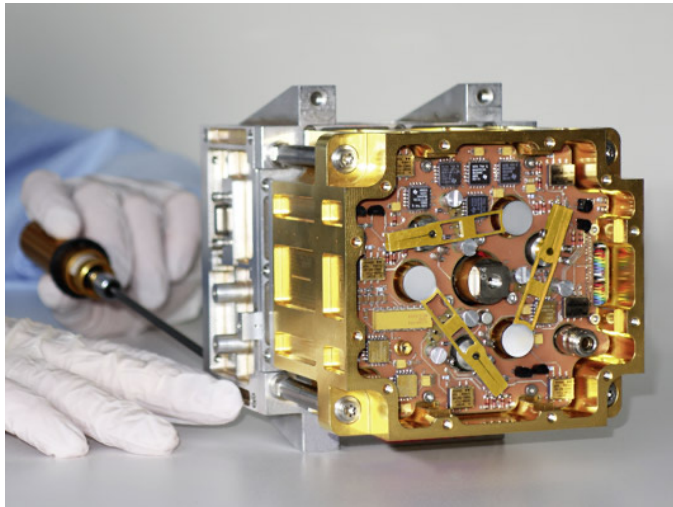
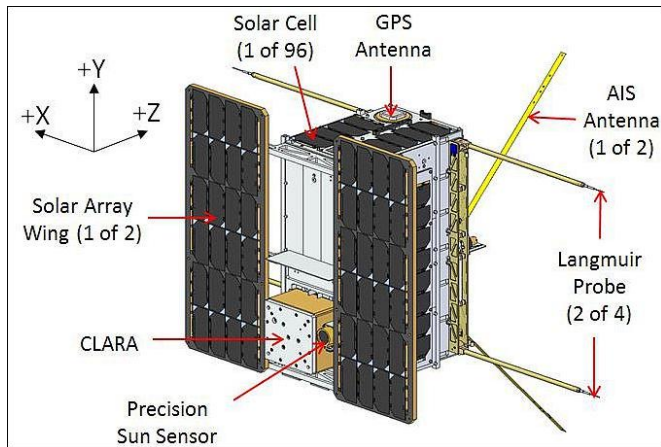


The digital absolute radiometer DARA and its Relatives

Retrospection to Last Decade of
Digitally Controlled Radiometers
for Space Application from the
Engineering Perspective

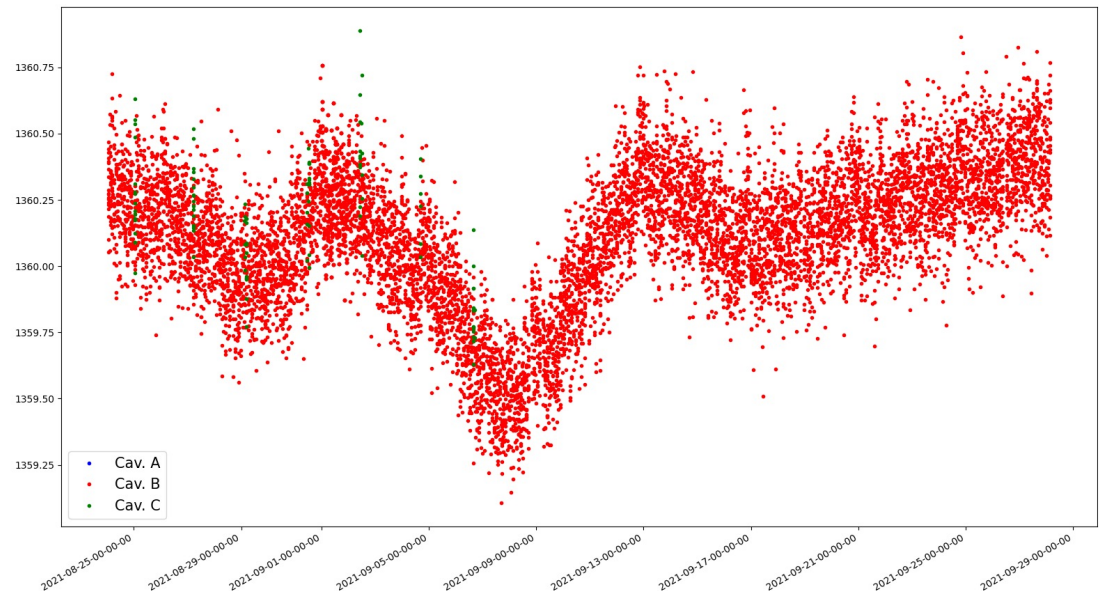
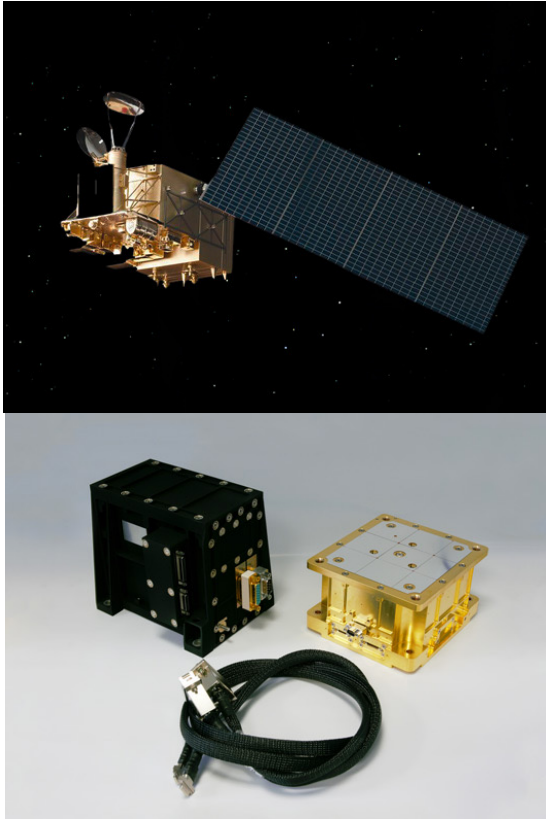
Robert Cerny



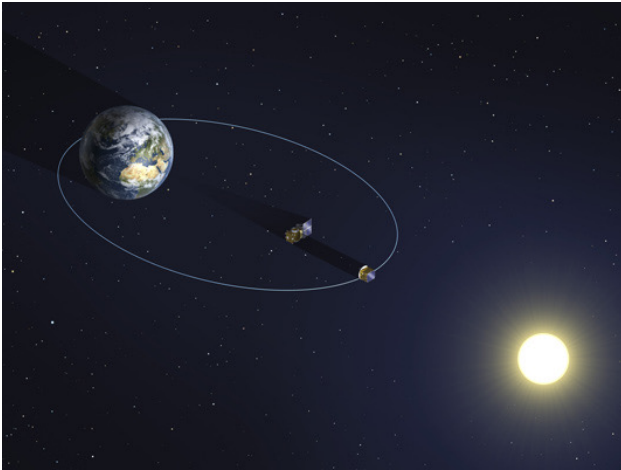
- **Launch date:** 14 July 2017 Baikonur, Kazakhstan
- **Orbit:** Sun-synchronous orbit, altitude 600 km
- **Status:** Instrument is operating, but pointing is not stable due to two defective giro-wheels

FY-3E (DARA-JTSIM)

- **Launch date:** 4. July 2021
- **Orbit:** Sun-synchronous orbit, altitude 836 km
- **Status:** Commissioning is running, first data have been received and are under evaluation



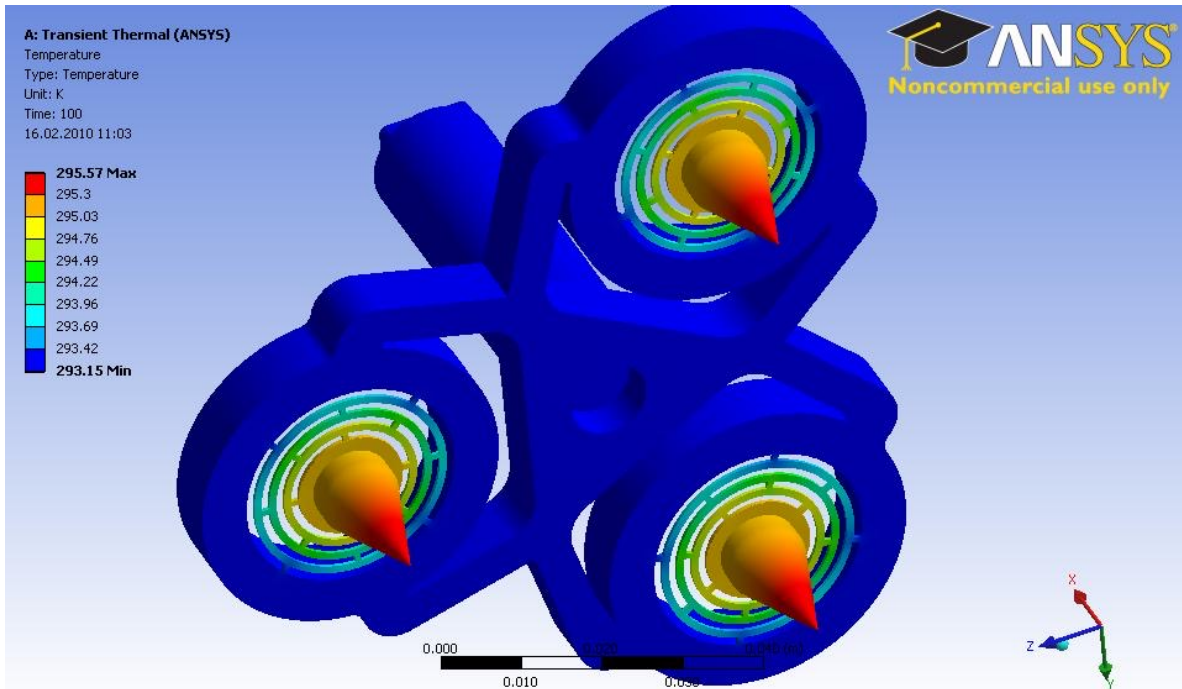
PROBA-3 DARA

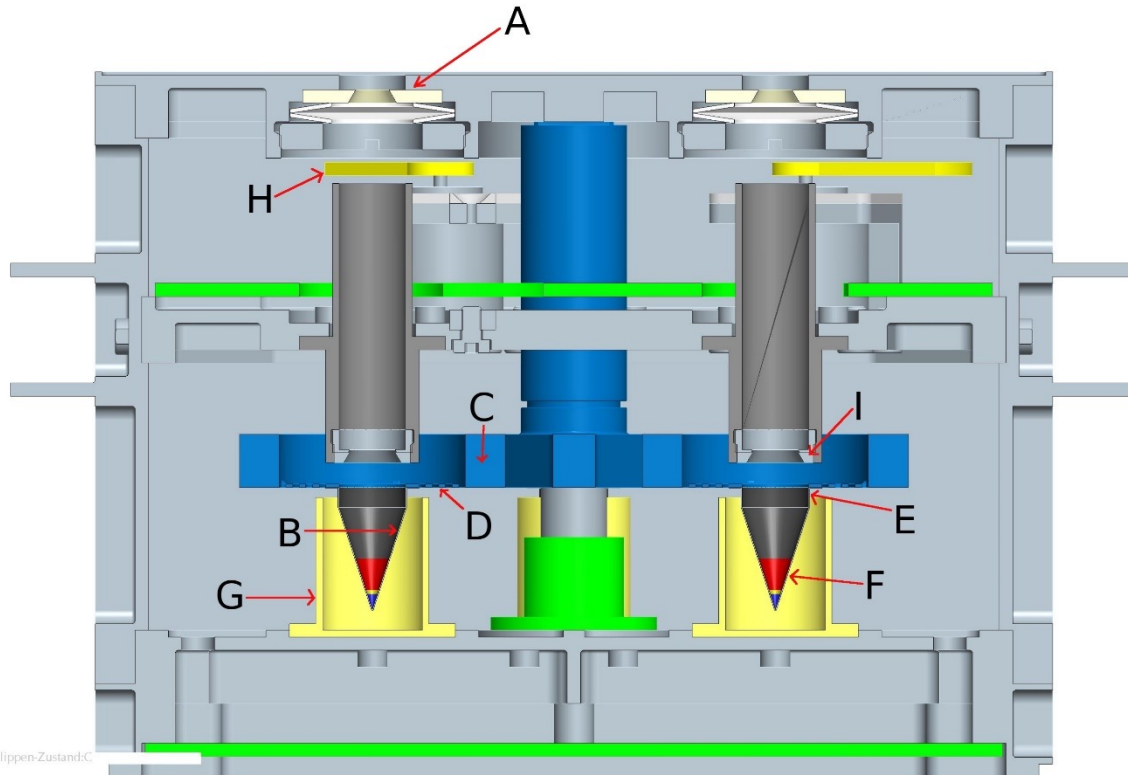


- **Launch date:** mid 2022
- **Orbit:** High Elliptical Earth orbit, 19.7 hours orbital period, 60 530 km apogee, 600 km perigee
- **Status:** Deliver in November 2021, currently in the optical laboratory for none equivalence measurement

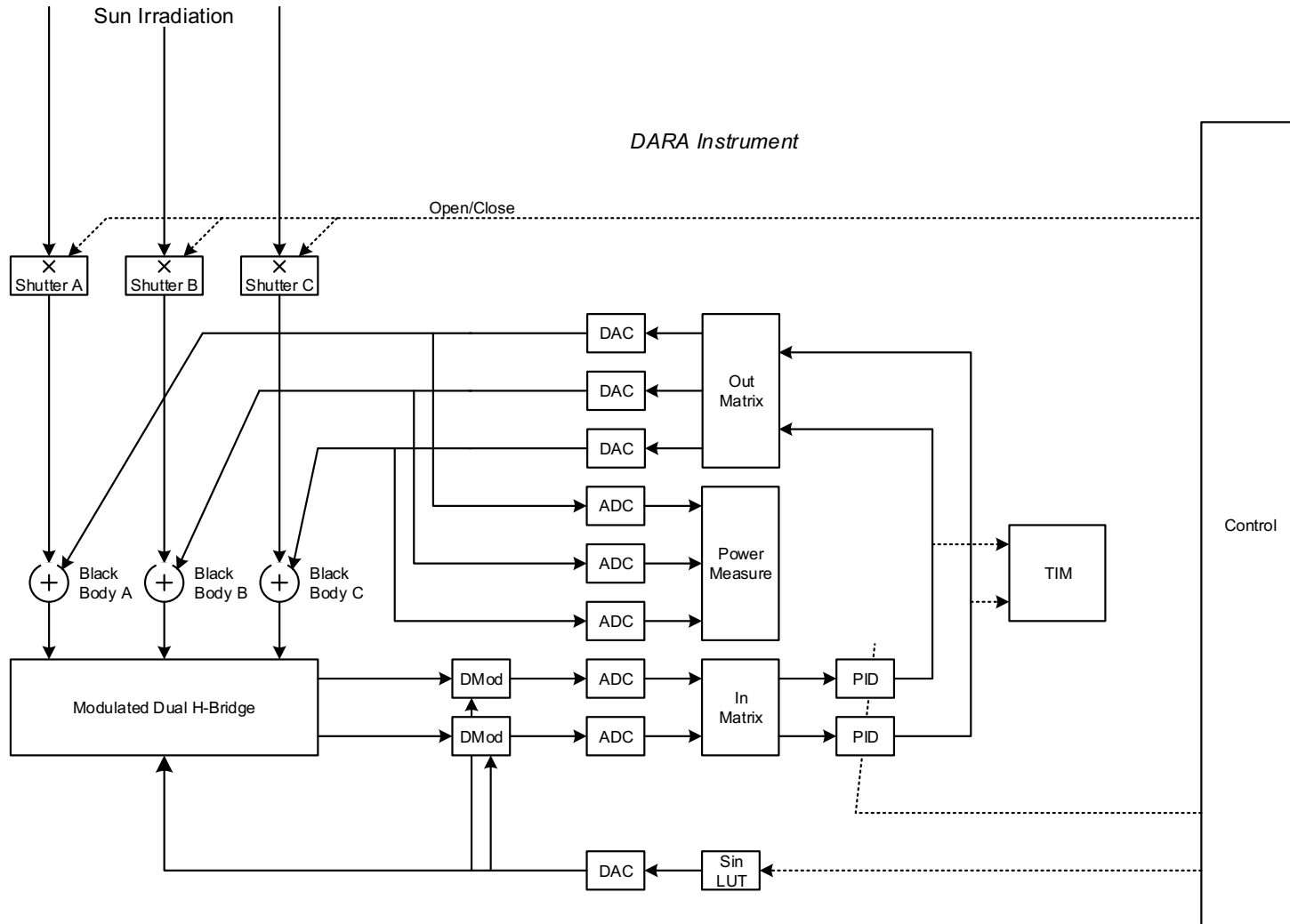
- 3 independently controllable cavities
- Offers several open/close measurement sequences
- Independent PID controllers for closed and open shutter state
- ~20 bit data acquisition for each I and U channel
- Measurement period down to a few seconds
- Uncorrelated sinus carrier for thermal error signal
- Cavities with minimal “Non-Equivalence”
- Very fast shutter speed (few steps and < 100 ms)
- New aperture geometry in comparison to PMO6
- Reduced stray light
- Remove uncertainties due to “Aperture Warming”
- Embedded SW using a RTOS and runs on a MC68332
- Sensor head is thermally isolated to the measurement electronic box

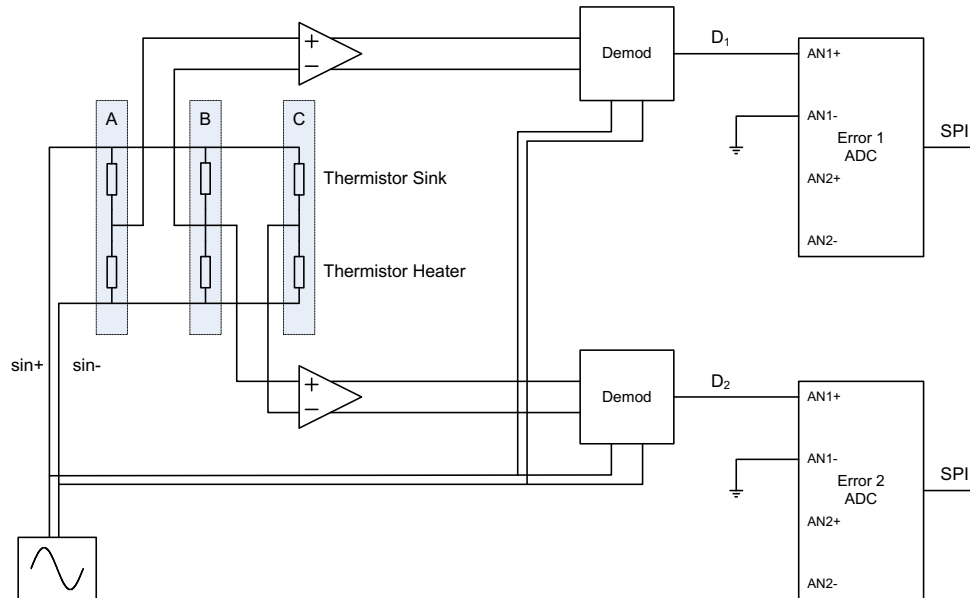






- A) Precision Aperture
- B) Cavity, Aeroglaze Z302 Coating
- C) Heat Sink
- D) Thermal Resistor
- E) Thermometer
- F) Electrical Heater
- G) Radiation Shield
- H) Shutter
- I) View Limiting Aperture

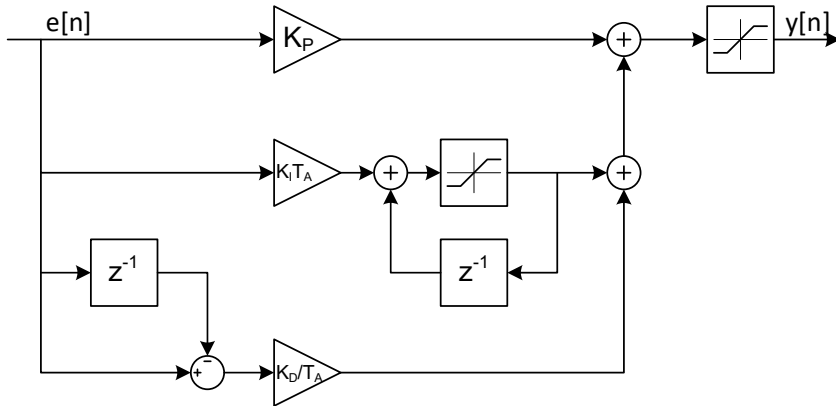




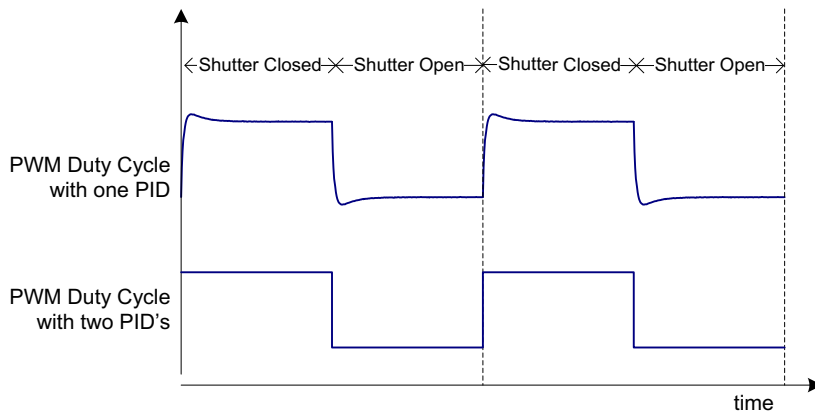
- Reducing noise in the error H-bridge by using a sine carrier
- Using a uncorrelated sine carrier frequency
- Means f_{Sin} is not an overtone of f_{ADC}
- $f_{\text{ADC}} = 20 \text{ Hz}$, $f_{\text{Sin}} = 750 \text{ Hz}$

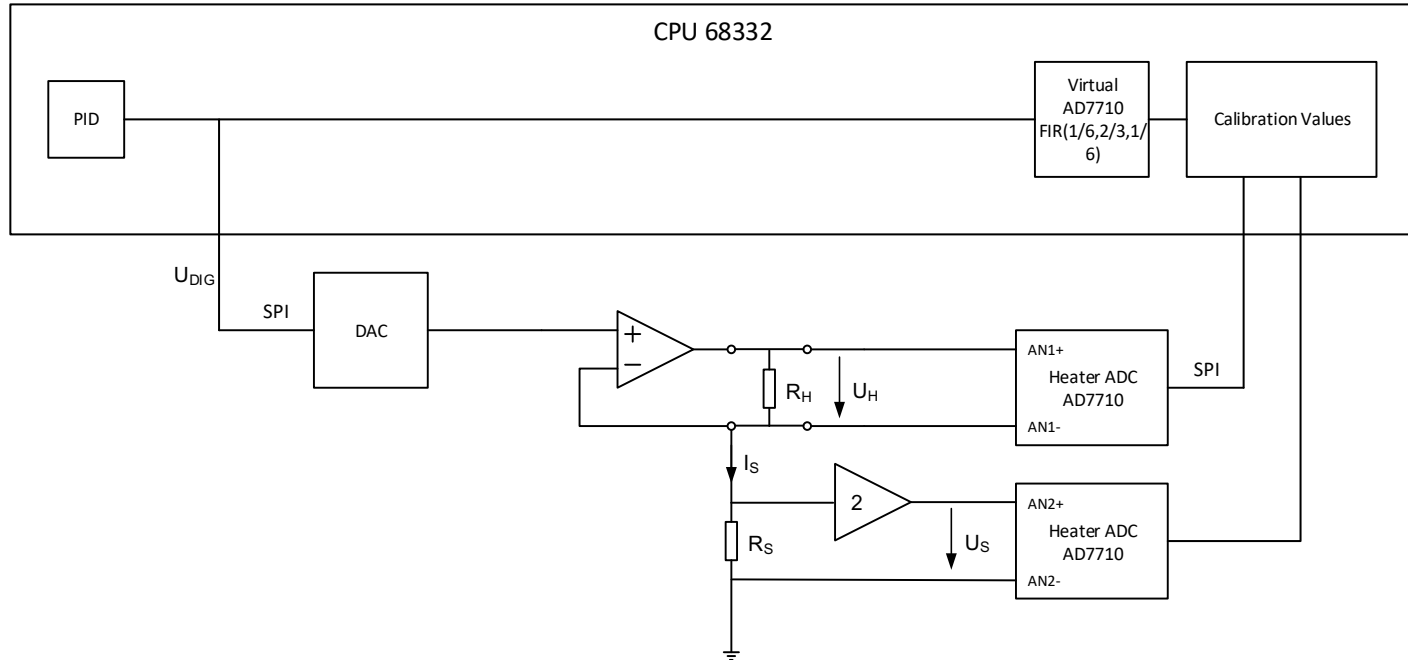
$$f_{\text{Sin}} = f_{\text{PWM}} \left(n + \frac{1}{2} \right)$$

PID Controller Switching



- How can the settling time be reduced when changing the shutter state?
- Two PID controllers per channel
- Significantly less settling time is needed
- Measurement period can be reduced

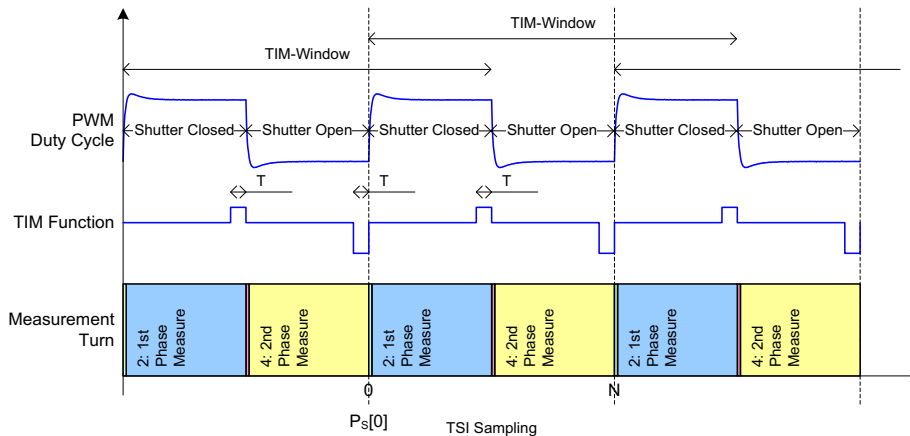




- The digital control value is used to calculate the TSI
- The gain of the heater driver and the heater resistor are periodically calibrated

$$R_H = \frac{2 \cdot U_H}{U_S} \cdot R_S$$

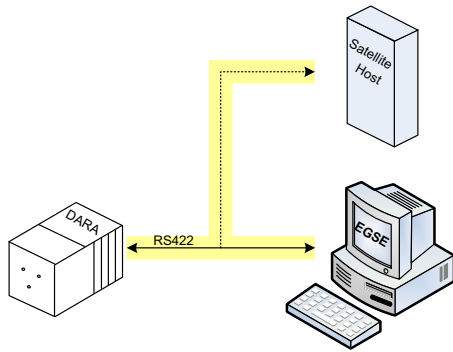
$$G = \frac{U_S}{2 \cdot F_{SINC3}(U_{DIG})}$$



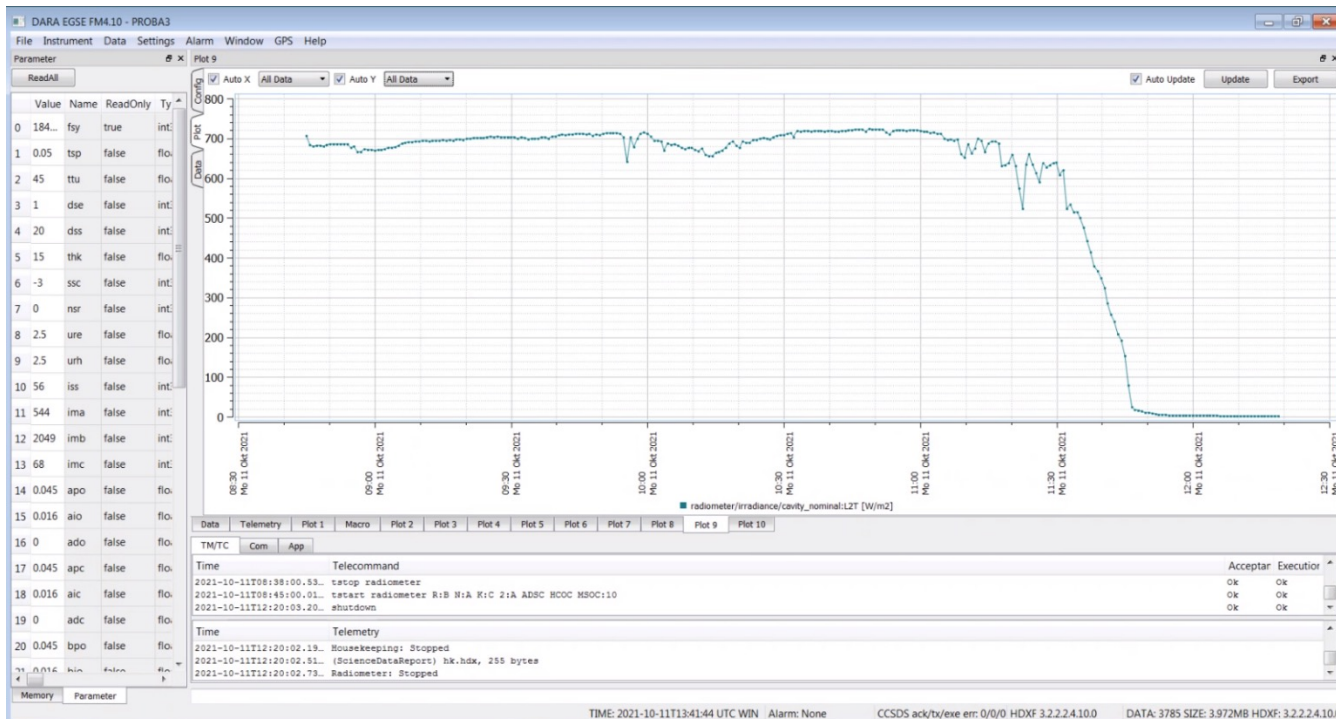
$$P_S = \sum_{n=-N/2-T}^{-N/2-1} P[n] - 2 \sum_{n=-T}^{-1} P[n] + \sum_{n=N/2-T}^{N/2-1} P[n]$$

$$I_S = C_{WRR} W_{Ap} P_S$$

- Tail Integration Method or Traditional Irradiation Measure
- The tail data are integrated
- The sun power is calculated as the difference of 2 measurements made with closed shutter and 1 with open shutter
- One measure per open/close turn



- RS422 communication
- Robust communication protocol
- EGSE software for data visualization and data storage



- Next generation of radiometers are already planned
- Intended features:
 - Increasing accuracy / lower the noise
 - Faster measurement cycles
 - Long term stable on-board voltage reference
 - New cavities design (flat receiver?) under evaluation
 - Leon 3 IP core CPU on a radiation tolerant FPGA