998; Sandwell and Smith, 2009). As discussed in Olgati et al. (1995) there are significant computational and accuracy benefits to constructing gravity from along-track slopes rather than first constructing a geoid model and then differentiating to obtain gravity. Moreover, factors that affect the absolute height accuracy of altimetric sea level such as radial orbit error, ionosphere/troposphere delays and deep ocean tides (Chelton et al., 2001) have correlation scales long enough that they yield negligible error in along-track slope (Sandwell and Smith, 2009). The conversion of vertical deflections to gravity anomalies is a boundary-value problem for Laplace's equation (Sandwell and Smith, 1997). The most accurate computations use spherical harmonics at long wavelengths, supplemented by Fourier transforms on data projected onto a flat plane for short wavelengths (Sandwell and Smith, 2009). This method meets the requirement of gravity field accuracy and omits the construction of complex kernel function at the same time. As a result, we follow this standard practice in geodesy known as “remove-restore” to construct the regional marine gravity model and the referred gravity model is EGM2008 in this paper.

We use all available altimeter data including: Geosat GM&ERM, ERS-1 GM&ERM, T/P, Envisat and Jason-1 ERM, CryoSat-2, Jason-1 GM and SARAL/AltiKa data to construct the regional marine gravity field

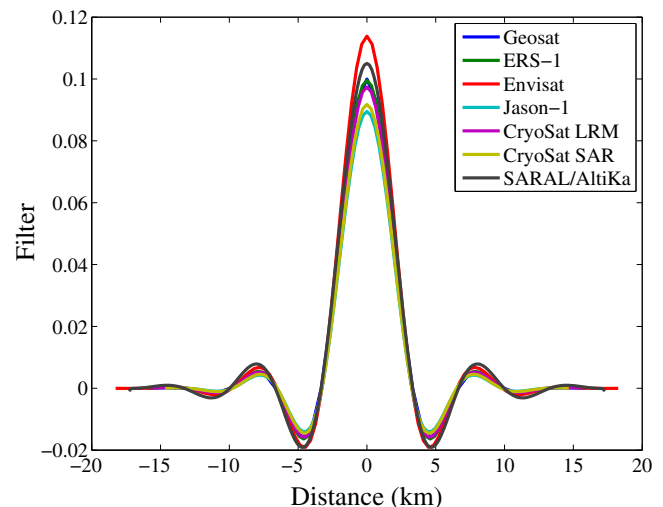


Fig. 5. Low-pass filters used in the resampling procedure for multi-satellite altimeters.

Table 4

Time-space interval before and after the resampling process for multi-satellite altimeters.

| Satellite missions | Velocity(m/s) | dt1(s) | dt2(s)/5 Hz | dx1(m) | dx2(m)/5 Hz |
|--------------------|---------------|--------|-------------|--------------|-------------|
| Geosat | 6770 | 0.098 | 0.196 | 663.5(10 Hz) | 1326.9 |
| ERS-1 | 6690 | 0.049 | 0.196 | 327.9 | 1312.0 |
| Envisat | 6690 | 0.055 | 0.222 | 372.6(18 Hz) | 1490.5 |
| Jason-1 | 5740 | 0.051 | 0.204 | 292.6 | 1170.4 |
| CryoSat-2/LRM | 6779 | 0.047 | 0.188 | 319.8 | 1279.2 |
| CryoSat-2/SAR | 6779 | 0.044 | 0.176 | 299.8 | 1197.3 |
| CryoSat-2/SIN | 6779 | 0.044 | 0.176 | 299.3 | 1193.8 |
| SARAL/AltiKa | 6690 | 0.026 | 0.209 | 174.7(40 Hz) | 1397.9 |

Table 5

Discrepancy value of 4 main components of ocean tide with respect to 137 tide gauges data Unit: cm.

| Tide model | M2 | S2 | K1 | O1 |
|------------|-------|-------|------|------|
| FES2004 | 28.99 | 14.86 | 5.38 | 4.14 |
| GOT4.7 | 24.75 | 13.20 | 3.26 | 4.26 |
| EOT10a | 28.50 | 15.20 | 4.70 | 3.57 |
| DTU10 | 21.22 | 12.08 | 3.97 | 3.19 |
| WHU12 | 17.88 | 11.03 | 3.62 | 2.72 |

model. Data distribution of multi-satellite altimeters over the South-eastern China Seas is shown in Fig. 2.

The Geosat, ERS-1 and Jason-1 data can all be divided into two categories - exact repetitive mission (red spots in Fig. 2) and geodetic mission (blue spots in Fig. 2) respectively. The T/P data has same distribution comparing to Jason-1 ERM data and the corresponding subfigure for Jason-1 does not distinguish them accordingly. In addition, Envisat does not include geodetic phase but have two phases of exact repetitive mission with different periods of 35 d (red spots in Fig. 2) and 30 d (blue spots in Fig. 2) separately. Moreover, CryoSat-2 has three measurement modes including the low-resolution mode (LRM, blue spots in Fig. 2), the synthetic aperture mode (SAR, red spots in Fig. 2) and the synthetic aperture interferometer mode (SIN, green spots in Fig. 2).

Based on the previous analysis in Section 2, the two-step WLS retracker was selected for retracking raw waveforms of various altimeter missions except CryoSat-2 SAR and SIN data which do not benefit from two-step retracking (Garcia et al., 2014). The corresponding parameters for different missions are provided in Table 2 and the fitting results for typical waveforms of CryoSat-2, Jason-1, Envisat and SARAL/AltiKa are shown in Fig. 3, demonstrating that the chosen parameters obtained reliable agreement between sample power values and the fitting modeled power values.

To assess the noise level of retracked data, we performed the statistical analysis of along-track standard deviations again as previously mentioned in Section 2. Under the typical condition of 2 m and 6 m SWH, mean values of standard deviations in 0.5 m SWH bins are listed in Table 3 (Garcia et al., 2014). The results demonstrate that the noise level of 2nd step retracked data by WLS estimator is significantly lower than the 1st step retracked results for most of satellite missions except CryoSat-2 SAR and SIN. The SAR and SIN mode data do not benefit from the 2nd step of WLS retracker as the arrival time and SWH are not strongly correlated during the least squared fitting process due to the more complex shape of waveforms. Moreover, the major

difference between 2nd step result and 1st step result is that the former procedure adopts along-track smoothed SWH as priori information rather than a parameter to be solved, which brings significantly improvement over the accuracy level as a factor of 1.5. It is remarkable that the retracked Ka-band data of SARAL/AltiKa has an obviously lower noise level compared to most of Ku-band retracked results. The precision dominance of Ka-band data is also mentioned by several publications (Raney and Phalippou, 2011; Smith, 2015).

The shortest wavelength that can be resolved in radar altimeter data is about 10 km (Marks and Smith, 2016). The spacing of the altimeter points at 20 Hz (40 Hz for AltiKa) sampling rate is ~350 m so we would like to downsample the data to ~5 Hz or about 1.4 km before computing the along-track sea surface slope. Prior to downsampling we apply a low-pass filter with a 0.5 gain at a wavelength of 6.7 km. For each satellite, the filter was designed in Matlab using the Parks-McClellan algorithm. Taking SARAL/AltiKa for example, the filter rolls off nearly linearly over a band from 10 km to 5 km (Fig. 4 lower). The detailed impulse response for the filter is shown in Fig. 4. Besides, the corresponding low-pass filters designed for different missions are plotted for a comparison in Fig. 5 according to their time-space intervals listed in Table 4. The lengths of along-track data series involved in the low-pass filter are 49, 99, 99 and 199, corresponding to along-track measurements with highest available data rate of 10 Hz, 18 Hz, 20 Hz and 40 Hz, respectively.

On the basis of processed range observations after waveform retracking and resampling, the SSH are computed for along-track 5 Hz sampling rate by considering corresponding corrections for path delay and geophysical environment effects. Among them, the ocean tide model errors are the major error sources for calculating sea surface height slopes (Sandwell and Smith, 2009). Therefore, all the corrections for path delay and geophysical environment are considered using items supplied by level 2 products during this procedure except the ocean tide.

The GOT4.7 model is the result of an empirical harmonic analysis of satellite altimetry relative to an adopted prior model, and follows the long series of similar efforts starting with Schrama and Ray (1994). FES2004 is one version of a series of finite element solutions tidal atlases, computed from tidal hydrodynamic equations and data assimilation (Lyard et al., 2006). The DTU10 model is based on an empirical correction to the FES2004, in which the largest residual tides were determined using the response method (Cheng and Andersen, 2011). EOT10a is a global solution for harmonic constants of the most dominant ocean tide constituents, derived by means of empirical analysis for multi-mission satellite altimetry data (Savcenko and

Table 6

Threshold for editing gross errors for multi-satellite altimeter along-track slopes Unit: m/s.

| Satellite missions | Geosat | ERS-1 | Envisat | T/P | Jason-1 | CryoSat-2 LRM | CryoSat-2 SAR | CryoSat-2 SIN | SARAL/AltiKa |
|--------------------|--------|-------|---------|-------|---------|---------------|---------------|---------------|--------------|
| Threshold | 25 | 30 | 33 | 20 | 28 | 31 | 35 | 48 | 30 |
| Delete percentage | 1.36% | 1.54% | 0.86% | 1.85% | 1.10% | 0.96% | 2.21% | 0.64% | 1.10% |

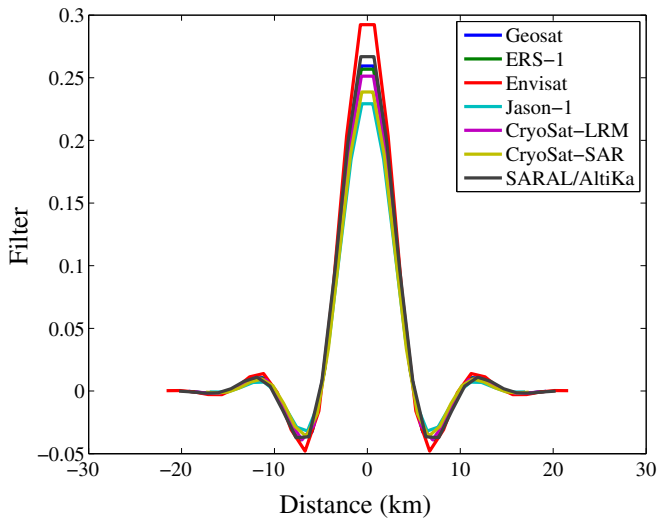


Fig. 6. Low-pass filters used for along-track slopes of multi-satellite altimeters.

Bosch, 2008). The recently published WHU12 is an empirical ocean tide model determined directly using an orthogonal representation of the response analysis without a background ocean tide model as a priori model. Comparing with 137 tide gauges data, the verification for 4 main components of ocean tide show that the WHU12 model has reliable accuracy level over China coastal areas as listed in Table 5. It is a reliable way to evaluate the accuracy of different models based on a comprehensive tide gauge data sets for tidal constituents (Stammer et al., 2014). As a result, we uniformly adopt WHU12 model to calculate the ocean tidal corrections for uniformly along-track 5 Hz measurement of different satellite missions.

After that, the along-track sea surface height gradients are computed, while along-track gradient of EGM2008 model are also interpolated for a preliminary verification. Our edit threshold of discrepancy between the two gradients was set at three times the standard deviation given in Table 6. This prior model furnishes a sanity check that allows us to detect outliers that produce spurious slopes. The corresponding proportions of eliminated data are also provided in Table 6. Considering that the high frequency noise is amplified during the process of

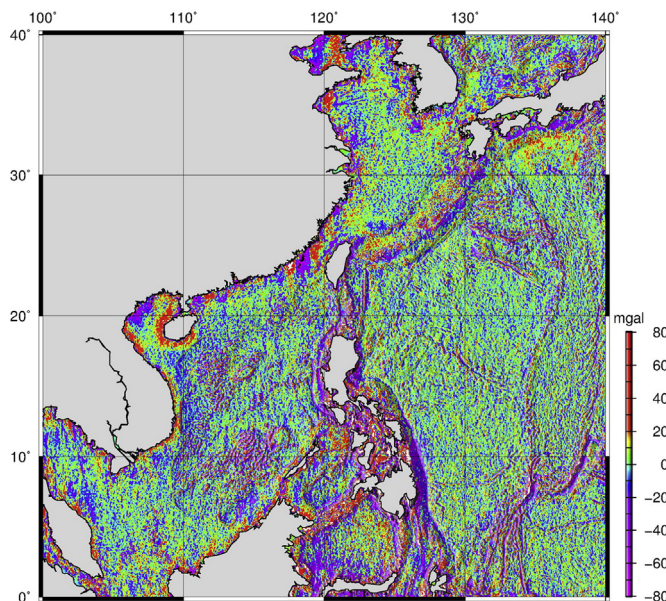


Fig. 7. Residual gravity anomaly in the research area.

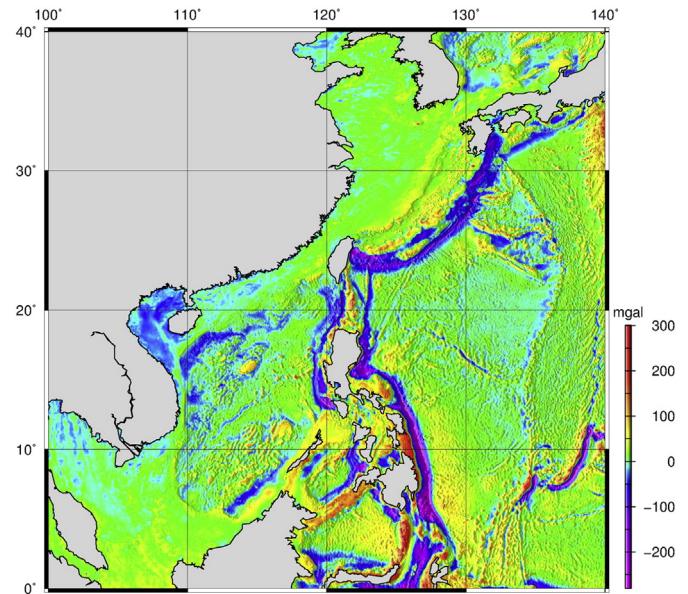


Fig. 8. Marine gravity field in the research area.

difference, we used a second low-pass filter according to the principle of a 0.5 gain at 10 km wavelength. The designed Parks-McClellan filters for various missions are shown in Fig. 6 and the lengths are uniformly set to be 30.

After the above steps, along-track filtered sea surface height gradients data are obtained for multi-satellite altimeters. Considering the effect of sea surface topography and geoid height, DOT2008A and EGM2008 model are selected respectively to interpolate and subtract from along-track 5 Hz observations. Then along-track residual vertical deflections are calculated according to velocity formulas at ground track (Sandwell and Smith, 1997). The relationship between along-track residual vertical deflections and 2-dimensional components of residual vertical deflections can be established as equations at each grid point with $1' \times 1'$ resolution. Consequently, the north and east components of residual vertical deflection are calculated using biharmonic splines with a tension parameter of 0.25 (Wessel and Bercovici, 1998), and then the residual gravity anomaly values shown in Fig. 7 on the basis of Laplace Equation and the Fast Fourier Transform (FFT) algorithm. A third low-pass filter having a 0.5 gain at 16 km is applied during this transformation. At last, the gravity anomaly values of EGM2008 model should be restored. We finally construct the $1' \times 1'$ marine gravity field model over Southeastern China Seas (Fig. 8).

4. Discussion

The resulting gravity anomaly grid is evaluated using two techniques. First, we examine the root mean square (RMS) misfit between the result and authoritative global marine gravity field models

Table 7
Validation information of inversed result with published gravity models Unit: mGal.

| Model description | Minimum | Maximum | Mean | RMS |
|-----------------------|----------|---------|--------|-------|
| New result VS DTU10 | -113.823 | 114.001 | -0.037 | 3.676 |
| New result VS DTU13 | -113.623 | 108.358 | -0.029 | 3.553 |
| New result VS V23.1 | -147.000 | 252.399 | -0.044 | 1.869 |
| New result VS EGM2008 | -106.862 | 108.198 | -0.024 | 3.901 |
| V23.1 VS DTU10 | -240.380 | 128.644 | 0.026 | 4.030 |
| V23.1 VS DTU13 | -186.643 | 127.894 | 0.023 | 3.811 |
| V23.1 VS EGM2008 | -178.061 | 124.937 | 0.028 | 4.144 |
| DTU13 VS DTU10 | -90.598 | 101.300 | 0.003 | 3.134 |
| DTU13 VS EGM2008 | -38.428 | 53.118 | -0.005 | 1.807 |
| DTU10 VS EGM2008 | -107.151 | 94.952 | 0.002 | 2.746 |

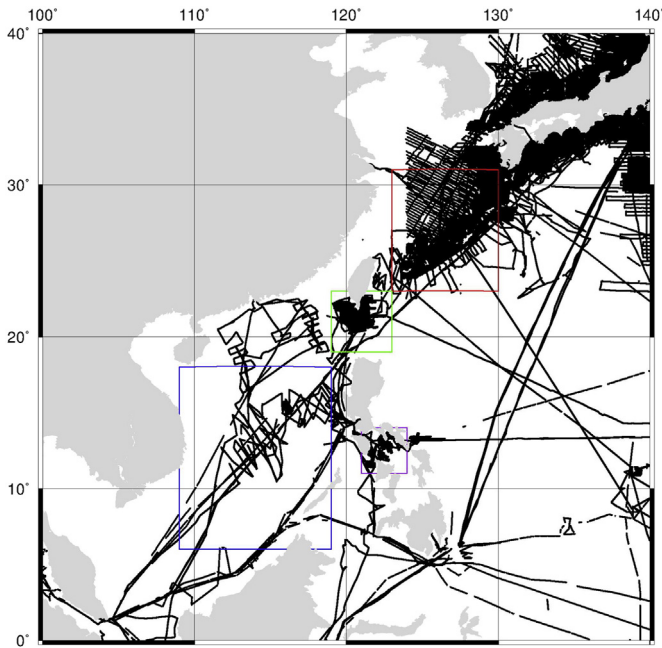


Fig. 9. Trajectory of NGDC ship-measured gravity data in the research area.

such as DTU10, DTU13, V23.1 and EGM2008. Second, we compare the result with gravity anomalies collected by ships. This comparison provides a more independent assessment of data accuracy but is limited to certain areas in which the high-quality shipboard data are available.

The statistical results with global models such as DTU10, DTU13, V23.1 and EGM2008 are provided in Table 7. The discrepancies between the new result and other 4 models are relatively small and the RMS values are within the range of 1.8– 3.9 mGal. Among them, the new result gets better accordance with V23.1 model due to the similar method for constructing marine gravity field model from along-track vertical deflections. Besides, the DTU series models agree better with EGM2008 model because of the data intersection with DNSC model while constructing EGM2008 model. Benefiting from the new-added altimeter data such as SARAL/AltiKa, the new result gets a better accuracy if we recognize DTU10, DTU13 and EGM2008 models as standard reference.

Moreover, the US National Geophysical Data Center (NGDC) provides globally distributed shipboard data and 117 tracks among them locate in the research area as shown in Fig. 9. We firstly computed the statistical information for these shipboard data cruise by cruise with respect to EGM2008 model and provided these preliminary evaluations in Table 8. Taking cruise 01010260 (28,392 observations) and 67010136 (24,462 observations) for instance, the mean values of discrepancies are 19.03 mGal and –12.88 mGal respectively while the RMS of discrepancies are 8.08 mGal and 5.6 mGal respectively. The verification with respect to the two cruises without considering the system bias will obtain inappropriate results of mean value (4.28 mGal) and RMS value (17.40 mGal). If we adapt a further step to eliminate the system bias

Table 8
Validation information of shipboard data with respect to EGM2008 model for each cruise Unit: mGal.

| Cruise | Mean | RMS | Cruise | Mean | RMS | Cruise | Mean | RMS | | | |
|--------|----------|--------|--------|------|----------|--------|-------|-----|----------|--------|-------|
| 1 | 01010258 | 7.90 | 8.94 | 2 | 01010259 | 21.11 | 7.07 | 3 | 01010260 | 19.03 | 8.08 |
| 4 | 02010055 | -3.41 | 2.99 | 5 | 02010079 | -4.13 | 3.73 | 6 | 03010016 | -2.50 | 10.03 |
| 7 | 06780070 | -1.88 | 8.11 | 8 | 08020049 | -5.93 | 12.72 | 9 | 08020071 | -3.58 | 6.29 |
| 10 | 08020072 | -4.04 | 11.97 | 11 | 15020205 | -2.09 | 4.55 | 12 | 15020206 | -5.42 | 5.83 |
| 13 | 15020207 | -1.39 | 3.76 | 14 | 15040215 | 0.22 | 5.80 | 15 | 16010004 | 9.05 | 11.41 |
| 16 | 16010007 | -5.64 | 6.27 | 17 | 29020003 | 0.13 | 9.49 | 18 | 29040003 | -5.48 | 9.33 |
| 19 | 29044004 | -7.82 | 24.93 | 20 | 29040006 | -4.80 | 7.07 | 21 | 29040007 | -15.24 | 15.31 |
| 22 | 29040008 | 13.41 | 9.62 | 23 | 29040009 | -18.79 | 5.51 | 24 | 29040010 | -17.48 | 4.07 |
| 25 | 29040018 | -12.97 | 3.11 | 26 | 29140001 | 4.57 | 15.09 | 27 | 67010135 | 352.77 | 38.09 |
| 28 | 67010136 | -12.88 | 5.60 | 29 | 67010137 | -0.05 | 7.67 | 30 | 67010138 | 1.87 | 8.55 |
| 31 | 67010139 | 199.44 | 7.81 | 32 | 67010140 | -1.04 | 7.15 | 33 | 67010141 | -1.69 | 6.52 |
| 34 | 67010142 | -5.28 | 12.88 | 35 | 67010143 | 16.17 | 3.54 | 36 | 67010145 | 3.26 | 7.06 |
| 37 | 67010146 | -2.90 | 6.61 | 38 | 67010147 | -0.97 | 6.48 | 39 | 77030001 | -8.12 | 14.63 |
| 40 | 77030003 | -12.41 | 13.32 | 41 | 77990001 | 4.55 | 15.10 | 42 | J1010001 | -26.85 | 23.53 |
| 43 | J1010036 | -4.95 | 7.46 | 44 | J1010037 | 1.79 | 8.16 | 45 | J1010038 | -1.03 | 6.89 |
| 46 | J1010039 | -0.09 | 6.88 | 47 | J1020001 | -0.94 | 8.99 | 48 | J1020002 | 2.01 | 7.00 |
| 49 | J1020003 | 2.24 | 6.13 | 50 | J1020006 | 7.87 | 7.50 | 51 | J1020007 | 2.90 | 6.08 |
| 52 | J1020008 | 4.97 | 7.45 | 53 | J1020009 | -4.07 | 7.30 | 54 | J1020010 | 3.98 | 8.16 |
| 55 | J1020011 | -5.96 | 7.76 | 56 | J1020012 | -2.92 | 5.64 | 57 | J1020016 | -0.19 | 6.67 |
| 58 | J1020021 | -4.85 | 7.46 | 59 | J1020022 | -5.27 | 5.88 | 60 | J1020024 | -1.96 | 6.91 |
| 61 | J1020026 | 6.57 | 7.07 | 62 | J1020027 | 5.18 | 6.68 | 63 | J1020029 | -2.61 | 8.40 |
| 64 | J1020030 | -5.27 | 8.63 | 65 | J1020031 | -2.96 | 10.61 | 66 | J1020032 | -2.56 | 8.42 |
| 67 | J1020033 | -6.18 | 5.87 | 68 | J1020038 | 0.87 | 5.46 | 69 | J1030002 | -2.13 | 9.98 |
| 70 | J1030007 | -11.90 | 13.24 | 71 | J1030008 | -5.95 | 5.56 | 72 | J1030009 | -3.49 | 7.60 |
| 73 | J1030010 | -0.16 | 7.27 | 74 | J1030024 | -8.91 | 8.72 | 75 | J1030025 | -4.26 | 5.43 |
| 76 | J1030027 | -2.24 | 5.66 | 77 | J1030028 | -1.01 | 7.22 | 78 | J1030030 | -1.27 | 7.41 |
| 79 | J1030031 | -2.25 | 9.38 | 80 | J1030033 | -8.63 | 4.81 | 81 | J1030034 | -10.99 | 13.65 |
| 82 | J2010002 | 0.04 | 15.07 | 83 | J2010003 | -1.31 | 15.85 | 84 | J2010004 | 1.21 | 13.15 |
| 85 | J2010005 | -0.87 | 9.95 | 86 | J2010008 | -5.35 | 41.68 | 87 | J2010009 | -6.34 | 10.88 |
| 88 | J2010010 | -0.19 | 11.88 | 89 | J2010011 | 2.83 | 23.10 | 90 | J2010012 | 1.82 | 10.26 |
| 91 | J2010013 | -2.20 | 35.39 | 92 | J2010014 | -0.98 | 9.03 | 93 | J2010015 | 2.56 | 9.31 |
| 94 | J2010027 | 0.15 | 6.00 | 95 | J2010028 | 0.29 | 4.53 | 96 | J2010029 | 0.81 | 5.54 |
| 97 | J2010030 | -0.08 | 3.40 | 98 | J2010031 | 0.61 | 5.29 | 99 | J2010032 | 0.55 | 6.24 |
| 100 | J2010033 | -1.08 | 5.41 | 101 | J2010034 | -0.35 | 5.78 | 102 | J2010035 | -0.65 | 5.43 |
| 103 | J2010036 | 1.10 | 5.65 | 104 | J2010037 | -0.18 | 5.46 | 105 | J2010038 | 0.23 | 6.37 |
| 106 | J2010039 | 0.46 | 4.03 | 107 | Ja010001 | -5.11 | 17.66 | 108 | Ja010004 | 12.24 | 22.57 |
| 109 | Ja010005 | -0.78 | 10.08 | 110 | Ja010006 | -7.30 | 11.67 | 111 | Ja010008 | -1.53 | 8.51 |
| 112 | Ja010009 | 0.64 | 73.63 | 113 | Ja010013 | -5.60 | 12.58 | 114 | Ja010019 | -8.81 | 5.89 |
| 115 | Ja010025 | 3.80 | 3.40 | 116 | Ja010026 | -11.39 | 6.37 | 117 | Ja010029 | 0.69 | 5.45 |

Table 9
Validation information of inversed result with NGDC shipboard gravity data Unit: mGal.

| Shipboard data description | Validate data | Minimum | Maximum | Mean | RMS |
|----------------------------|-------------------------|---------|---------|--------|-------|
| ALL (3.17%) | New result VS shipboard | −40.078 | 71.381 | −0.097 | 6.043 |
| | EGM2008 VS shipboard | −19.999 | 19.999 | 0.131 | 6.273 |
| | DTU10 VS shipboard | −26.886 | 27.643 | 0.140 | 6.247 |
| | DTU13 VS shipboard | −31.972 | 33.281 | 0.139 | 5.969 |
| | V23.1 VS shipboard | −42.594 | 83.899 | −0.122 | 6.108 |
| Coastal area (<100 m) | New result VS shipboard | −39.969 | 47.336 | 1.432 | 7.678 |
| | EGM2008 VS shipboard | −19.997 | 19.977 | 1.662 | 7.108 |
| | DTU10 VS shipboard | −23.881 | 21.706 | 1.651 | 7.211 |
| | DTU13 VS shipboard | −26.673 | 28.141 | 1.870 | 7.279 |
| | V23.1 VS shipboard | −35.391 | 58.192 | 1.293 | 7.696 |
| Open sea (>3000 m) | New result VS shipboard | −32.055 | 25.172 | 0.240 | 5.445 |
| | EGM2008 VS shipboard | −19.995 | 19.999 | 0.445 | 5.642 |
| | DTU10 VS shipboard | −23.676 | 22.073 | 0.466 | 5.596 |
| | DTU13 VS shipboard | −28.444 | 25.258 | 0.390 | 5.534 |
| | V23.1 VS shipboard | −32.303 | 25.201 | 0.262 | 5.432 |

for the two cruises, the corresponding mean value and RMS are respectively 0.0001 mGal and 7.04 mGal, which are more reasonable. Meanwhile, these ship-measured data inevitably contain certain number of gross error data limited to various measuring conditions.

Consequently these shipboard gravity data need extra procedures to eliminate system bias and delete gross error data according to the preliminary evaluations with respect to EGM2008, while the threshold of 20 mGal leads to a total proportion of 3.17% for deleted data. Then these shipboard data were used for a more reasonable verification. Besides, we also counted the statistical results for shipboard data of which water depths are either larger than 3000 m or smaller than 100 m on the basis of values interpolated from ETOPO1 model. The verifications with respect to ship-measured gravity data are all provided in Table 9, which demonstrate that the new result reaches the accuracy level of DTU13 and V23.1, also is superior to DTU10 and EGM2008. In addition, the accuracy of calculated result over open seas is almost 2 mGal better than the result over coastal area with a shallow water depth.

Considering the effect of complicated submarine topography and sea surface topography, we selected typical regions over the research area for a further comparison. The selected 4 rectangular areas are South China Sea Basin (blue rectangular in Fig. 9), sea areas off Taiwan's southern coast (green rectangular in Fig. 9), Okinawa through and its adjacent area (red rectangular in Fig. 9), and sea areas around Philippine Islands (purple rectangular in Fig. 9), respectively. As is shown in Table 10, the verification between shipboard profiles and gravity

models demonstrates the improvement in accuracy due to waveform retracking and updated correction of ocean tide, especially obvious over South China Sea Basin and sea areas around Philippine Islands. Besides, the supplement of latest CryoSat-2 and SARAL/AltiKa data also brings better accuracy for constructing marine field model in comparison with V23.1 model.

5. Conclusion

Satellite altimetry provides the most comprehensive images of marine gravity field with accuracies approaching typical shipboard gravity data. Based on multi-satellite altimeter data including the supplement of SARAL/AltiKa, Jason-1 GM and CryoSat-2, we discussed the detailed procedures of constructing regional gravity anomaly grids derived from along-track waveforms. Our analysis used three approaches to reduce the error in the satellite-derived results. First, we compared 6 retracking methods with Jason-1 GM sample data over the research area and selected the two-step WLS retracker with minimum along-track slope error to process raw waveforms of various altimetry missions. Second, we used a resampling procedure combined with a designed low-pass filter to obtain uniformly along-track 5 Hz data with enhanced sampling rate and measuring accuracy. Third we compared 5 ocean tide models with tide gauge data and selected WHU12 model to update corrections. We finally calculated the $1' \times 1'$ marine gravity field model over the Southeastern China Seas using EGM2008 model in the remove/restore procedure.

Table 10
Validation information with NGDC shipboard gravity data over typical areas Unit: mGal.

| Typical area | Validate data description | Minimum | Maximum | Mean | RMS |
|---------------------------------------|---------------------------|---------|---------|--------|-------|
| South China Sea Basin | New result VS Shipboard | −27.984 | 27.208 | −0.938 | 5.986 |
| | EGM2008 VS Shipboard | −20.362 | 20.030 | −1.060 | 6.324 |
| | DTU10 VS Shipboard | −21.242 | 20.428 | −1.045 | 6.403 |
| | DTU13 VS Shipboard | −28.363 | 23.838 | −1.152 | 6.058 |
| | V23.1 VS Shipboard | −3.123 | 29.940 | −1.025 | 6.223 |
| Off Taiwan's southern coast | New result VS Shipboard | −26.338 | 34.126 | 0.187 | 5.217 |
| | EGM2008 VS Shipboard | −20.122 | 20/159 | 0.377 | 5.546 |
| | DTU10 VS Shipboard | −21.301 | 22.399 | 0.349 | 5.478 |
| | DTU13 VS Shipboard | −24.903 | 32.348 | 0.510 | 5.176 |
| | V23.1 VS Shipboard | −36.272 | 29.497 | 0.074 | 6.120 |
| Okinawa through and its adjacent area | New result VS Shipboard | −31.773 | 40.089 | −0.670 | 5.647 |
| | EGM2008 VS Shipboard | −20.031 | 19.997 | 0.040 | 5.610 |
| | DTU10 VS Shipboard | −21.991 | 22.281 | −0.029 | 5.672 |
| | DTU13 VS Shipboard | −28.554 | 28.180 | −0.199 | 5.453 |
| | V23.1 VS Shipboard | −36.029 | 42.795 | −0.682 | 6.141 |
| Around Philippine Islands | New result VS Shipboard | −42.073 | 35.654 | −0.056 | 8.279 |
| | EGM2008 VS Shipboard | −20.395 | 20.112 | −1.834 | 9.216 |
| | DTU10 VS Shipboard | −27.713 | 26.043 | −1.802 | 9.122 |
| | DTU13 VS Shipboard | −25.033 | 27.409 | −1.930 | 8.244 |
| | V23.1 VS Shipboard | −82.436 | 39.187 | 0.478 | 9.539 |

Two approaches are used to evaluate the accuracy of the new gravity model: published global gravity models and NGDC shipboard gravity data, respectively. Kinds of verifications show that accuracy of the new result reaches the level of DTU13 and V23.1. Meanwhile, the new gravity result is slightly better than DTU10 and EGM2008 model. In the selected typical areas with complicated seafloor topography and sea surface topography, the new result is also superior to V23.1 model. Generally speaking, the new result significantly improve the accuracy and resolution of regional gravity models over the Southeastern China Seas due to waveform retracking, low-pass filtering, correction updating and data supplement of new satellite missions.

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