

# SIMBA

## A CubeSat to measure Sun-Earth Imbalance

Julien Amand, Stijn Nevens, Luca Schifano and Christian  
Conscience

Absolute Radiometry  
Royal Meteorological Institute of Belgium (RMIB)  
Solar-Terrestrial Centre of Excellence (STCE)  
ESA IOD funded by BELSPO

IPC XIII, Davos, Switzerland  
October 12, 2021

## Royal Meteorological Institute of Belgium, south of Brussels SOLAR : Sun Observation and Laboratory for Absolute Radiometry



SIMBA

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Intro

RIMB, SOLAR team  
SIMBA

Design

General  
Cavity  
Flat Spectral Sensor

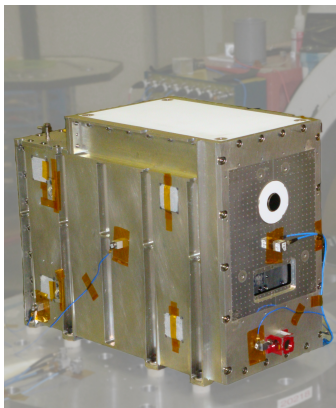
Early Flight

Launch  
Deployment

Characterize the  
Cavity

Active Measure

Looking forward



SovaP radiometer during  
PICARD integration



during a former ICP, Davos,  
CH

# SIMBA : first CubeSat mission

RMIB, Laboratory for Absolute Radiometry

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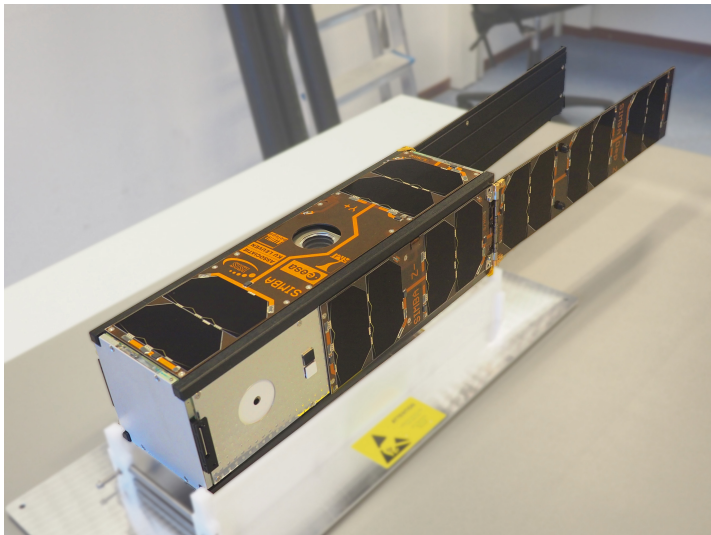
Launch

Deployment

### Characterize the Cavity

### Active Measure

### Looking forward



## The Satellite

- ▶ 3U CubeSat, 4kg, 3.5W, 0.6 MB/day downlink
- ▶ Shared-ride proof-of-concept:
  - ▶ Payload by RMI
  - ▶ ADCS by KUL/Arcsecs
- ▶ kicked off 2014, launched 9/2020
- ▶ mission duration : 2–3 years

## Scientific Payload

**Goal** : measure and monitor the ERB

**Method** : Single Absolute radiometer, swivel from Earth to Sun

# The BUS

Satellite's features

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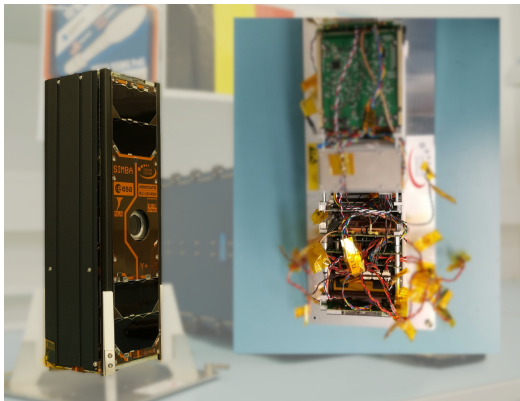
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Conception and  
built : ISISpace,  
Delft, The  
Netherlands



Power,  
communications,  
on-board  
computer

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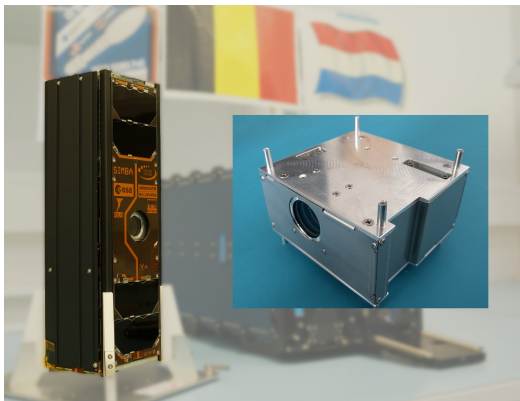
### Early Flight

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### Looking forward



Conception and built : Arcsec, spun off KULeuven, Belgium



Star tracker,  
inertial wheels  
and  
magnetotorquers  
 $\delta\angle \approx 0.1 \text{ deg}$

# The Payload Bay

Satellite's features

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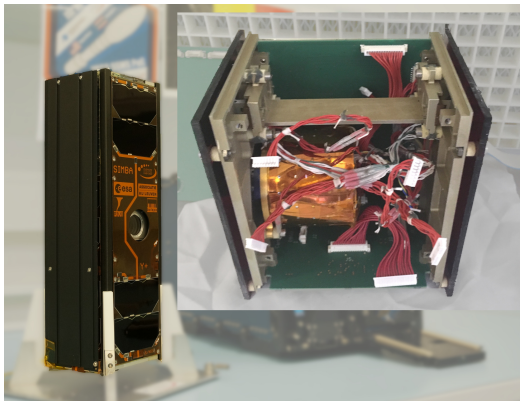
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Conception and  
built : SOLAR  
group, RMI,  
Belgium



Cavity + sensors,  
data acquisition  
and storage



# Bolometric cavity

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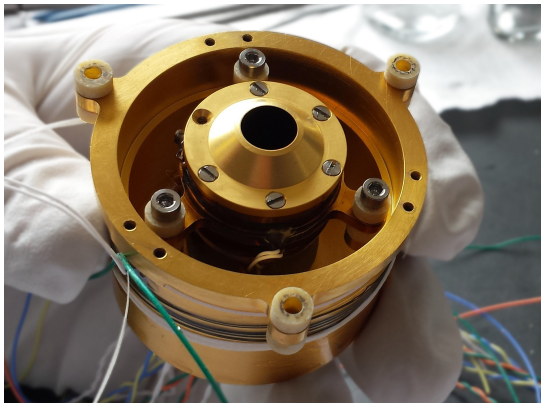
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Bolometric cavity, gold plated anodized aluminium, Velvet Black coating



# Cavity's aperture

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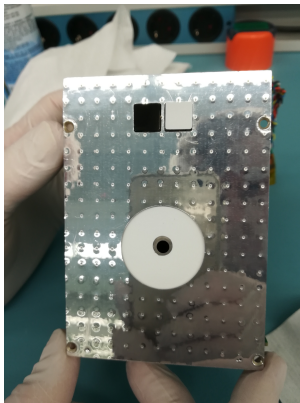
Launch  
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Active Measure

Looking forward

Nadir face of the Sensors bay : cavity precision aperture (Ti + coating), diameter = 5 mm, view angle = 135 deg



# Cavity's sensors and heaters

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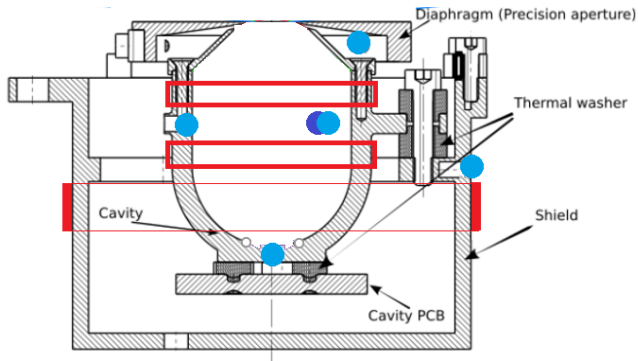
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**Cavity** 2 heating wires + 4 NTC temperature sensors

**Shield** 1 heating wire + 1 NTC

**prec. ap.** 1 NTC



# Flat Surface Spectral sensors (FSS)

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**Flat Spectral Sensor**

Early Flight

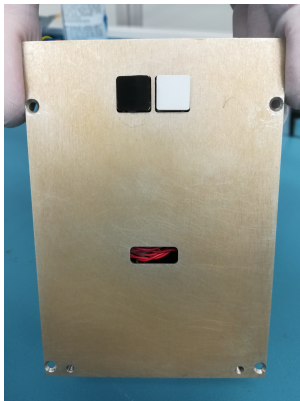
Launch  
Deployment

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Looking forward

1 cm<sup>2</sup>, coated with Velvet Black and white paint to discriminate SWR and LWE



Zenith face with complementary FSS sensors.

# Flat Surface Spectral sensors (FSS)

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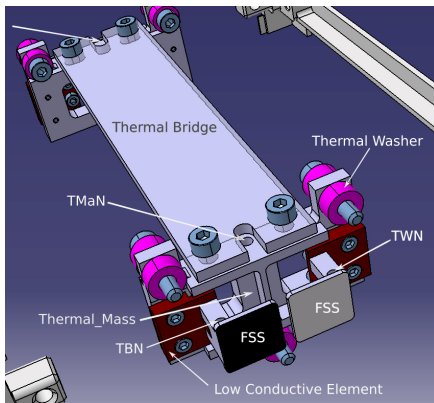
Launch  
Deployment

Characterize the  
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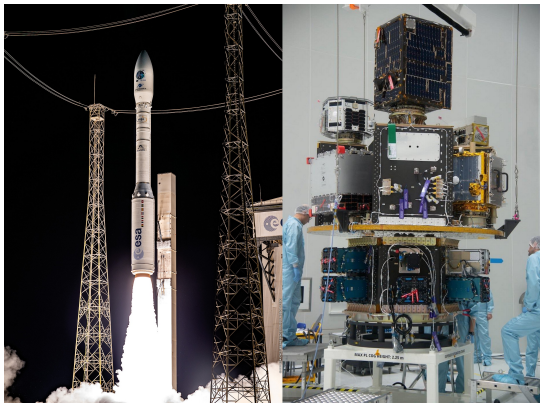
Active Measure

Looking forward

FSS : flux monitored ( $\Delta T$  between surf. and thermal mass),  
Thermal bridge between the faces



Launched with Vega VV16, Small Spacecraft Mission Service (SSMS) PoC (53 CubeSats and two small sats on a single platform) on September the 3rd, 2020, from Kourou.



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**Orbit** "Sun-synchronous", polar orbit

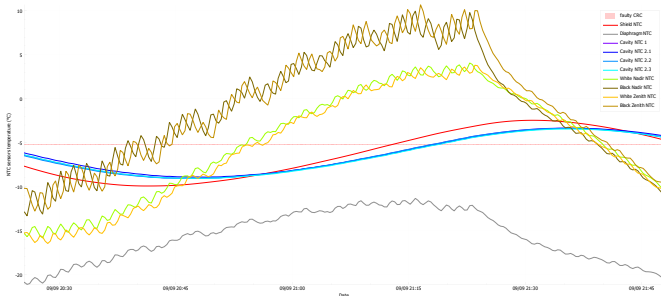
**inclination** 97 deg

**altitude** 550 km

**period**  $\approx$  90 min

**flight-by** 3–5 useful flight-by of ground station in Delft per day

First payload test on sept 9, 2020, passive acquisition,  $\approx 1$  orbit





# FSS Heater test

## Temperature regulation test

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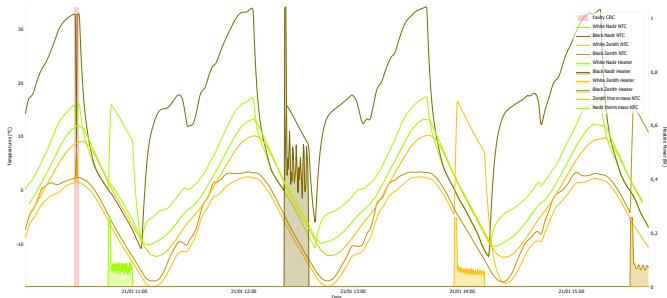
Early Flight

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Looking forward



FSS heated to keep a constant temperature difference with their thermal mass.

# Cavity first regulation test

## Temperature regulation test

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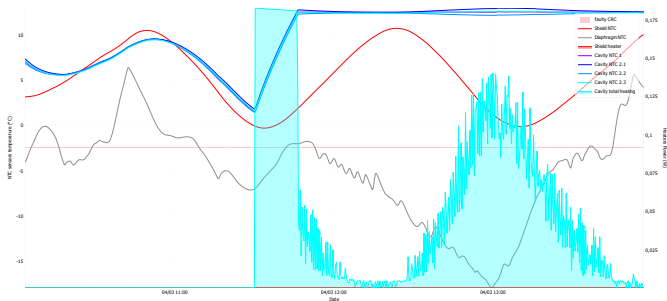
Early Flight

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Looking forward



Cavity can be regulated at a constant temperature with a st. dev as low as  $0.01\text{ }^{\circ}\text{C}$  on the feedback-providing NTC

but

anisotropy with st. dev. on other NTC up to  $0.2\text{ }^{\circ}\text{C}$

# Cavity heater malfunction

## Temperature regulation test

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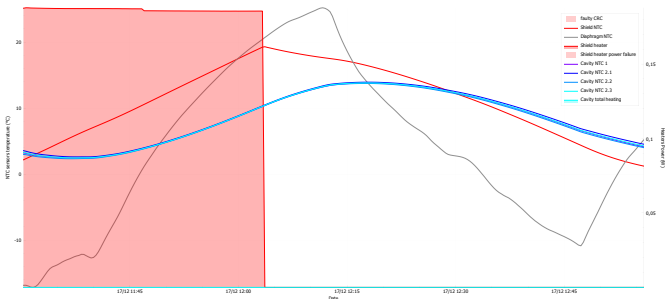
Early Flight

Launch  
Deployment

Characterize the  
Cavity

Active Measure

Looking forward



Shield's heater always at nominal power, probably short-circuited, cannot set at desired temperature.

# Thermal equilibrium in the cavity

## Characterisation of the Cavity

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## Thermal equilibrium in the cavity

$$\underbrace{C^{\theta} \frac{\partial T}{\partial t}}_{=0} = P_{opt}^{in} + P_{opt}^{out} + \Delta R_{dia}^{in} + \Delta R_{dia} + \Delta R_{sh} + \Delta P_{cond} + P_{elec}$$

with

$P_{opt}^{in}$  : the incoming radiation (what we search)

$P_{opt}^{out} = -A_{out}^* \sigma T_{cav}^4$  : thermal radiation escaping the cavity

$\Delta R_{dia}^{in} = A_{dia,in}^* \sigma (T_{dia}^4 - T_{cav}^4)$  : radiation exchange between the precision aperture and the cavity's inside

$\Delta R_{dia} = A_{dia}^* \sigma (T_{dia}^4 - T_{cav}^4)$  : radiation exch. between the prec. ap. and the cavity's outer walls

$\Delta R_{sh} = A_{sh}^* \sigma (T_{sh}^4 - T_{cav}^4)$  : radiation exch. between the shield and the cavity's outer walls

$\Delta P_{cond} = S^{\theta} (T_{sh} - T_{cav})$  : conductive exch. between the shield and the cavity

$P_{elec} = V^2 / R$  : the electrical power input

in a perfect world

$T_{cav}$ ,  $T_{sh}$ ,  $T_{dia}$  being constant, thermal equilibrium becomes

$$P_{opt}^{in} + P_{elec} = Cst$$

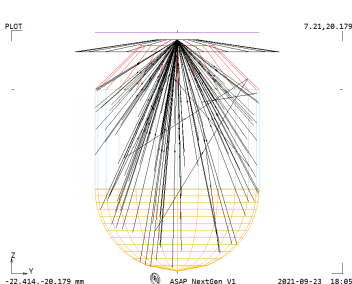
and thus

$$P_{elec}^{\star} - P_{elec}^{\odot} = TSI, \quad P_{elec}^{\star} - P_{elec}^{\otimes} = EOR$$

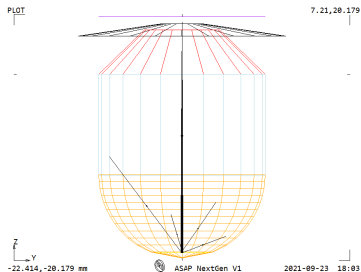
**BUT**

without the shield's regulation and with a precision aperture's temperature varying greatly, all the aforementioned terms must be evaluated.

The absorption of the cavity was evaluated by mean of Ray-Tracing



source at aperture, Earth-like irradiation  
absorption of the cavity : 98,93%



source at infinity, sun-like irradiation  
absorption of the cavity : 98,958%

*Work and figures by Luca Schifano, 2021*

# Radiative exchange with the cavity

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Thermal exchange between two grey-body surfaces  $i$  &  $j$  :

$$\Delta R_{ij} = A_{ij}^* \sigma (T_i^4 - T_j^4)$$

with a fictive equivalent surface

$$A_{ij}^* = \frac{1}{\frac{1-\varepsilon_i}{\varepsilon_i A_i} + \frac{1}{A_i f_{i \rightarrow j}} + \frac{1-\varepsilon_j}{\varepsilon_j A_j}}$$

With the view factors between surface  $i$  &  $j$  :

$$A_i f_{i \rightarrow j} = A_j f_{j \rightarrow i} = \iint \frac{\cos \theta_i \cos \theta_j}{r_{ij}^2} dA_i dA_j.$$

(view factors between geometric forms often have parametric solutions)

### View

factors from the cavity to the shield and the precision aperture

Cavity	Shield		Diaphragm (precision aperture)	
	base (a)	wall (b)	pierced disk (c)	rim inner wall (d)
conical top (1)			0.7487	0.1684
flat top (2)			0.8125	0.092
cylinder (3)	0.0411	0.645	0.0502	0.2173
hemisphere (4)	0.3037	0.3219		
PCB top (5)		0.0407		
PCB sides (6)	0.2271	0.7357		
PCB bottom (7)	0.9425	0.0575		



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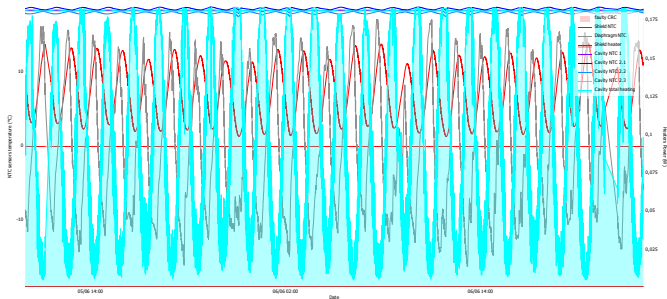
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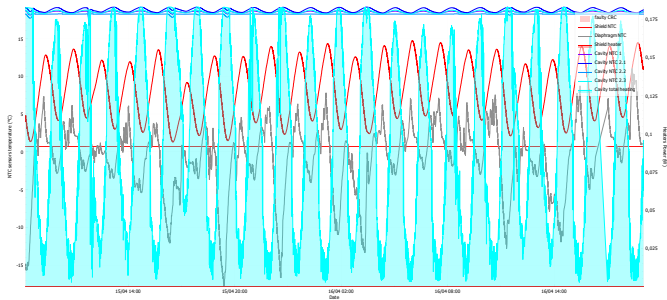
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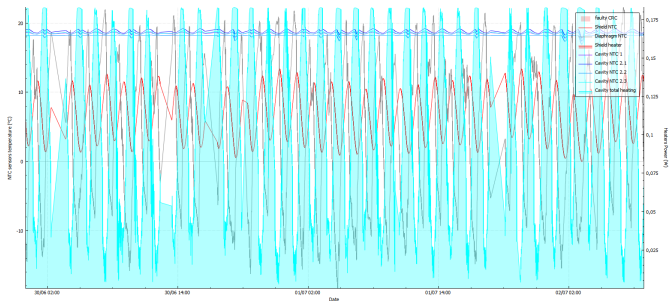
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- ▶ the characterisation of the cavity as for now does not allow yet to balance the equations
- ▶ the pointing inaccuracies (the ADCS took a long time to improve)
- ▶ the minimalist design increases the cost of post treatment

- ▶ share-riding two PoCs brings a lot of uncertainties
- ▶ redundancy!
- ▶ updating the software in orbit might help go around the problem
- ▶ traditional designs are more cumbersome but at least more sturdy
- ▶ cavities should better be tested on the ground before in orbit